

MOOREBANK INTERMODAL TERMINAL PROJECT

Measurement of Existing Levels of Rail Noise (2018) per Condition 3C

16 July 2019

Tactical Group

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Supplementary professional advice should be sought in respect of these issues.

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1 Introduction

The Moorebank Intermodal Terminal (IMT) involves the development of intermodal freight terminal facilities at Moorebank in south-west Sydney, linked by rail to Port Botany and the interstate rail network. The Project includes the IMT, a rail link connecting the IMT to the Southern Sydney Freight Line (SSFL) and road entry and exit points along Moorebank Avenue.

An Environmental Impact Statement (EIS) for the IMT was prepared and exhibited in 2014. Following the preparation of a Submissions Report and a Supplementary Response to Submissions Report in 2015, the project was approved by the NSW Planning Assessment Commission in 2016. Construction works commenced in 2017.

The final approval for the Moorebank IMT¹ includes conditions which relate to operational noise from freight trains.

This report has been prepared to establish the existing levels of rail noise in accordance with the Rail Infrastructure Noise Guideline (RING). This information will form part of the Rail Noise Management Plan for the Moorebank IMT. The requirements of Mitigation Measure 3C are copied verbatim below. This report addresses the scope shown in **bold** font.

*3C. A Rail Noise Management Plan (RNMP) (or equivalent) will be prepared prior to operation of the Proposal. The RNMP will include procedures for the application of friction modifiers to the Rail link and measurement and reporting of subsequent rail noise levels should be documented in a Rail Noise Management Plan (RNMP) (or equivalent) to be prepared prior to the operation of the proposal. **During preparation of the RNMP, background rail noise monitoring will be undertaken to establish existing levels of rail noise levels in accordance with the RING.** The RNMP will prescribe mitigation measures where modelling predicts and/or operational monitoring shows an exceedance attributable to the Proposal that RING prescribes as a trigger level.*

The work documented in this report was carried out in accordance with the Renzo Tonin & Associates Quality Assurance System, which is based on Australian Standard / NZS ISO 9001. Appendix A contains a glossary of acoustic terms used in this report.

¹ State Significant Development (SSD) Approval 6766, Minister for Planning, 12 December 2016

2 Monitoring locations and dates

Attended and unattended noise measurements have been undertaken to establish the existing levels of rail noise at four locations near the Moorebank IMT development site. These locations are to the west, south-west, south and east of the IMT. The four measurement locations are considered representative of the residential areas potentially most impacted by freight trains accessing the IMT.

Long-term unattended measurements to the west (Glenfield Farm) were undertaken over a 2-week period in August 2017. Additional long-term unattended measurements to the south-west, south and east were undertaken over a 2-week period between 27 November and 10 December 2018. Attended measurements were conducted at each location to confirm the relative contribution of rail traffic and other extraneous noise influencing the measurement results.

A diagram of the track layout is provided in Figure 2-1. Existing rail traffic in the vicinity of the IMT consists of passenger services on the East Hills and Main South Lines and freight traffic on the Southern Sydney Freight Line (SSFL) and Main South Line. The East Hills Line diverges from the Main South Line north of Glenfield Station. At this point the Up track is on viaduct and the Down track is at-grade. Freight trains generally travel on the SSFL north of Glenfield, with occasional freight services on the Main South Line. The SSFL continues north on viaduct from Glenfield for approximately 2 km before returning to grade.

A map of the noise measurement locations in relation to the existing rail lines and IMT is provided in Figure 2-2. The noise measurement periods are summarised in Table 2-1.

Figure 2-1 Track diagram

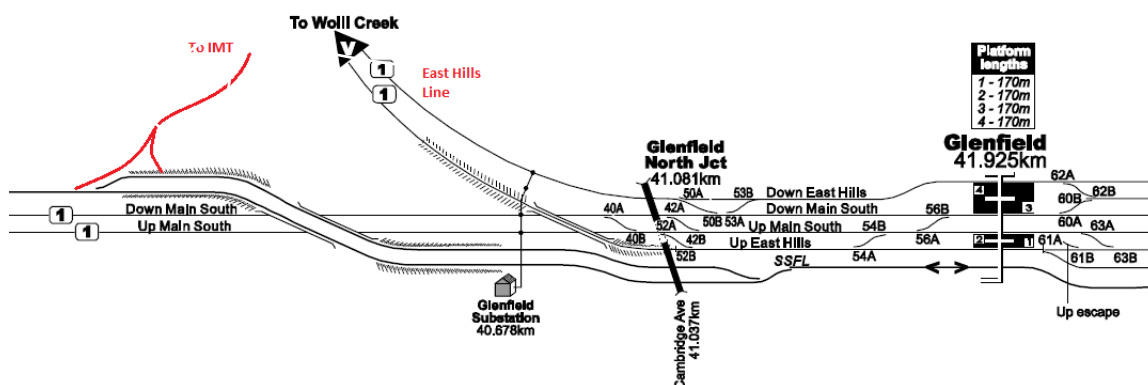


Figure 2-2 Noise measurement locations



Table 2-1 Noise measurement locations and dates

Location	Direction from the IMT	Unattended measurement period	Attended measurement period
88 Leacocks Lane, Casula (Glenfield Farm) ¹	West ¹	01/08/2017 – 13/08/2017 ¹	01/08/2018 ¹
15 Slessor Road, Casula	West	27/11/2018 – 10/12/2018	10/12/2018
11 Goodenough Street, Glenfield	South	27/11/2018 – 10/12/2018	10/12/2018
Public area adjacent to 19 Wallcliffe Court, Wattle Grove	East	27/11/2018 – 10/12/2018	10/12/2018

Note: 1. Measurements conducted as part of an expert report prepared by Dr Renzo Tonin (ref 2)

2.1 88 Leacocks Lane, Casula (Glenfield Farm)

Noise measurements to the west of the IMT development site at 88 Leacocks Lane or “Glenfield Farm” were conducted as part of an expert report by Dr Renzo Tonin². Long-term unattended monitoring was conducted between 1 August and 13 August 2017. The noise logger was placed in the rear yard overlooking the Glenfield Waste Facility. The logger was positioned approximately 207 m from the nearest track and 18 m from the nearest façade of the main house. The microphone was at a height of 1.5 m above the local ground level. Attended monitoring was conducted at the same location.

A map of the measurement location is shown in Figure 2-3. A picture of the noise logger and the attended monitoring equipment is provided in Figure 2-4.

² Qube Holdings Limited & Minister for Planning ats Residents Against Intermodal Development Moorebank Incorporated – Site: Moorebank Avenue, Moorebank NSW | L&EC Proceedings No 2017/81889 | Expert Report in Acoustics of Renzo Tonin

Figure 2-3 88 Leacocks Lane, Casula (Glenfield Farm) - Noise Measurement Location



Figure 2-4 Leacocks Lane, Casula – Noise Measurement Equipment



2.2 15 Slessor Road, Casula

Noise measurements to the south west of the IMT development site were taken at 15 Slessor Road. For long-term unattended monitoring, the noise logger was placed in a position clear of obstructions within the property boundary, approximately 1.3 m from the boundary fence facing the rail corridor and 6.5 m from the nearest façade of the residence. The logger was positioned approximately 132 m from the nearest track. The microphone was placed on an extension pole at a height of 3.2 m above ground (approximately 1 m above the top of the boundary fence).

Attended monitoring was conducted adjacent to the rail corridor in the public near 15 Slessor Road. The microphone was positioned approximately 21 m from the freight viaduct at a height of 1.5 m above the local ground level.

A map of the unattended and attended monitoring locations is shown in Figure 2-5. A picture of the noise logger position is provided in Figure 2-6.

Figure 2-5 15 Slessor Road, Casula - Noise Measurement Locations



Figure 2-6 15 Slessor Road, Casula – Unattended Noise Measurement Equipment



2.3 11 Goodenough Street, Glenfield

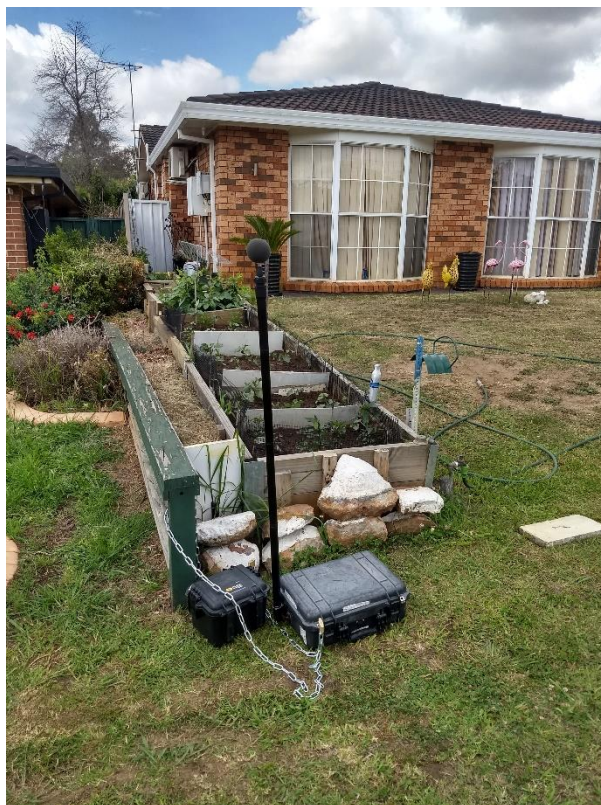
Noise measurements to the south of the IMT development site were taken at 11 Goodenough Street. For long-term unattended monitoring, the noise logger was placed in a position clear of obstructions near the property boundary facing the rail corridor. The logger was positioned approximately 620 m from the nearest track and 8 m from the nearest façade of the residence. The microphone was at a height of 1.5 m above the local ground level. Attended monitoring was conducted using the same logger at the same location.

A map of the measurement location is shown in Figure 2-7. A picture of the noise logger used for both unattended and attended measurements is provided in Figure 2-8.

Figure 2-7 11 Goodenough Street, Glenfield – Noise Measurement Location



Figure 2-8 11 Goodenough Street, Glenfield – Noise Measurement Equipment



2.4 19 Wallcliffe Court, Wattle Grove

Noise measurements to the east of the IMT development site were taken at 19 Wallcliffe Court. The unattended monitor was positioned on public land, adjacent to 19 Wallcliffe Court, as access to the residence could not be obtained at the time of installation. The unattended noise logger was positioned approximately 64 m from the nearest track, 23 m from the nearest façade of the residence, and the microphone was 1.5 m above the local ground level. The southern façade of the residence at 19 Wallcliffe Court is 85 m from the nearest track.

Attended measurements were conducted at three positions for the purposes of determining the rate at which noise levels reduce with increasing distance from the East Hills Line. Microphone distances were 26 m from the nearest track (near 30 Wallcliffe Circuit) at a height of 3.2 m, 64 m from the nearest track (unattended logger location) at a height of 1.5 m and 146 m from the nearest track (near 14 Somercotes Circuit) at a height of 1.5 m.

A map of measurement locations is shown in Figure 2-9. Pictures of the noise logger and attended measurement equipment are provided in Figure 2-10.

Figure 2-9 19 Wallcliffe Court, Wattle Grove - Noise Measurement Locations



Figure 2-10 19 Wallcliffe Court, Wattle Grove - Noise Measurement Equipment

3 Measurement methodology

3.1 Details of noise survey and measurement equipment

At each monitoring location, unattended measurement equipment consisted of one RTA Technology noise logger which comprises an NTi Audio XL2 Type 1 sound level meter. Attended measurement equipment also consisted of RTA Technology noise loggers. The calibration of each instrument was verified prior and subsequent to measurements using a Bruel and Kjaer Type 4231 calibrator. In all cases, no significant drift [less than 0.5 dB(A)] in calibration level was observed. Microphones were fitted with windscreens for the entire duration of measurements.

All instrumentation complies with IEC 61672 (parts 1-3) '*Electroacoustics - Sound Level Meters*' and IEC 60942 '*Electroacoustics - Sound calibrators*' and carries current NATA certification.

Table 3-1 Measurement Equipment

Location	Instrument	Make	Model	Serial Number	Last Calibrated
88 Leacocks Lane, Casula (Glenfield Farm)	RTA Technology Noise Logger (RTA 07_018)	NTi	XL2	A2A-12698-E0	22 May 2017
15 Slessor Road, Casula	RTA Technology Noise Logger (RTA 05_006)	NTi	XL2	A2A-04313-D1	20 May 2017
Public area adjacent to 19 Wallcliffe Court, Wattle Grove	RTA Technology Noise Logger (RTA 07_017)	NTi	XL2	A2A-12143-E0	10 March 2017
11 Goodenough Street, Glenfield	RTA Technology Noise Logger (RTA 06_010)	NTi	XL2	A2A-05811-E0	31 Oct 2018
Attended measurements, Park Near 15 Slessor Road, Casula	RTA Technology Noise Logger (RTA 06_010)	NTi	XL2	A2A-05811-E0	31 Oct 2018
Attended measurements, Public area adjacent to 19 Wallcliffe Court, Wattle Grove 26 m from rail	RTA Technology Noise Logger (RTA 05_006)	NTi	XL2	A2A-04313-D1	20 May 2017
Attended measurements, Public area adjacent to 19 Wallcliffe Court, Wattle Grove 64 m from rail	RTA Technology Noise Logger (RTA 07_017)	NTi	XL2	A2A-12143-E0	10 March 2017
Attended measurements, Public area adjacent to 19 Wallcliffe Court, Wattle Grove 146 m from rail	RTA Technology Noise Logger (RTA 06_010)	NTi	XL2	A2A-05811-E0	31 Oct 2018
Attended and Unattended measurement locations	Type 1 Sound Level Meter Calibrator	Bruel & Kjaer	Type 4231	3017534	27 July 2018

3.2 Site features and observations

During set up of the noise loggers and attended measurements, observations of any site features and/or audible characteristics potentially influencing the measurement results were made.

88 Leacocks Lane, Casula (Glenfield Farm)

At 88 Leacocks Lane, noise from passenger and freight train operations on the Main South Line and SSFL was audible. During the day period, noise levels during train passby events were frequently influenced by extraneous noise sources, including noise from birds, sheep, aircraft and equipment operating at the Glenfield Waste Plant.

15 Slessor Road, Casula

At 15 Slessor Road, noise from passenger and freight train operations on the Main South Line and SSFL was audible. Other noise sources included road traffic noise from Glenfield Road and natural noise sources.

11 Goodenough Street, Glenfield

At 11 Goodenough Street, noise emissions were primarily influenced by road traffic noise on Cambridge Avenue, construction noise, aircraft noise and birds. Train passbys were not audible during the day period. During night periods, passbys were occasionally audible (usually freight trains on the Main South Line and SSFL).

19 Wallcliffe Court, Wattle Grove

At the monitoring location adjacent to 19 Wallcliffe Court, all train passbys were passenger rail services on the East Hills Line and were clearly audible. Other noise sources included noise from natural noise sources and construction noise.

3.3 Weather observations

Weather conditions during the noise surveys was based on Bureau of Meteorology results and observations from the noise logging audio and spectra. Weather data from the weather station at Holsworthy Aerodrome was used to assist in identifying periods for data exclusion. Any periods impacted by excessive wind (> 5 m/s) or heavy rain were excluded from the analysis.

3.4 Measurement parameters and data analysis

For long-term monitoring at each location, each noise logger was set up to measure the L_{Aeq} and $L_{Amax,fast}$ noise levels in consecutive 1 second intervals throughout the survey period, and also the statistical noise levels in each 15-minute interval.

For each train passby event, the time period for the noise measurement was determined on the basis of the procedure described in Section 6.6.3 of International Standard ISO3095:2013, whereby the measurement commences when the noise level is at least 10 dB lower than when the front of the train is opposite the microphone and concludes when the noise level is at least 10 dB lower than when the end of the train is opposite the microphone.

Train passbys were identified using the NTi Data Explorer software. This was used to produce a summary of the $L_{Aeq(passby)}$, SEL (L_{AE}) and $L_{Amax,fast}$ noise levels for each passby. For each train passby, the train type (passenger or freight) was determined based on the passby duration and time lapse photography captured from two vision loggers (refer Figure 2-2). The noise measurement results were used to calculate the $L_{Aeq(15hour)}$, $L_{Aeq(9hour)}$ and $L_{AFmax,95\%}$ noise levels for each day and night period for passenger and freight trains.

4 Measurement results

4.1 Overall noise levels

The measurement of overall noise levels was undertaken based on the procedure documented in the NSW Noise Policy for Industry (EPA 2017)³. The long-term noise levels were established based on the measured noise levels in consecutive 15-minute intervals after removing weather-affected periods and other extraneous noise. The long-term noise levels include noise contributions from all ambient sources near the monitoring locations, including road traffic noise, rail noise and natural sources. The noise contribution from rail traffic only (refer Section 4.2) will be less than the ambient noise levels from all sources in Table 4-1.

A graphical summary of the 15-minute noise measurement results at each location is provided in APPENDIX C.

Table 4-1 Summary of measured ambient L_{Aeq} noise levels - facade reflected (weekly average)

Location	Measured Daytime (7am to 10 pm) $L_{Aeq(15hour)}$ Noise Levels, dB(A) ²	Measured Night-time (10pm to 7 am) $L_{Aeq(9hour)}$ Noise Levels, dB(A) ²
88 Leacocks Lane (Glenfield Farm)	60 ¹	55 ¹
15 Slessor Road	57	54
11 Goodenough Street	54	50
19 Wallcliffe Court	55	51

Note: 1. Measurements conducted as part of an expert report by Dr Renzo Tonin (Ref 2)

Note: 2. The measured noise levels include noise contributions from all ambient sources near the monitoring locations, including road traffic noise, rail noise and natural sources.

4.2 Rail noise contributions

At each monitoring location, the $L_{Aeq(passby)}$, SEL (L_{AE}) and $L_{Amax,fast}$ noise levels were determined for each train passby as described in Section 3.4. The procedure in Clause 3.4.1.1 of the Rail Infrastructure Noise Guideline (EPA, 2013) was used, together with the number of train passbys during the day and night periods to calculate the $L_{Aeq(15hour)}$ daytime, $L_{Aeq(9hour)}$ night-time and $L_{Amax,95\%}$ noise levels from train passbys.

A summary of the measurement results for each train passby is provided in a spreadsheet format as a separate deliverable.

³ NSW EPA Noise Policy for Industry – Fact Sheet B: Measurement procedures for determining background noise, 2017

The measurement results for each passby include the following information:

- Date
- Start time of the train passby
- Train type (Passenger or Freight)
- Measurement duration (between approximate 10 dB down points before and after passby)
- SEL (L_{Ae}) noise measurement
- L_{AFmax} noise measurement

The $L_{Aeq(15hour)}$ daytime, $L_{Aeq(9hour)}$ night-time and $L_{AFmax,95\%}$ noise levels were calculated at the façade of the four receiver locations for passenger and freight trains separately.

A summary of the daily noise contributions from each train type is provided in APPENDIX B. The weekly logarithmic average L_{Aeq} noise levels (weekday average). This is considered to represent the noise levels associated with the reasonable maximum use, or the 'worst-case' typical day per the requirements of Table Note 9 in the RING. The L_{Aeq} and highest daily $L_{AFmax,95\%}$ noise levels are summarised in Table 4-2.

At 11 Goodenough Street, rail noise was not audible during the equipment setup or attended monitoring. Review of the noise logger data revealed four detectable freight train passbys with L_{AFmax} levels between 47 dB(A) and 52 dB(A) and one detectable passenger train passby with L_{AFmax} of 42 dB(A). All detectable passbys occurred between 12:00 am (midnight) and 3:00 am when background noise levels were lowest.

Table 4-2 Summary of measured train passby noise levels - facade reflected (weekly average)

Location	Measured Daytime Noise Level (7am to 10 pm) $L_{Aeq(15hour)}$, dB(A)			Measured Night-time Noise Level (10pm to 7 am) $L_{Aeq(9hour)}$, dB(A)			Measured $L_{AFmax,95\%}$ (highest daily) Noise Level, dB(A)		
	Passenger	Freight	Total	Passenger	Freight	Total	Passenger	Freight	Total
88 Leacocks Ln	54	52	56	48	50	52	76	85	-
15 Slessor Rd	50	52	54	47	51	52	72	80	-
11 Goodenough St	The noise contribution from existing passenger and freight trains is negligible at this locality. The highest L_{Amax} noise level from freight trains not influenced by ambient noise was 52 dB(A).								
30 Wallcliffe Ct (26 m from rail)	61 ³	n/a	61 ³	58 ³	n/a	58 ³	85 ³	n/a	85 ³
19 Wallcliffe Ct Logger Location (64 m from rail)	53	n/a	53	49	-	49	77	n/a	77
14 Somercotes Ct (146 m from rail)	46 ³	n/a	46 ³	43 ³	n/a	43 ³	69 ³	n/a	69 ³

Note: 1. Measurements conducted as part of a report by Dr Renzo Tonin (Ref 2).

2. Passenger train noise not included.

3. Distance attenuation determined from attended measurements (refer Appendix D).

5 Conclusions

Unattended noise monitoring was undertaken at four representative locations to the west, south west, south and east of the Moorebank IMT development site for a period of 2-weeks at each location.

Rail noise contributions have been calculated at the façade of the representative receivers, consistent with the requirements of the RING. Noise levels have been separately quantified for passenger and freight trains. The weekly average L_{Aeq} and highest daily $L_{AFmax,95\%}$ noise levels at the façade of the nearest residence to each monitoring location is provided in Table 4-2.

APPENDIX A Glossary of terminology

The following is a brief description of the technical terms used to describe noise to assist in understanding the technical issues presented.

Adverse weather	Weather effects that enhance noise (that is, wind and temperature inversions) that occur at a site for a significant period of time (that is, wind occurring more than 30% of the time in any assessment period in any season and/or temperature inversions occurring more than 30% of the nights in winter).
Ambient noise	The all-encompassing noise associated within a given environment at a given time, usually composed of sound from all sources near and far.
Assessment period	The period in a day over which assessments are made.
Assessment point	A point at which noise measurements are taken or estimated. A point at which noise measurements are taken or estimated.
Background noise	Background noise is the term used to describe the underlying level of noise present in the ambient noise, measured in the absence of the noise under investigation, when extraneous noise is removed. It is described as the average of the minimum noise levels measured on a sound level meter and is measured statistically as the A-weighted noise level exceeded for ninety percent of a sample period. This is represented as the L90 noise level (see below).
Decibel [dB]	The units that sound is measured in. The following are examples of the decibel readings of every day sounds: 0dB The faintest sound we can hear 30dB A quiet library or in a quiet location in the country 45dB Typical office space. Ambience in the city at night 60dB CBD mall at lunch time 70dB The sound of a car passing on the street 80dB Loud music played at home 90dB The sound of a truck passing on the street 100dB The sound of a rock band 115dB Limit of sound permitted in industry 120dB Deafening
dB(A)	A-weighted decibels. The A-weighting noise filter simulates the response of the human ear at relatively low levels, where the ear is not as effective in hearing low frequency sounds as it is in hearing high frequency sounds. That is, low frequency sounds of the same dB level are not heard as loud as high frequency sounds. The sound level meter replicates the human response of the ear by using an electronic filter which is called the "A" filter. A sound level measured with this filter switched on is denoted as dB(A). Practically all noise is measured using the A filter.
dB(C)	C-weighted decibels. The C-weighting noise filter simulates the response of the human ear at relatively high levels, where the human ear is nearly equally effective at hearing from mid-low frequency (63Hz) to mid-high frequency (4kHz), but is less effective outside these frequencies.
Frequency	Frequency is synonymous to pitch. Sounds have a pitch which is peculiar to the nature of the sound generator. For example, the sound of a tiny bell has a high pitch and the sound of a bass drum has a low pitch. Frequency or pitch can be measured on a scale in units of Hertz or Hz.
Impulsive noise	Having a high peak of short duration or a sequence of such peaks. A sequence of impulses in rapid succession is termed repetitive impulsive noise.
Intermittent noise	The level suddenly drops to that of the background noise several times during the period of observation. The time during which the noise remains at levels different from that of the ambient is one second or more.
L _{Aeq} (15hour)	The "equivalent A-weighted noise level" is the summation of noise events integrated over the 15 hour daytime period.

L _{Aeq(9hour)}	The "equivalent A-weighted noise level" is the summation of noise events integrated over the 9 hour night-time period.
L _{AFmax,95%}	The 95th percentile L _{AFmax} level for train passbys (i.e. the L _{AFmax} level not exceeded by 95% of passbys). The L _{AFmax} level is the maximum A-weighted, fast response sound pressure level measured over a given period
L _{Max}	The maximum sound pressure level measured over a given period.
L _{Min}	The minimum sound pressure level measured over a given period.
L ₁	The sound pressure level that is exceeded for 1% of the time for which the given sound is measured.
L ₁₀	The sound pressure level that is exceeded for 10% of the time for which the given sound is measured.
L ₉₀	The level of noise exceeded for 90% of the time. The bottom 10% of the sample is the L ₉₀ noise level expressed in units of dB(A).
L _{eq}	The "equivalent noise level" is the summation of noise events and integrated over a selected period of time.
Reflection	Sound wave changed in direction of propagation due to a solid object obscuring its path.
SEL	Sound Exposure Level (SEL) is the constant sound level which, if maintained for a period of 1 second would have the same acoustic energy as the measured noise event. SEL noise measurements are useful as they can be converted to obtain L _{eq} sound levels over any period of time and can be used for predicting noise at various locations.
Sound	A fluctuation of air pressure which is propagated as a wave through air.
Sound absorption	The ability of a material to absorb sound energy through its conversion into thermal energy.
Sound level meter	An instrument consisting of a microphone, amplifier and indicating device, having a declared performance and designed to measure sound pressure levels.
Sound pressure level	The level of noise, usually expressed in decibels, as measured by a standard sound level meter with a microphone.
Sound power level	Ten times the logarithm to the base 10 of the ratio of the sound power of the source to the reference sound power.
Tonal noise	Containing a prominent frequency and characterised by a definite pitch.

APPENDIX B Daily train noise levels at nearest receiver

Measurements at 88 Leacocks Lane

Table 5-1 88 Leacocks Lane (Glenfield Farm): Daily number of identified passenger and freight trains on track

Date	Day	Daytime (7am to 10 pm)			Night-time (7am to 10 pm)		
		Passenger	Freight	Total	Passenger	Freight	Total
1/08/2017	Tue	120 ¹	15 ¹	135 ¹	34	10	44
2/08/2017	Wed	172	16	188	33	13	46
3/08/2017	Thur	146 ²	19 ²	165 ²	2 ²	7 ²	9 ²
4/08/2017	Fri	Note 3	21	21	Note 3	6	6
5/08/2017	Sat	Note 3	14	14	Note 3	10	10
6/08/2017	Sun	Note 3	13	13	Note 3	10	10
7/08/2017	Mon	Note 3	17	17	Note 3	11	11
8/08/2017	Tue	Note 3	21	21	Note 3	12	12
9/08/2017	Wed	Note 3	15	15	Note 3	13	13
10/08/2017	Thur	Note 3	21	21	Note 3	18	18
11/08/2017	Fri	Note 3	24	24	Note 3	8	8
12/08/2017	Sat	Note 3	20	20	Note 3	12	12
13/08/2017	Sun	Note 3	2 ¹	2 ¹	Note 3	- ¹	- ¹

Note: 1. Incomplete data set due to start/end time of unattended measurements

2. Incomplete data due to weather events (passbys excluded)

3. Passenger train noise not included in detailed analysis

Table 5-2 88 Leacocks Lane (Glenfield Farm): L_{Aeq} noise levels – at nearest residence – facade reflected

Date	Day	Daytime (7am to 10 pm)			Night-time (7am to 10 pm)			L _{AFmax,95%}		
		L _{Aeq} (15hour)			L _{Aeq} (9hour)					
		Passenger	Freight	Total	Passenger	Freight	Total	Passenger	Freight	Total
1/08/2017	Tue	53.9 ¹	49.4 ¹	55.2 ¹	48.0	49.0	51.5	73.2	78.1	-
2/08/2017	Wed	54.0	50.0	55.5	47.1	48.1	50.6	74.0	74.5	-
3/08/2017	Thur	54.3 ¹	51.3 ¹	56.1 ¹	Weather affected			76.3	79.9	-
4/08/2017	Fri	54.0 ³	50.9	50.9 ³	47.6 ³	48.1	50.9	-	80.3	-
5/08/2017	Sat	Note 4	48.5	-	Note 4	49.8	-	-	77.2	-
6/08/2017	Sun	Note 4	48.5	-	Note 4	50.0	-	-	85.3	-
7/08/2017	Mon	54.0 ³	49.2	45.3	47.6 ³	49.8	51.9	-	75.4	-
8/08/2017	Tue	54.0 ³	54.3	57.2	47.6 ³	51.9	53.2	-	80.4	-
9/08/2017	Wed	54.0 ³	50.1	55.5	47.6 ³	51.4	52.9	-	80.7	-
10/08/2017	Thur	54.0 ³	51.7	56.0	47.6 ³	50.8	52.5	-	83.2	-
11/08/2017	Fri	54.0 ³	52.3	56.3	47.6 ³	48.7	51.2	-	83.7	-
12/08/2017	Sat	Note 4	49.4	-	Note 4	50.8	-	-	73.1	-

Date	Day	Daytime (7am to 10 pm) L _{Aeq} (15hour)			Night-time (7am to 10 pm) L _{Aeq} (9hour)			L _{AFmax,95%}		
		Passenger	Freight	Total	Passenger	Freight	Total	Passenger	Freight	Total
13/08/2017	Sun	Note 4	39.3 ¹	-				-	-	-
Overall		54.0	51.5	56.0	47.6	49.9	51.9	76.3	85.3	-

Note: 1. Due to incomplete data set, calculated noise levels have been normalised to the number of passbys observed on Wed 2/8/2017
 2. Incomplete data due to weather events (passbys excluded)
 3. Passenger train noise level analysis not undertaken for these days and is assumed to be the same as the values measured on Wed 2/8/2017
 4. Passenger train noise analysis not undertaken for Saturday and Sunday but is expected to be lower than the measured noise levels on weekdays
 5. Grey shading indicates excluded data for overall noise calculations

Measurements at 15 Slessor Road

Table 5-3 15 Slessor Road: Daily number of identified passenger and freight trains on track

Date	Day	Daytime (7am to 10 pm)			Night-time (7am to 10 pm)		
		Passenger	Freight	Total	Passenger	Freight	Total
27/11/2018	Tue	183 ¹	23 ¹	206 ¹	47 ²	14 ²	61 ²
28/11/2018	Wed	38 ²	5 ²	43 ²	84	15	99
29/11/2018	Thur	246	32	278	85	19	104
30/11/2018	Fri	231	36	267	81	9	90
1/12/2018	Sat	151	28	179	91	10	101
2/12/2018	Sun	78 ²	5 ²	83 ²	69	18	87
3/12/2018	Mon	228	22	250	86	13	99
4/12/2018	Tue	252	18	270	85	14	99
5/12/2018	Wed	242	21	263	81 ²	14 ²	95 ²
6/12/2018	Thur	247	22	269	79	10	89
7/12/2018	Fri	229	29	258	74	10	84
8/12/2018	Sat	144	19	163	81	11	92
9/12/2018	Sun	154	14	168	85	9	94
10/12/2018	Mon	251	21	272	3 ¹	0 ¹	3 ¹

Note: 1. Incomplete data set due to start/end time of unattended measurements

2. Incomplete data due to weather events (passbys excluded)

Table 5-4 15 Slessor Road: L_{Aeq} noise levels – at nearest residence – facade reflected

Date	Day	Daytime (7am to 10 pm)			Night-time (7am to 10 pm)			L _{AFmax,95%}		
		L _{Aeq(15hour)}			L _{Aeq(9hour)}					
		Passenger	Freight	Total	Passenger	Freight	Total	Passenger	Freight	Total
27/11/2018	Tue	48.7 ¹	51.3 ¹	53.2 ¹	44.1 ²	49.6 ²	50.7 ²	68.8 ^{1,2}	77.0 ^{1,2}	72.8 ^{1,2}
28/11/2018	Wed	42.3 ²	42.4 ²	45.3 ²	47.4	52.8	53.9	69.0 ²	77.6 ²	73.1 ²
29/11/2018	Thur	50.8	53.6	55.5	48.2	52.2	53.7	71.3	80.3	74.6
30/11/2018	Fri	49.2	51.7	53.6	46.8	49.3	51.3	70.6	77.3	73.3
1/12/2018	Sat	47.5	50.4	52.2	46.9	49.3	51.2	68.4	76.0	-
2/12/2018	Sun	43.5 ²	42.1 ²	45.8 ²	46.4	51.0	52.3	70.2 ²	78.0 ²	-
3/12/2018	Mon	48.0	49.5	51.8	47.6	50.5	52.3	69.5	78.9	-
4/12/2018	Tue	50.3	51.1	53.8	47.0	49.9	51.7	71.1	77.9	-
5/12/2018	Wed	50.0	52.0	54.1	46.9 ²	51.3 ²	52.7 ²	69.7 ²	79.8 ²	-
6/12/2018	Thur	50.0	52.6	54.5	47.9	50.7	52.5	70.7	80.4	-
7/12/2018	Fri	50.3	51.1	53.7	46.2	48.6	50.6	71.6	77.4	-
8/12/2018	Sat	47.6	50.6	52.4	47.3	50.5	52.2	69.1	78.7	-
9/12/2018	Sun	47.8	49.0	51.4	47.1	48.5	50.9	68.9	77.3	-
10/12/2018	Mon	49.7	50.3	53.0	-	-	-	69.0 ¹	78.1 ¹	-
Overall		49.9	51.7	53.9	47.4	50.8	52.4	71.6	80.4	-

Note: 1. Incomplete data due to start/end of recording

2. Incomplete data due to weather events (passbys excluded)

3. Grey shading indicates excluded data for overall noise calculations

Measurements at 11 Goodenough Street

Refer Section 4.2

Measurements at 19 Wallcliffe Court

Table 5-5 19 Wallcliffe Court: Daily number of identified passenger and freight trains on track

Date	Day	Daytime (7am to 10 pm)			Night-time (7am to 10 pm)		
		Passenger	Freight	Total	Passenger	Freight	Total
27/11/2018	Tue	107 ¹	- ¹	107 ¹	26 ²	- ²	26 ²
28/11/2018	Wed	22 ²	- ²	22 ²	43	-	43
29/11/2018	Thur	157	-	157	46	-	46
30/11/2018	Fri	158	-	158	49	-	49
1/12/2018	Sat	124	-	124	49	-	49
2/12/2018	Sun	61 ²	- ²	61 ²	39	-	39
3/12/2018	Mon	152	-	152	45	-	45
4/12/2018	Tue	162	-	162	48	-	48
5/12/2018	Wed	162	-	162	46 ²	- ²	46 ²
6/12/2018	Thur	156	-	156	51	-	51
7/12/2018	Fri	162	-	162	48	-	48
8/12/2018	Sat	121	-	121	48	-	48
9/12/2018	Sun	124	-	124	44	-	44
10/12/2018	Mon	158	-	158	- ¹	- ¹	- ¹

Note: 1. Incomplete data set due to start/end time of unattended measurements

2. Incomplete data due to weather events (passbys excluded)

Table 5-6 19 Wallcliffe Court: L_{Aeq} noise levels – at logger location 64 m from rail – facade reflected

Date	Day	Daytime (7am to 10 pm)			Night-time (7am to 10 pm)			L _{Afmax,95%}		
		L _{Aeq(15hour)}			L _{Aeq(9hour)}					
		Passenger	Freight	Total	Passenger	Freight	Total	Passenger	Freight	Total
27/11/2018	Tue	50.0 ¹	-	-	45.6 ²	-	-	74.9 ^{1,2}	-	-
28/11/2018	Wed	45.0 ²	-	-	50.1	-	-	76.4 ²	-	-
29/11/2018	Thur	53.6	-	-	49.5	-	-	76.5	-	-
30/11/2018	Fri	52.5	-	-	49.1	-	-	75.3	-	-
1/12/2018	Sat	50.2	-	-	49.1	-	-	74.6	-	-
2/12/2018	Sun	47.9 ²	-	-	48.9	-	-	75.5 ²	-	-
3/12/2018	Mon	51.9	-	-	50.0	-	-	76.0	-	-
4/12/2018	Tue	52.9	-	-	48.5	-	-	75.7	-	-
5/12/2018	Wed	52.7	-	-	48.4 ²	-	-	75.5 ²	-	-
6/12/2018	Thur	52.0	-	-	50.0	-	-	75.2	-	-
7/12/2018	Fri	51.7	-	-	48.6	-	-	74.9	-	-
8/12/2018	Sat	49.1	-	-	48.6	-	-	74.4	-	-
9/12/2018	Sun	50.0	-	-	48.4	-	-	73.9	-	-
10/12/2018	Mon	52.2	-	-	-	-	-	75.4 ¹	-	-
Overall		52.5	-	-	49.4			76.5		

Note: 1. Incomplete data due to start/end of recording

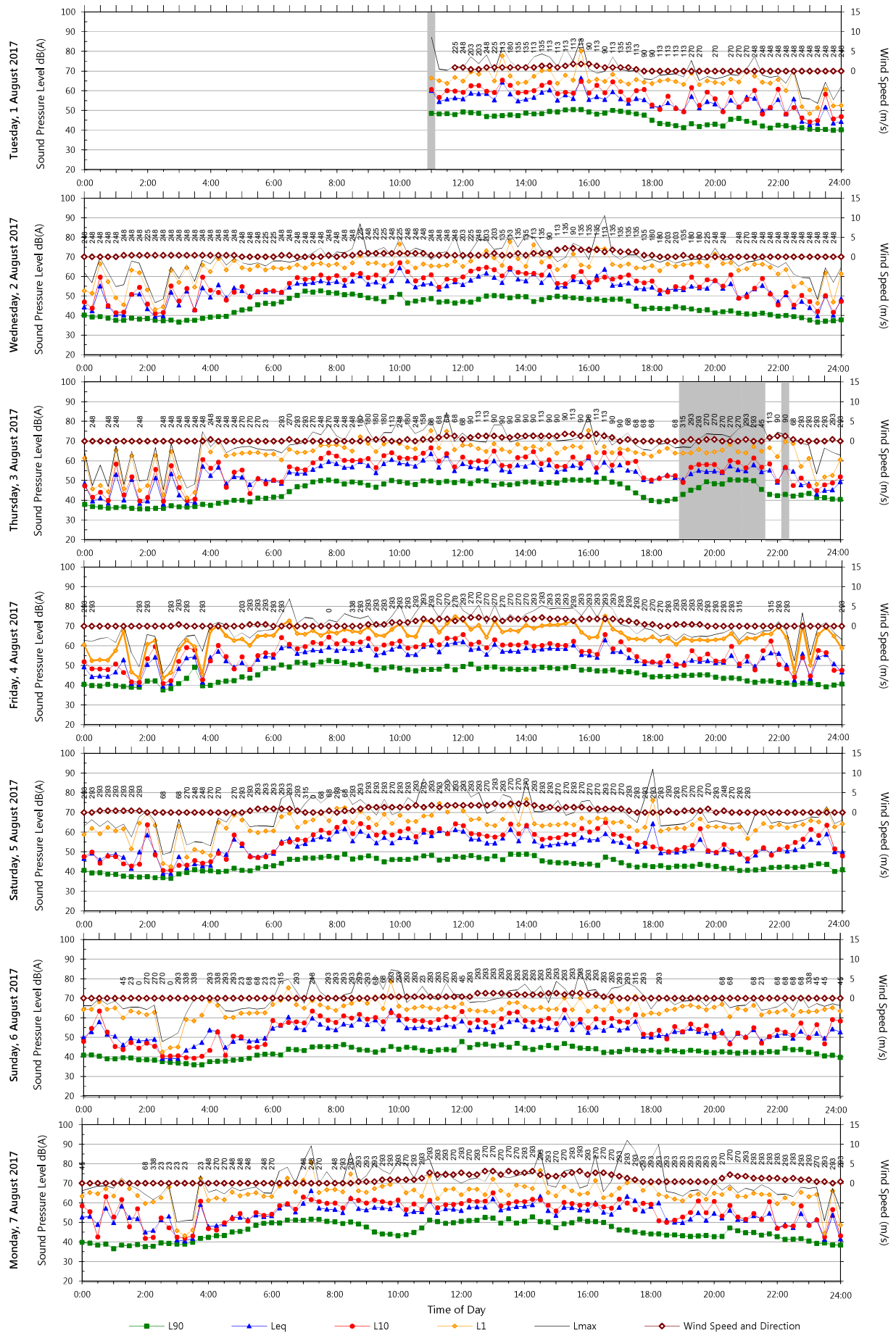
2. Incomplete data due to weather events (passbys excluded)

3. Grey shading indicates excluded data for overall noise calculations

APPENDIX C Long-term 15-minute noise level results

Unattended Monitoring Results

Location: L11 - 88 Leacocks Lane, Casula

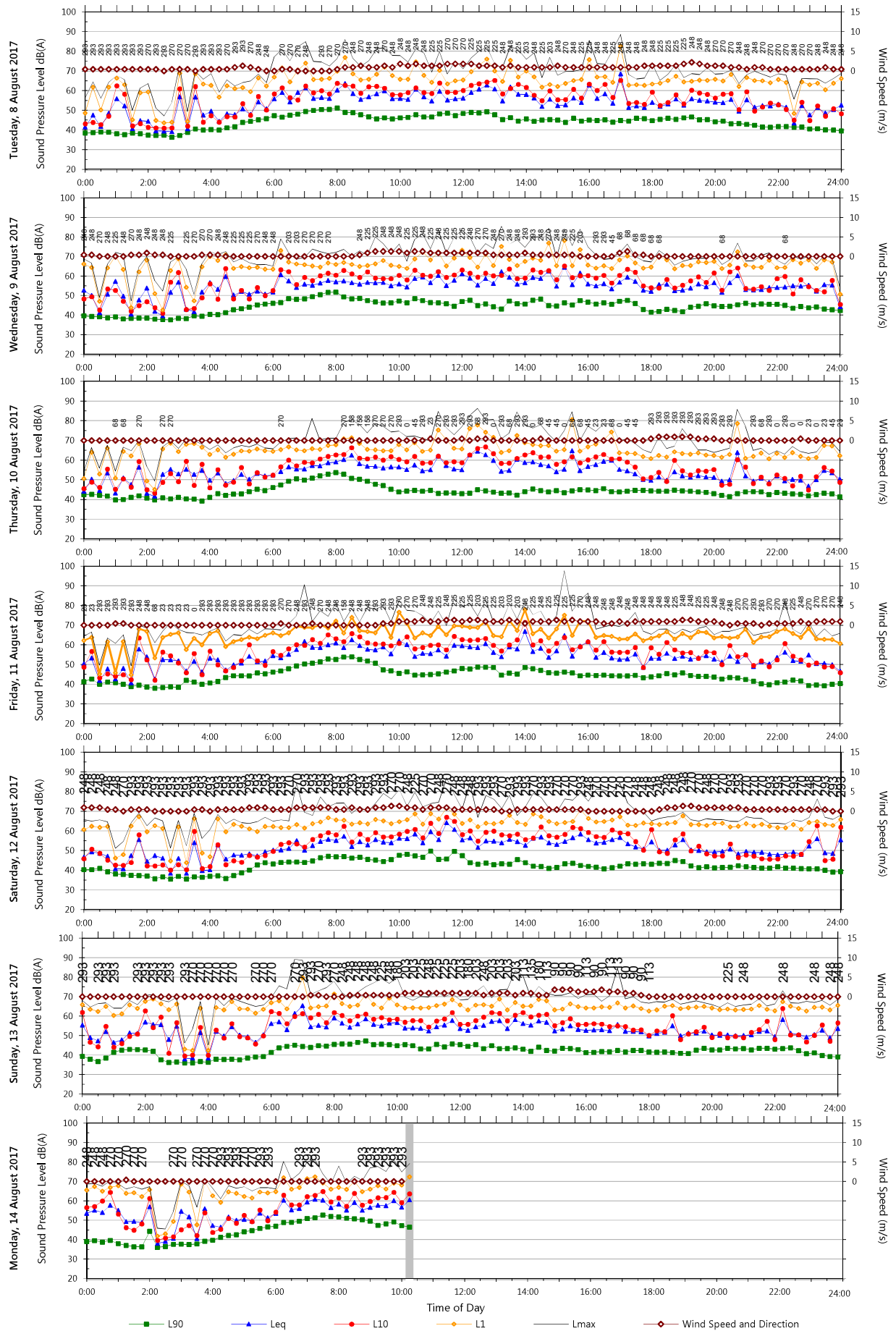


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Template: QTE-26 (rev 16) Logger Graphs Program

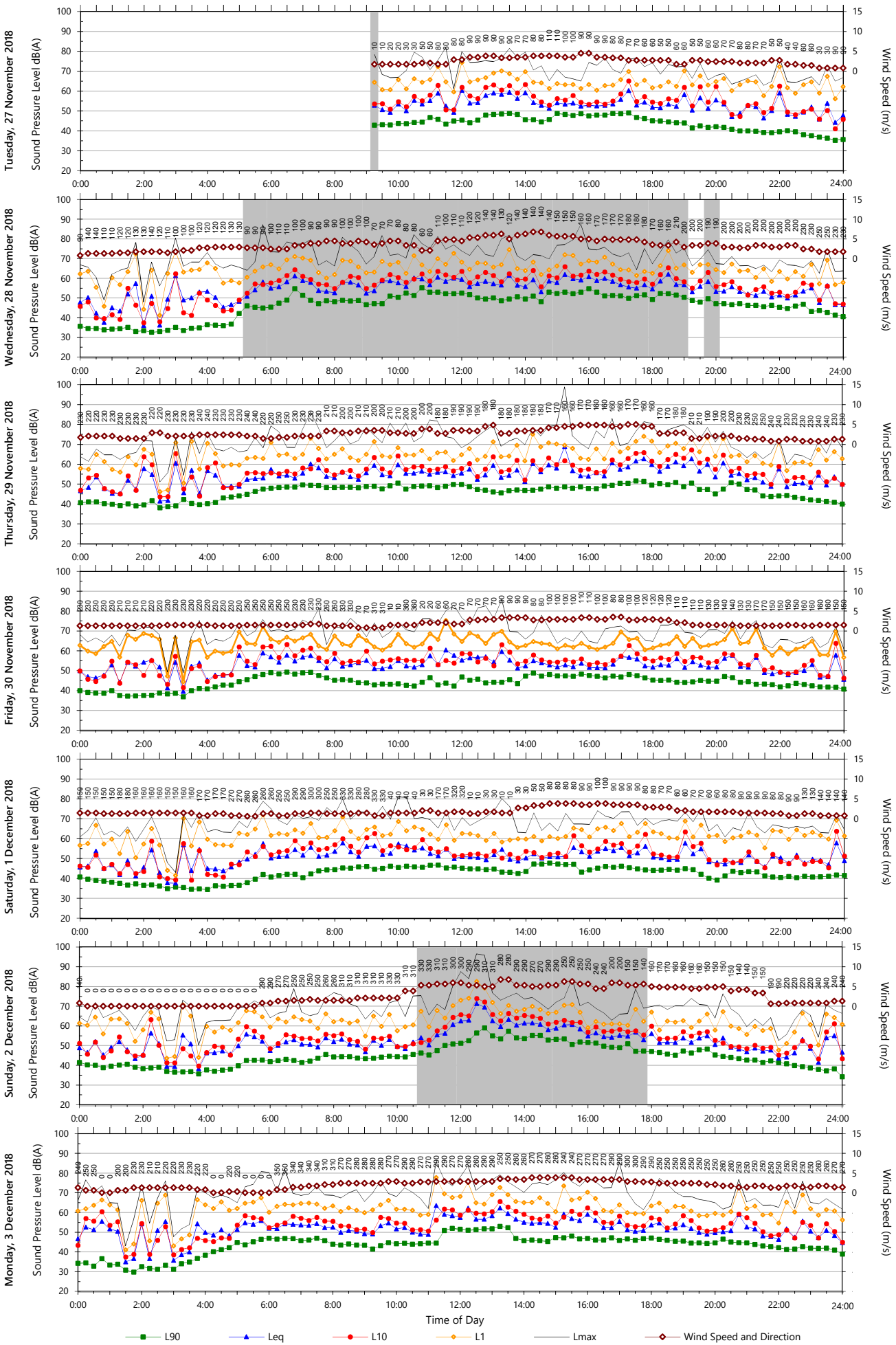
Unattended Monitoring Results

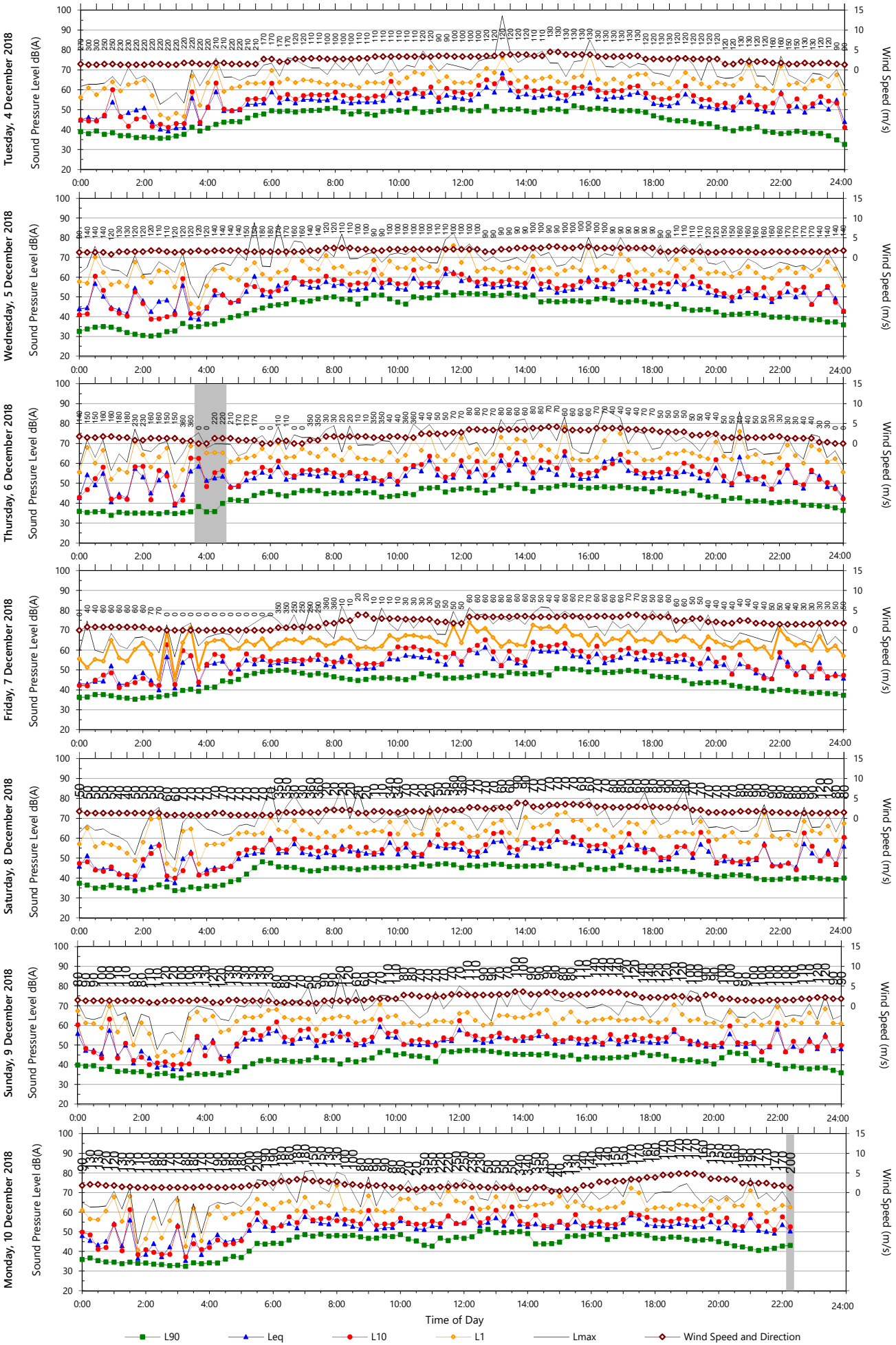
Location: L11 - 88 Leacocks Lane, Casula

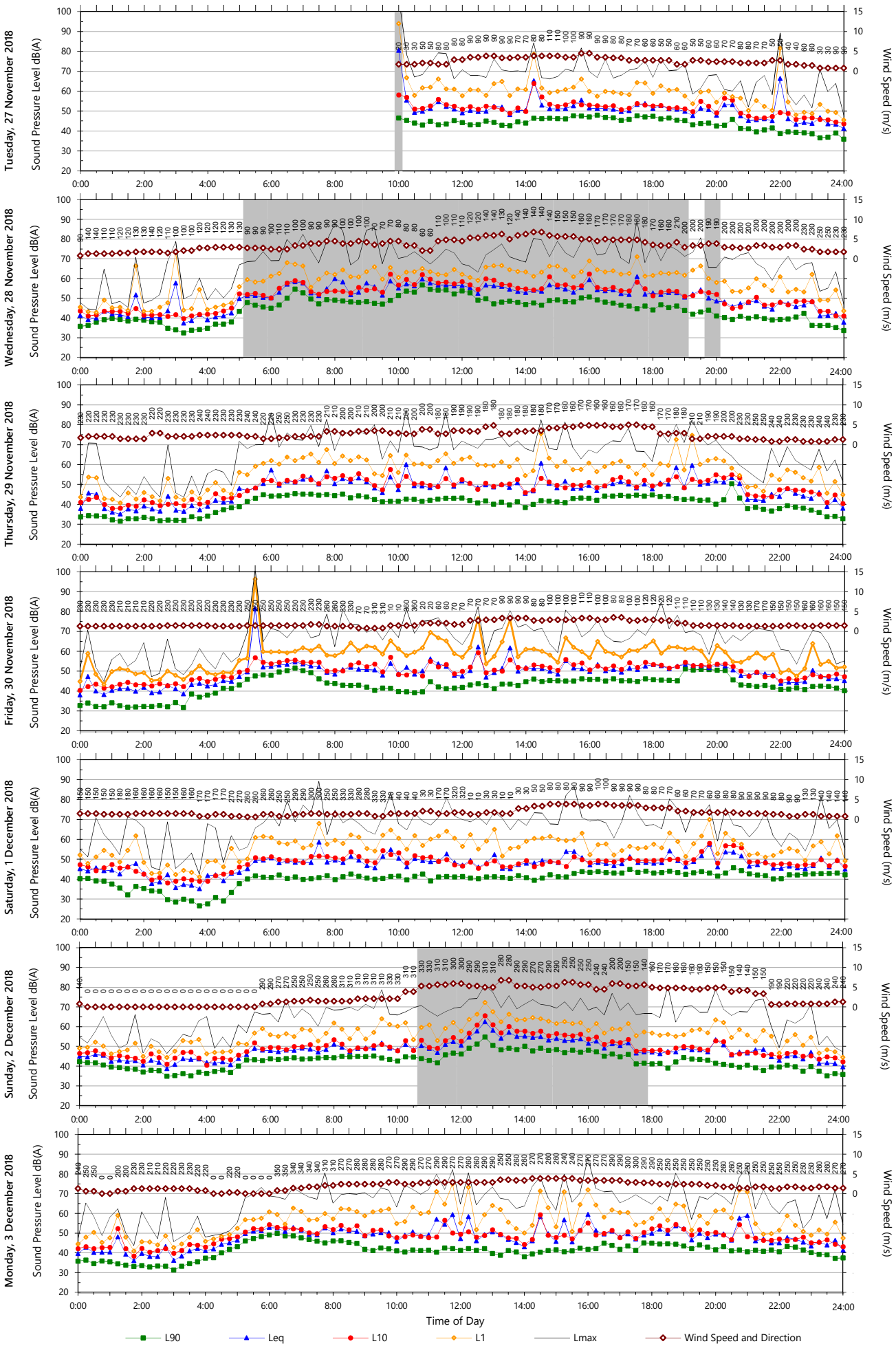


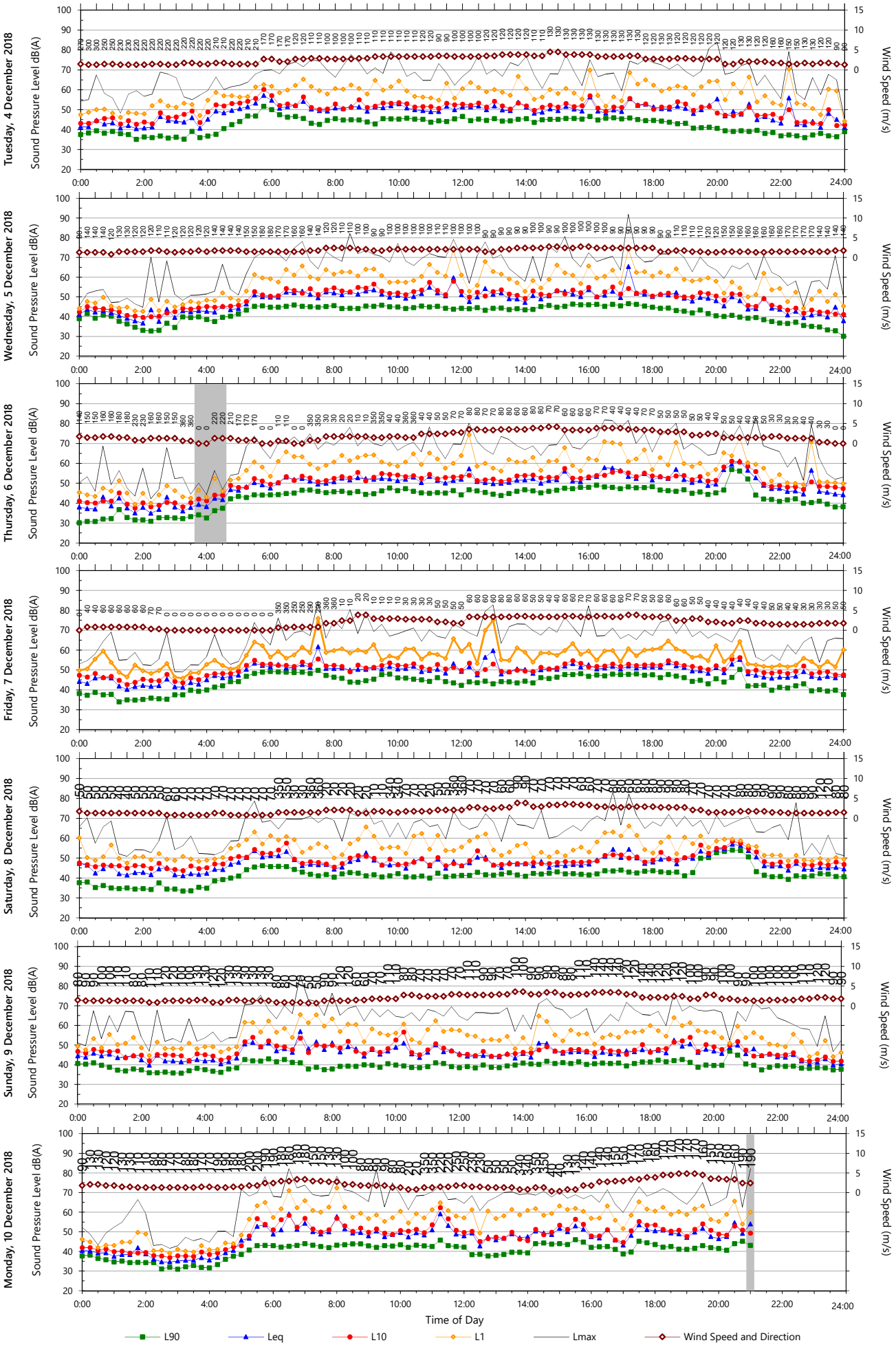
Data File: 2017-08-01_SLM_000_123_Rpt_Report.txt

Template: QTE-26 (rev 16) Logger Graphs Program



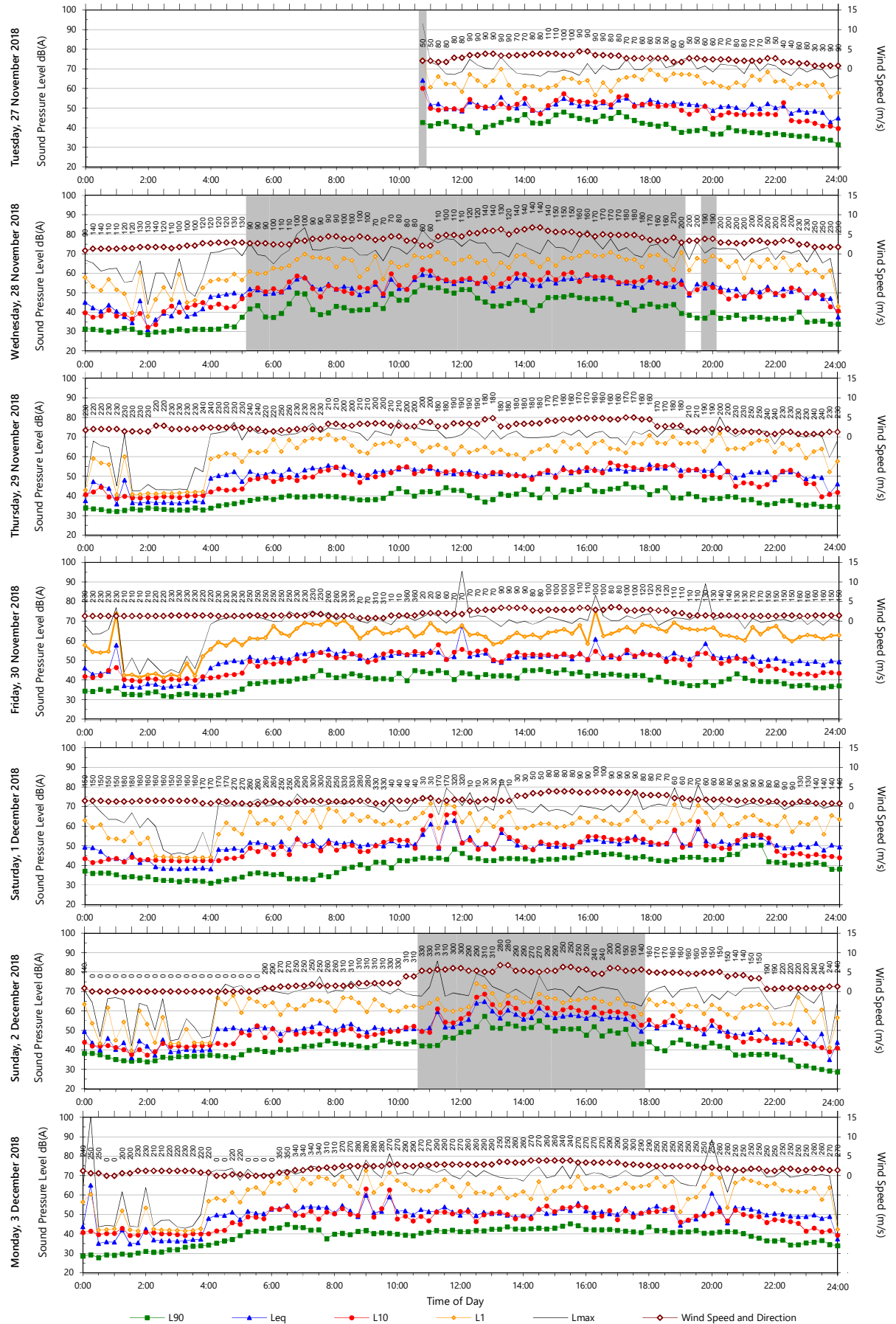






Unattended Monitoring Results

Location: Public area adjacent to 19 Wallcliffe Court, Wattle Grove

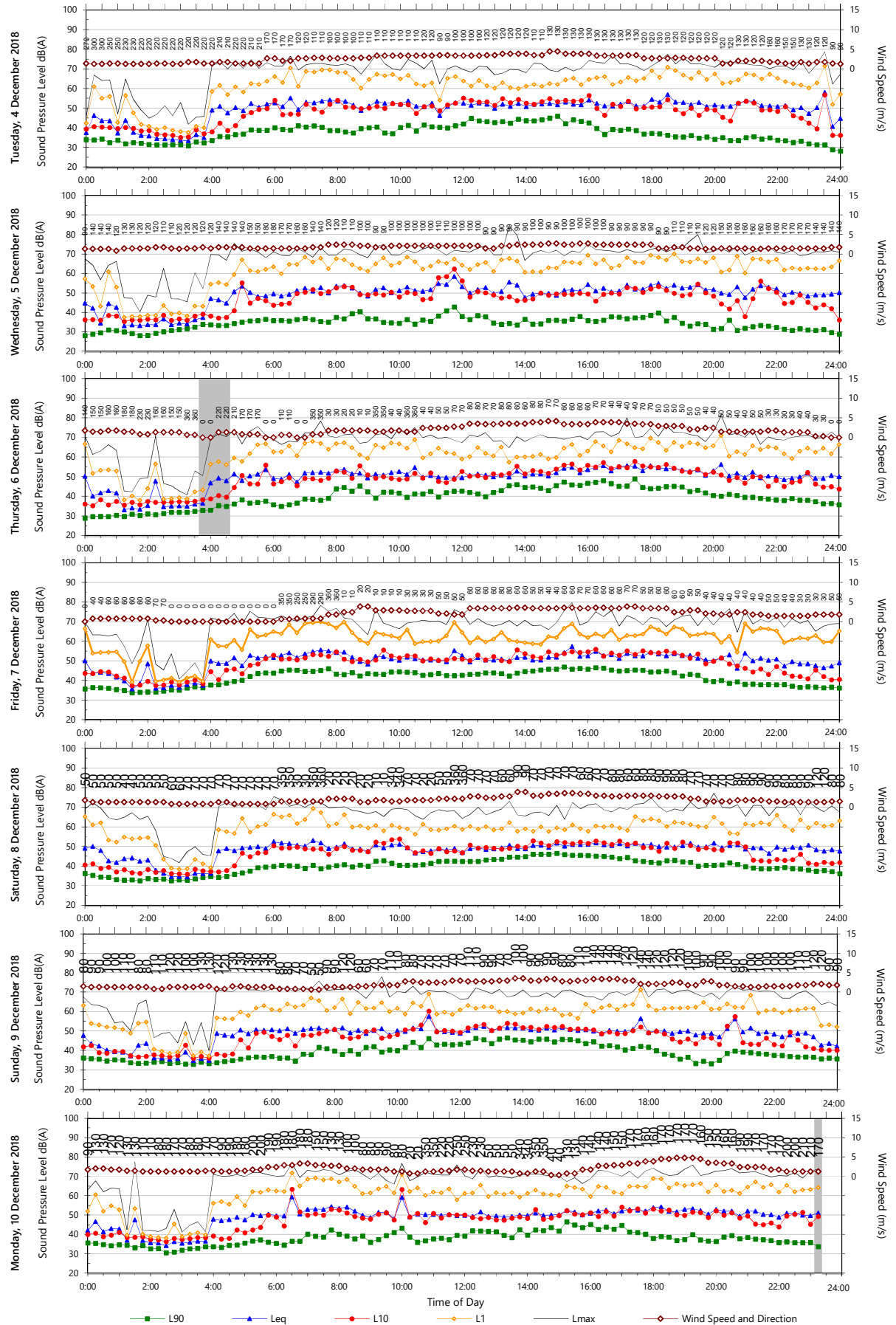


Data File: 2018-11-27_SLM_001_123_Rpt_Report.txt

Template: QTE-26 (rev 23) Logger Graphs Program

Unattended Monitoring Results

Location: Public area adjacent to 19 Wallcliffe Court, Wattle Grove



Data File: 2018-11-27_SLM_001_123_Rpt_Report.txt

Template: QTE-26 (rev 23) Logger Graphs Program

APPENDIX D Distance Attenuation – 19 Wallcliffe Court

Attended measurements were conducted at three positions for the purposes of determining the rate at which noise levels reduce with increasing distance from the East Hills Line.

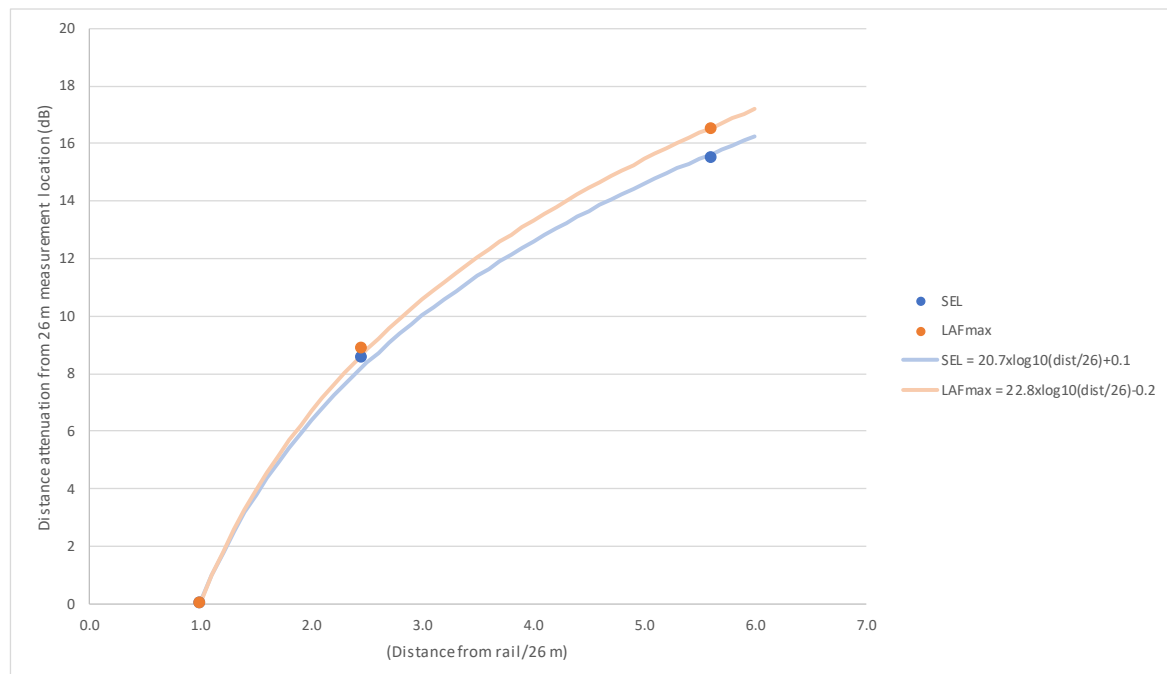
In the area near 19 Wallcliffe Court, attended measurements were conducted at three locations with increasing distance from the rail (see Figure 2-9) to determine the rate at which noise levels reduce with increasing distance from the East Hills Line.

The attended measurements were conducted on 10 December between 23:20 and 00:15 during 5 representative train passbys. A summary of the logarithmic average SEL noise levels and average L_{AFmax} noise levels is provided in Figure 5-1.

Table 5-7 19 Wallcliffe Court – Distance attenuation measurement results

Distance from Rail	Logarithmic average SEL noise level, dB(A)	SEL noise level reduction compared with near location, dB(A)	Average L_{AFmax} Noise Level, dB(A)	L_{Amax} noise level reduction compared with near location, dB(A)
26 m	82.3	0	74.7	0
64 m	73.8	8.6	65.9	8.9
146 m	66.8	15.5	58.2	16.5

Figure 5-1 19 Wallcliffe Court – Distance attenuation measurement results



B.13 Rail Noise Levels at Glenfield Farm (2020)

Renzo Tonin & Associates Report TL116-05F05 Rail Link Noise Monitoring (r1)

MOOREBANK INTERMODAL TERMINAL PROJECT

Rail Link Noise Monitoring per Approval Condition G7B of SSD 6766

15 September 2020

Tactical Group

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Attention:	

Document control

Date	Revision history	Non-issued revision	Issued revision	Prepared	Instructed	Reviewed / Authorised
19.08.2020	First Issue	0	1			

Important Disclaimers:

The work presented in this document was carried out in accordance with the Renzo Tonin & Associates Quality Assurance System, which is based on Australian/New Zealand Standard AS/NZS ISO 9001.

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We have derived data in this report from information sourced from the Client (if any) and/or available in the public domain at the time or times outlined in this report. The passage of time, manifestation of latent conditions or impacts of future events may require further examination and re-evaluation of the data, findings, observations and conclusions expressed in this report.

We have prepared this report in accordance with the usual care and thoroughness of the consulting profession, for the sole purpose described above and by reference to applicable standards, guidelines, procedures and practices at the date of issue of this report. For the reasons outlined above, however, no other warranty or guarantee, whether expressed or implied, is made as to the data, observations and findings expressed in this report, to the extent permitted by law.

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1 Introduction

The Moorebank Intermodal Terminal involves the development of intermodal freight terminal facilities at Moorebank in south-west Sydney, linked by rail to Port Botany and the interstate rail network. The Project includes a new rail link, connecting the Intermodal Terminal to the Southern Sydney Freight Line (SSFL).

This report has been prepared to determine if current noise levels from train movements on the new rail link comply with noise limit in State Significant Development (SSD) Approval SSD 6766. The requirements of condition G7B are copied verbatim below.

G7B. The Applicant shall:

(a) not less than three months and not more than twelve months from commencement of operation, engage an appropriately qualified and experienced acoustic engineer to undertake a night-time noise survey at Glenfield Farm (or an equivalent location if access is denied).

(b) the noise survey shall be conducted in accordance with the EPA's Rail Infrastructure Noise Guideline 2013 to determine:

(i) the contribution of any new rail traffic travelling to and from the development; and,

(ii) the increase in the total rail traffic noise level caused by any new rail traffic to and from the development.

(c) the noise survey shall be conducted for not less than 12 contiguous days in the winter months (July, August or September). [Note that this should be June, July and August]

(d) if as a result of the noise survey there is a sustained increase in the total rail traffic noise level due to the noise level from rail traffic travelling to and from the development of more than 2dB(A) for more than 30% of nights surveyed, the Applicant shall:

within twelve months, construct a noise barrier along the relevant sections of rail link in accordance with the specifications provided by an appropriately qualified and experienced acoustic engineer so as to limit the increase in the total rail traffic noise level at Glenfield Farm caused by any new rail traffic to and from the development to not exceed 2dB(A).

(e) the report of the noise survey including the results and recommendations shall be provided to the Secretary.

The existing level of rail traffic noise prior to construction of the new rail link is documented in Renzo Tonin & Associates Report TJ741-04F03 (*Moorebank Intermodal Terminal Project - Measurement of Existing Levels of Rail Noise (2018) per Condition 3C*, dated 16 July 2019).

Renzo Tonin & Associates is a member firm of the Association of Australian Acoustical Consultants (AAAC). The work documented in this report was carried out in accordance with the Renzo Tonin & Associates Quality Assurance System, which is based on Australian Standard / NZS ISO 9001.

Appendix A contains a glossary of acoustic terms used in this report.

2 Timing of night-time noise survey

Approval Condition G7B requires that the timing of the noise measurements to be performed:

- not less than three months from the commencement of operations;
- not more than twelve months from the commencement of operations;
- for not less than 12 contiguous days in the winter months

The commencement of rail operations on the new rail link occurred in November 2019 (spring). Noise compliance measurement are therefore required to be performed in winter 2020.

Noise monitoring was performed over 22 contiguous days between 13 August and 4 September 2020 in accordance with the above requirements. Due to the small number of train movements on the rail link during night-time periods, the monitoring was extended beyond the minimum requirement, including four days in spring.

3 Noise monitoring locations

Approval Condition G7B requires night-time measurements to be performed at Glenfield Farm (or an equivalent location if access is denied).

Permission was sought from the resident of the Glenfield Farm to perform the required noise monitoring in accordance with Approval Condition G7B. As permission was denied, an equivalent location in the publicly accessible area immediately north of the Glenfield Farm was selected. The alternative location has an equivalent noise exposure to the rail link and is positioned at the same distance from the nearest track.

The location of the Glenfield Farm and equivalent noise measurement location in relation to the new rail link is provided in Figure 1. A picture of the attended measurement location is provided in Figure 2.

At the alternative measurement location, there was no secure location to perform unattended noise measurements over a contiguous noise monitoring period of two or more weeks. In lieu of performing unattended noise monitoring, the following approach was adopted:

- Attended noise measurements were performed at the equivalent noise monitoring location during night-time periods when QUBE advised that a freight train movement on the new rail link was proposed to occur (to or from the Intermodal Terminal).
- Contiguous unattended noise measurements were performed at a position adjacent to the new rail link between 13 August and 4 September 2020 to capture all passby events. The noise monitoring data at this location can be referred to in the event that freight train movements occur outside the advised schedule and are not captured by the attended measurements.

The unattended noise measurements adjacent the new rail link were performed at two locations. The measurements at Unattended Location 1 were performed between 13 and 28 August. The unattended noise logger was moved to an alternative position (Unattended Location 2) between 28 August and 4 September, to determine if there was any change in the source noise characteristics. The unattended noise measurement positions are shown in Figure 1.

Figure 1 Glenfield Farm, equivalent noise measurement location and Intermodal Terminal rail link

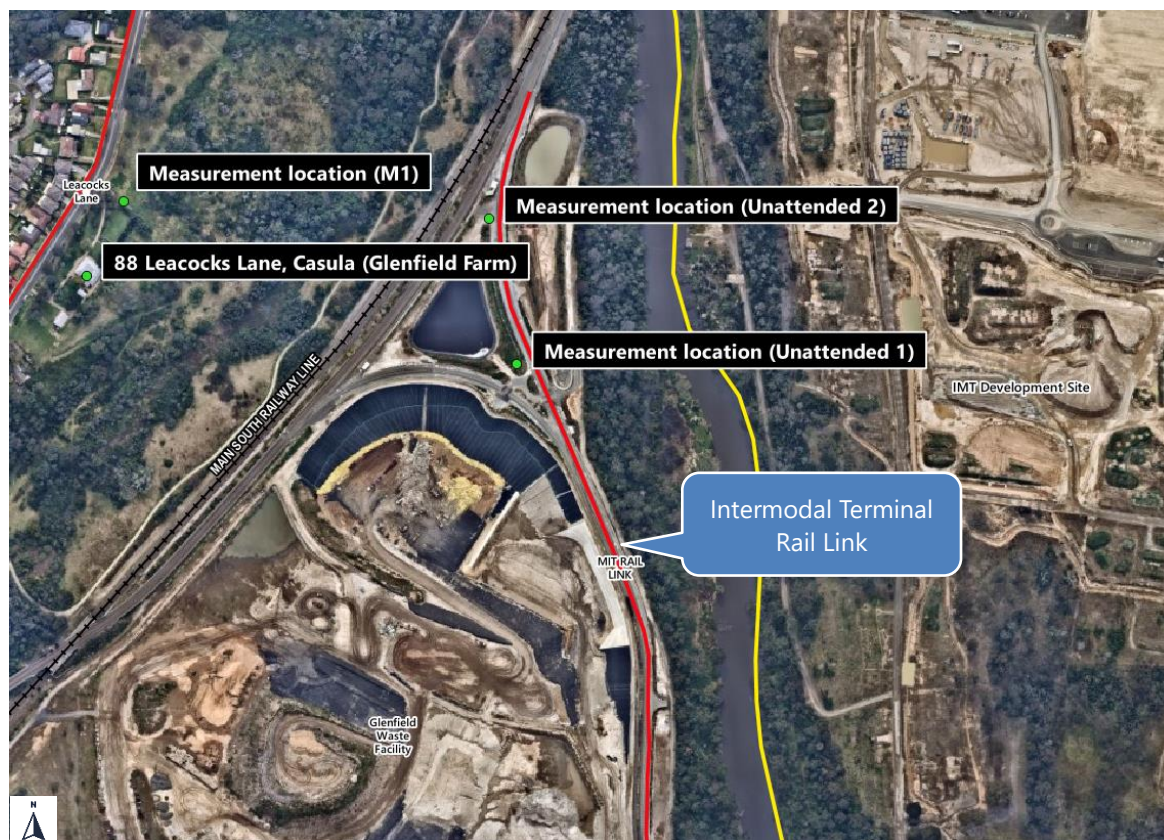


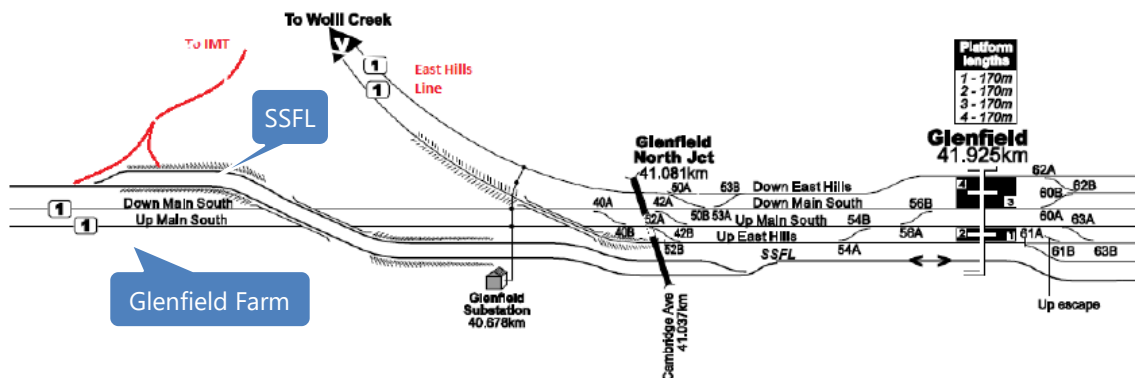
Figure 2 Measurement location adjacent Glenfield Farm



4 Summary of rail movements

A rail network schematic is provided in Figure 3 and illustrates the approximate location of Glenfield Farm in relation to the Intermodal Terminal rail link, the existing Southern Sydney Freight Line (SSFL), the Main South Line and the East Hills Line.

Figure 3 Rail network schematic



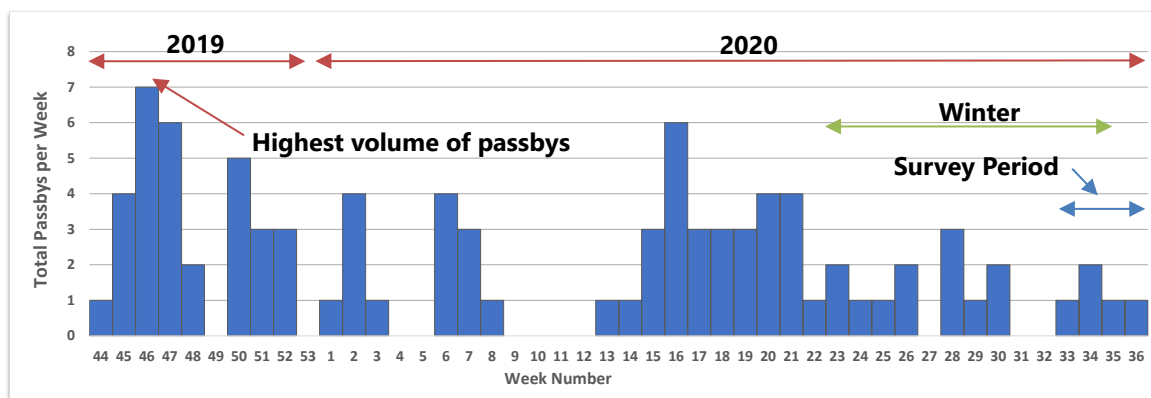
The East Hills Line is an electric passenger train only line. The Main South Line includes electric passenger trains, diesel passenger trains and diesel freight trains. The SSFL includes diesel freight trains only. These existing lines carry frequent rail traffic during the daytime and night-time periods.

The Intermodal Terminal rail link includes diesel freight trains only, operating to and from the Intermodal Terminal. The commencement of rail operations occurred in November 2019 and includes movements during the daytime (7am to 10pm) and night-time (10pm to 7am) periods. A summary of the number of night-time train movements per week on the new rail link, between November 2019 and September 2020, is shown in Figure 4. These movements have been derived from the permanent rail noise monitoring system results. The following observations are noted:

- The highest number of night-time passbys per week since the commencement of operations was seven. This occurred during week 46 of 2019 (week ending Sunday 3 November)
- The average number of night-time passbys since the commencement of operations was two per week
- There are eleven weeks where no night-time rail movements occurred to or from the Intermodal Terminal
- During the 22 day survey period in this report, there was a total of five train movements to or from the Intermodal Terminal. This corresponds to an average of less than two train movements per week and is representative of the average number of train movements during the winter period.

Approval Condition G7B requires the construction of a noise barrier if there is a sustained increase in total rail traffic noise levels greater than 2 dB(A) for more than 30% of nights surveyed. This equates to a noise increase greater than 2 dB(A) for two or more nights per week.

Figure 4 Summary of weekly night-time train passbys on new Intermodal Terminal rail link



5 Measurement methodology

Approval Condition G7B requires the noise survey to be conducted in accordance with the EPA's *Rail Infrastructure Noise Guideline* (RING, 2013) to determine the noise contribution from new rail traffic travelling to and from the Intermodal Terminal, and the total increase in rail traffic noise.

The measurement methodology in the following sections is consistent with the requirements in Section 3.4 (measuring existing levels of rail noise and vibration), of the RING.

5.1 Details of noise survey and measurement equipment

The equipment used for noise measurements comprised NTi Audio Type XL2 precision sound level analysers, which are class 1 instruments having an accuracy suitable for field and laboratory use. All instruments were calibrated prior to and subsequent to each measurement using a Bruel & Kjaer Type 4231 calibrator. No significant drift in calibration was observed.

All instrumentation complies with IEC 61672 (parts 1-3) '*Electroacoustics - Sound Level Meters*' and IEC 60942 '*Electroacoustics - Sound calibrators*' and carry current NATA certification (or if less than 2 years old, manufacturers certification). For all measurements, the microphone was positioned at a height of 1.5 m above ground level.

A summary of the equipment used in the noise surveys is provided in Table 1.

Table 1 Summary of monitoring equipment

Instrument	Make	Model	Serial Number	Last Calibrated
Sound level meter / analyser	NTi	XL2	A2A-07815-E0	09 Nov 2018
			A2A-08520-E0	14 Mar 2019
			A2A-02386-D2	08 July 2019
			A2A-13529-E0	20 Dec 2019
Field Calibrator	Bruel & Kjaer	Type 4231	3017534	30 June 2020
			1821397	7 Aug 2020
			2677710	16 Mar 2020

5.2 Measurement parameters and data analysis

For the attended measurement, the sound level meter was set up to measure the L_{AFmax} and single event sound exposure level (SEL) noise levels for each train passby.

The time period of train passbys measurements was determined using the procedure described in Section 6.6.3 of International Standard ISO3095:2013, whereby the measurement commences when the noise level is at least 10 dB lower than when the front of the train is opposite the microphone and

concludes when the noise level is at least 10 dB lower than when the end of the train is opposite the microphone.

The procedure in Clause 3.4.1.1 of the RING was used, together with the number of train passbys during night-time periods to calculate the $L_{Aeq(9hour)}$ night-time noise levels from train passbys on the new rail link.

For the unattended noise measurements adjacent the new rail link, the sound level meter was set up to record the L_{AFmax} and SEL noise levels in consecutive 1-second intervals. The measurement results were post-processed to identify train passby events on the new rail link and to determine the L_{AFmax} and SEL noise levels for each night-time train passby. The near-field noise measurement results were normalised to a reference measurement distance of 15 m.

6 Summary of existing rail noise levels

Approval Condition G7B requires the construction of a noise barrier if there is a sustained increase in total rail traffic noise levels greater than 2 dB(A). This increase is based on the total rail noise levels in the absence of the new rail link.

The existing level of rail noise at the Glenfield Farm is documented in Renzo Tonin & Associates Report TJ741-04F03 (*Moorebank Intermodal Terminal Project - Measurement of Existing Levels of Rail Noise (2018) per Condition 3C*, dated 16 July 2019). This is based on measurements performed over a 2-week period in August 2017. A summary of the measurement results is provided in Table 2.

Table 2 Summary of existing passenger and freight train noise levels at Glenfield Farm (2017) - facade reflected

Date	Night-time (7am to 10 pm) $L_{Aeq(9hour)}$, dB(A)			$L_{AFmax,95\%}$, dB(A)		
	Passenger	Freight	Total	Passenger	Freight	Total
1/08/2017	48.0	49.0	51.5	73.2	78.1	-
2/08/2017	47.1	48.1	50.6	74.0	74.5	-
3/08/2017	Weather affected			76.3	79.9	-
4/08/2017	47.6 ¹	48.1	50.9	-	80.3	-
5/08/2017	Note 2	49.8	-	-	77.2	-
6/08/2017	Note 2	50.0	-	-	85.3	-
7/08/2017	47.6 ¹	49.8	51.9	-	75.4	-
8/08/2017	47.6 ¹	51.9	53.2	-	80.4	-
9/08/2017	47.6 ¹	51.4	52.9	-	80.7	-
10/08/2017	47.6 ¹	50.8	52.5	-	83.2	-
11/08/2017	47.6 ¹	48.7	51.2	-	83.7	-
12/08/2017	Note 2	50.8	-	-	73.1	-
Overall	47.6	49.9	51.9	76.3	85.3	-

Note: 1. Passenger train noise level analysis not undertaken for these days and is assumed to be the same as the values measured on Wed 2/8/2017

2. Passenger train noise analysis not undertaken for Saturday and Sunday but is expected to be lower than the measured noise levels on weekdays

3. Grey shading indicates excluded data for overall noise calculations

4. All noise levels are facade corrected

The results in the above table indicate that the overall $L_{Aeq(9hour)}$ noise levels from existing passenger and freight train passbys is 52 dB(A). The $L_{AFmax,95\%}$ noise level from existing freight trains is 85 dB(A).

7 Intermodal Terminal rail link noise levels

7.1 Noise levels adjacent Glenfield Farm

During the 22 day measurement period between 13 August and 4 September 2020, there were five freight train movements to or from the Intermodal Terminal. For three of these passby events, attended noise measurements were performed at the measurement location adjacent Glenfield Farm.

A summary of the noise measurement results is provided in Table 3.

Table 3 Summary of Intermodal Terminal freight train noise levels adjacent Glenfield Farm (2020) - facade reflected

Date / time	Measured SEL noise level, dB(A)	Night-time (7am to 10 pm) $L_{Aeq(9hour)}$, dB(A)	Measured $L_{AFmax,95\%}$, dB(A)
	Intermodal Terminal Freight	Intermodal Terminal Freight	Intermodal Terminal Freight
15/08/2020 1:40 am	81	36	69
17/08/2020 06:42 am	Train not captured as arrived early		
22/08/2020 02:05 am	74	29	63
27/08/2020 02:10 am	Train not captured as arrived two hours late		
04/09/2020 04:33 am	73	28	63

Note: 1. All noise levels are facade corrected

The results in the above table show that the measured $L_{Aeq(9hour)}$ noise levels were between 28-36 dB(A) for the three train passby events measured, compared with an existing $L_{Aeq(9hour)}$ noise level of 52 dB(A). For current operations, the maximum increase in rail noise levels during the night-time period is calculated to be 0.1 dB(A), compared with the 2 dB(A) allowance in Approval Condition G7B.

For noise levels to increase by 2 dB(A) or more at the Glenfield Farm noise monitoring position, an SEL noise level of 95 dB(A) is required (assuming one train per night). The maximum measured SEL of 81 dB(A) is 14 dB(A) below this requirement.

The results in the above table show that the measured L_{AFmax} noise levels were between 63-69 dB(A) for the three train passby events measured. It can be seen that L_{AFmax} noise levels from train passbys on the new rail link are well below the existing L_{AFmax} noise levels in Table 2.

7.2 Noise levels adjacent new rail link (15 m)

A summary of the noise measurement results adjacent the new rail link, normalised to a reference measurement distance of 15 m is provided in Table 4.

Table 4 Summary of near-field Intermodal Terminal freight train noise levels – reference distance of 15 m

Date / time	Measured SEL noise level, dB(A)	Measured L _{AFmax,95%} , dB(A)
	Intermodal Terminal Freight	Intermodal Terminal Freight
15/08/2020 1:40 am	94	87
17/08/2020 06:42 am	95	93
22/08/2020 02:05 am	100	93
27/08/2020 02:10 am	86	82
04/09/2020 04:33 am	95	92

The measurement results in the above table show that the passby noise levels for the freight trains on 17/08/2020 and 27/08/2020, which were not captured at the measurement location adjacent Glenfield Farm, are consistent with the remaining noise measurement results. On this basis, it is concluded that the two train passbys that were not captured at the measurement location adjacent Glenfield Farm are likely to have similar measurement results to the other three train passbys that were captured.

8 Conclusion

This report has been prepared to determine if current noise levels from train movements on the new rail link comply with noise limit in State Significant Development (SSD) Approval SSD 6766. Specifically, noise measurements have been performed at a location adjacent the Glenfield Farm to determine if the overall noise increase from train passbys on the Moorebank Intermodal Terminal Rail Link are generating a sustained noise level increase of more than 2 dB(A).

Noise monitoring was performed over 22 contiguous days between 13 August and 4 September 2020. During this period, a total of five freight trains travelled on the new rail link to or from the Intermodal Terminal.

The measured $L_{Aeq(9\text{hour})}$ noise levels during the 10pm to 7am night-time period varied between 28-36 dB(A), compared with a total rail noise level of 52 dB(A) from existing train operations.

For current operations on the Moorebank Intermodal Terminal Rail Link, the maximum increase in overall rail noise levels was 0.1 dB(A) compared with the 2 dB(A) allowance in Approval Condition G7B. The maximum SEL passby noise level on the new rail link was 14 dB(A) lower than the required level to generate an overall noise increase of 2 dB(A) or more.

On this basis, the measured noise levels comply with the requirements in the Approval Condition and the construction of a noise barrier along relevant sections of rail link is not required.

APPENDIX A Glossary of terminology

The following is a brief description of the technical terms used to describe noise to assist in understanding the technical issues presented.

Adverse weather	Weather effects that enhance noise (that is, wind and temperature inversions) that occur at a site for a significant period of time (that is, wind occurring more than 30% of the time in any assessment period in any season and/or temperature inversions occurring more than 30% of the nights in winter).																																								
Ambient noise	The all-encompassing noise associated within a given environment at a given time, usually composed of sound from all sources near and far.																																								
Assessment period	The period in a day over which assessments are made.																																								
Assessment Point	A point at which noise measurements are taken or estimated. A point at which noise measurements are taken or estimated.																																								
Background noise	Background noise is the term used to describe the underlying level of noise present in the ambient noise, measured in the absence of the noise under investigation, when extraneous noise is removed. It is described as the average of the minimum noise levels measured on a sound level meter and is measured statistically as the A-weighted noise level exceeded for ninety percent of a sample period. This is represented as the L90 noise level (see below).																																								
Decibel [dB]	The units that sound is measured in. The following are examples of the decibel readings of common sounds in our daytime environment: <table><tr><td rowspan="2">threshold of hearing</td><td>0 dB</td><td>The faintest sound we can hear</td></tr><tr><td>10 dB</td><td>Human breathing</td></tr><tr><td rowspan="2">almost silent</td><td>20 dB</td><td></td></tr><tr><td>30 dB</td><td>Quiet bedroom or in a quiet national park location</td></tr><tr><td rowspan="2">generally quiet</td><td>40 dB</td><td>Library</td></tr><tr><td>50 dB</td><td>Typical office space or ambience in the city at night</td></tr><tr><td rowspan="2">moderately loud</td><td>60 dB</td><td>CBD mall at lunch time</td></tr><tr><td>70 dB</td><td>The sound of a car passing on the street</td></tr><tr><td rowspan="2">loud</td><td>80 dB</td><td>Loud music played at home</td></tr><tr><td>90 dB</td><td>The sound of a truck passing on the street</td></tr><tr><td rowspan="2">very loud</td><td>100 dB</td><td>Indoor rock band concert</td></tr><tr><td>110 dB</td><td>Operating a chainsaw or jackhammer</td></tr><tr><td rowspan="2">extremely loud</td><td>120 dB</td><td>Jet plane take-off at 100m away</td></tr><tr><td>130 dB</td><td></td></tr><tr><td>threshold of pain</td><td>140 dB</td><td>Military jet take-off at 25m away</td></tr></table>			threshold of hearing	0 dB	The faintest sound we can hear	10 dB	Human breathing	almost silent	20 dB		30 dB	Quiet bedroom or in a quiet national park location	generally quiet	40 dB	Library	50 dB	Typical office space or ambience in the city at night	moderately loud	60 dB	CBD mall at lunch time	70 dB	The sound of a car passing on the street	loud	80 dB	Loud music played at home	90 dB	The sound of a truck passing on the street	very loud	100 dB	Indoor rock band concert	110 dB	Operating a chainsaw or jackhammer	extremely loud	120 dB	Jet plane take-off at 100m away	130 dB		threshold of pain	140 dB	Military jet take-off at 25m away
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dB(A)	A-weighted decibels. The A- weighting noise filter simulates the response of the human ear at relatively low levels, where the ear is not as effective in hearing low frequency sounds as it is in hearing high frequency sounds. That is, low frequency sounds of the same dB level are not heard as loud as high frequency sounds. The sound level meter replicates the human response of the ear by using an electronic filter which is called the “A” filter. A sound level measured with this filter switched on is denoted as dB(A). Practically all noise is measured using the A filter.																																								
dB(C)	C-weighted decibels. The C-weighting noise filter simulates the response of the human ear at relatively high levels, where the human ear is nearly equally effective at hearing from mid-low frequency (63Hz) to mid-high frequency (4kHz), but is less effective outside these frequencies.																																								

Frequency	Frequency is synonymous to pitch. Sounds have a pitch which is peculiar to the nature of the sound generator. For example, the sound of a tiny bell has a high pitch and the sound of a bass drum has a low pitch. Frequency or pitch can be measured on a scale in units of Hertz or Hz.
Impulsive noise	Having a high peak of short duration or a sequence of such peaks. A sequence of impulses in rapid succession is termed repetitive impulsive noise.
Intermittent noise	The level suddenly drops to that of the background noise several times during the period of observation. The time during which the noise remains at levels different from that of the ambient is one second or more.
L _{Max}	The maximum sound pressure level measured over a given period.
L _{Min}	The minimum sound pressure level measured over a given period.
L ₁	The sound pressure level that is exceeded for 1% of the time for which the given sound is measured.
L ₁₀	The sound pressure level that is exceeded for 10% of the time for which the given sound is measured.
L ₉₀	The level of noise exceeded for 90% of the time. The bottom 10% of the sample is the L90 noise level expressed in units of dB(A).
L _{eq}	The "equivalent noise level" is the summation of noise events and integrated over a selected period of time.
Reflection	Sound wave changed in direction of propagation due to a solid object obscuring its path.
SEL	Single Event Sound Exposure Level (SEL) is the constant sound level which, if maintained for a period of 1 second would have the same acoustic energy as the measured noise event. SEL noise measurements are useful as they can be converted to obtain L _{eq} sound levels over any period of time and can be used for predicting noise at various locations.
Sound	A fluctuation of air pressure which is propagated as a wave through air.
Sound absorption	The ability of a material to absorb sound energy through its conversion into thermal energy.
Sound level meter	An instrument consisting of a microphone, amplifier and indicating device, having a declared performance and designed to measure sound pressure levels.
Sound pressure level	The level of noise, usually expressed in decibels, as measured by a standard sound level meter with a microphone.
Sound power level	Ten times the logarithm to the base 10 of the ratio of the sound power of the source to the reference sound power.
Tonal noise	Containing a prominent frequency and characterised by a definite pitch.

B.14 Curve Noise Monitoring Report

Renzo Tonin Report TL116-02F02 Curve noise monitoring report (r1)

MOOREBANK INTERMODAL TERMINAL RAIL LINK

Curve Noise Monitoring Report

6 March 2020

Tactical

TL116-02F02 Curve noise monitoring report (r1).docx

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The work presented in this document was carried out in accordance with the Renzo Tonin & Associates Quality Assurance System, which is based on Australian Standard / NZS ISO 9001.

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We have prepared this report in accordance with the usual care and thoroughness of the consulting profession, for the sole purpose described above and by reference to applicable standards, guidelines, procedures and practices at the date of issue of this report. For the reasons outlined above, however, no other warranty or guarantee, whether expressed or implied, is made as to the data, observations and findings expressed in this report, to the extent permitted by law.

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Supplementary professional advice should be sought in respect of these issues.

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1 Introduction

Renzo Tonin & Associates was engaged by Tactical to monitor rail noise levels on curves along the Moorebank Intermodal Terminal rail link. Noise levels from freight train passbys were monitored at six curve locations between 27 September 2019 and 16 December 2019.

Two rail friction modifier systems were installed on the rail link on 22 November 2019. The noise monitoring results were analysed to quantify the overall rail noise levels and squealing noise events that occurred during the passbys. 13 passbys were analysed for the period before installation of the rail friction modifier systems and a further 16 passbys were analysed afterwards. The results before and after the installation of the friction modifiers have been compared to quantify the effectiveness of the systems.

A description of technical acoustic terms used within this report is provided in Appendix A.

The work documented in this report was carried out in accordance with the Renzo Tonin & Associates Quality Assurance System, which is based on Australian Standard / NZS ISO 9001. Appendix A contains a glossary of acoustic terms used in this report.

2 Methodology

Continuous unattended noise monitoring was performed at the six curves along the Moorebank Intermodal Terminal (MIMT) Rail Link. The designation of each curve along the rail link is presented in Figure 1. Details of the measurement equipment are provided in Table 1 with the location of the noise logger at each curve shown in APPENDIX B. All locations selected had an unobstructed view of the rail line and no significant reflective objects nearby.

2.1 Monitoring locations and equipment

Figure 1 Curves along the Intermodal Terminal Rail Link

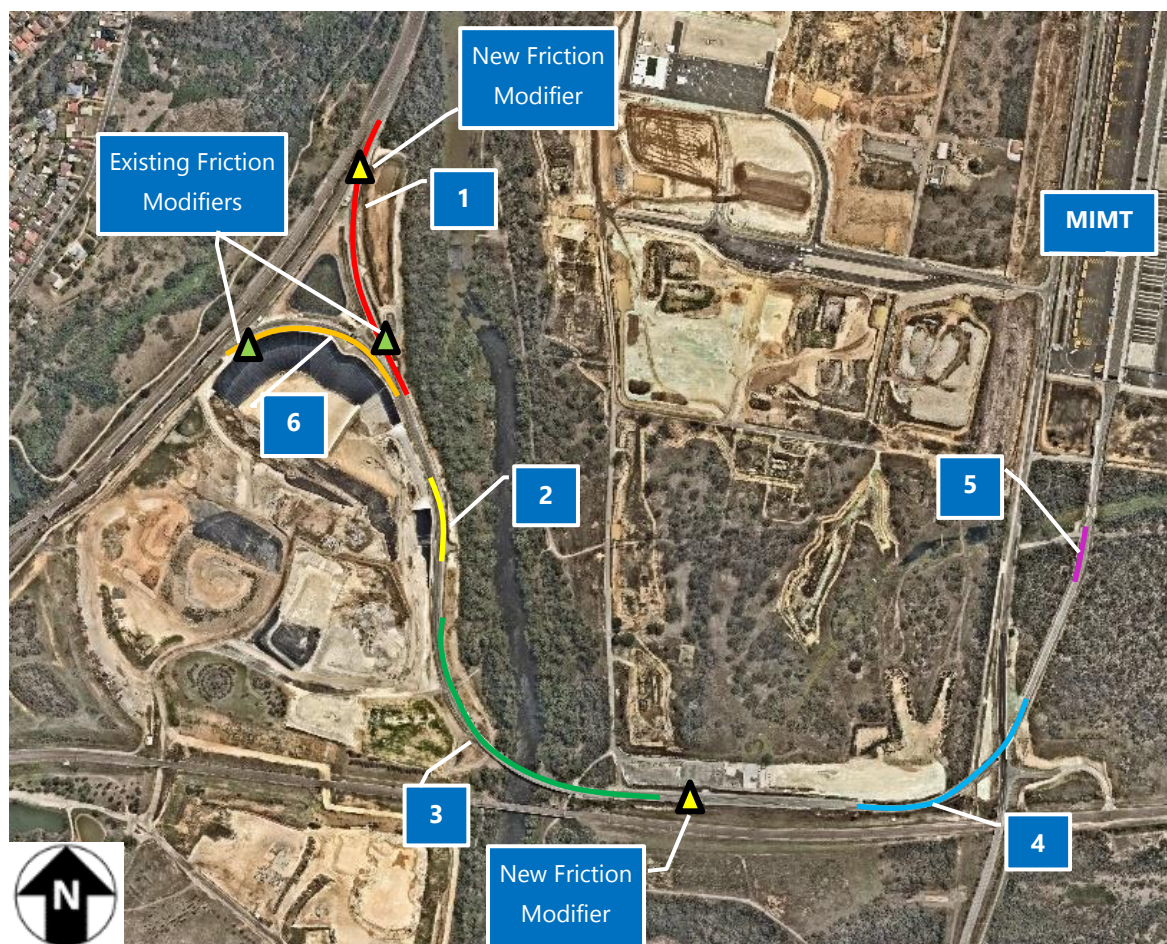


Table 1 Measurement equipment

Location	Curve radius (m)	Curve length (m)	Chainage	Distance to near track centreline (m)	Noise logger	Serial number	Last calibrated
Curve 1	275	214	39.580 km	8.2	NTi XL2	RTA07-021	20/12/2019
Curve 2	260	56	40.390 km	3.1	NTi XL2	RTA07-018	01/05/2019
Curve 3	245	280	40.345 km	7.4	NTi XL2	RTA07-020	14/12/2017
Curve 4	200	243	41.470 km	8.0	NTi XL2	RTA07-017	15/02/2019

Location	Curve radius (m)	Curve length (m)	Chainage	Distance to near track centreline (m)	Noise logger	Serial number	Last calibrated
Curve 5	200	52	41.870 km	3.3	NTi XL2	RTA07-008	14/03/2019
Curve 6	160	297	40.087 km	5.7	NTi XL2	RTA07-022	20/12/2019

The noise loggers used were NTi XL2 precision sound level analysers which are Class 1 instruments having accuracy suitable for field and laboratory use. The noise loggers were calibrated prior and subsequent to the measurements using a Brüel & Kjær Type 4231 calibrator. No significant drift in calibration was observed. All instrumentation complies with IEC 61672 (parts 1–3) '*Electroacoustics - Sound Level Meters*' and IEC 60942 '*Electroacoustics - Sound calibrators*' and carry current NATA certification (or if less than 2 years old, manufacturers certification).

2.2 Friction modifiers

Two existing friction modifiers were in operation for the duration of monitoring, positioned on the MIMT North Track at Chainage 39.840 km on the MIMT South Track at Chainage 39.580 km (shown as green triangles in Figure 1). Lubrication was manually applied to both rails along Curve 4 on 13 September 2019. Two new friction modifiers were installed on 23 November 2019 on the MIMT North track at Chainage 39.611 km and 41.000 km, both on the Up rail (shown as yellow triangles in Figure 1). One of the installed friction modifiers is shown in Figure 2.

Figure 2 Existing friction modifier installed on Curve 1



2.3 Weather observations

Weather conditions during each train passby were based on measurement data from the nearest Bureau of Meteorology weather station at Holsworthy Military Airfield. Passbys during any periods impacted by excessive wind (> 18 km/h) or heavy rain were checked to determine if weather events contributed to noise levels during the passby. For all passbys it was found that weather events did not adversely affect the passby noise results.

2.4 Measurement parameters and analysis

The XL2 noise loggers were set up to measure the L_{Aeq} , $L_{Amax,fast}$ and L_{AE} noise levels in consecutive 0.1 second intervals throughout the measurement period. The loggers also recorded noise levels in one-third octave centre frequency bands between 10 Hz and 20 kHz.

Train passbys were identified manually using the NTi Data Explorer software and verified with the passbys recorded from the temporary G7a passby noise monitoring results. Train passbys affected by other extraneous noise sources and safety devices such as horns were excluded from the results.

In accordance with the requirements of International Standard ISO 3095:2013 *Acoustics - Railway applications - Measurement of noise emitted by railbound vehicles*, measurements were commenced as the train noise rose above the ambient level and concluded when the train noise returned to the ambient level.

All passbys were processed using the NTi Data Explorer software to manually identify the following types of noise events:

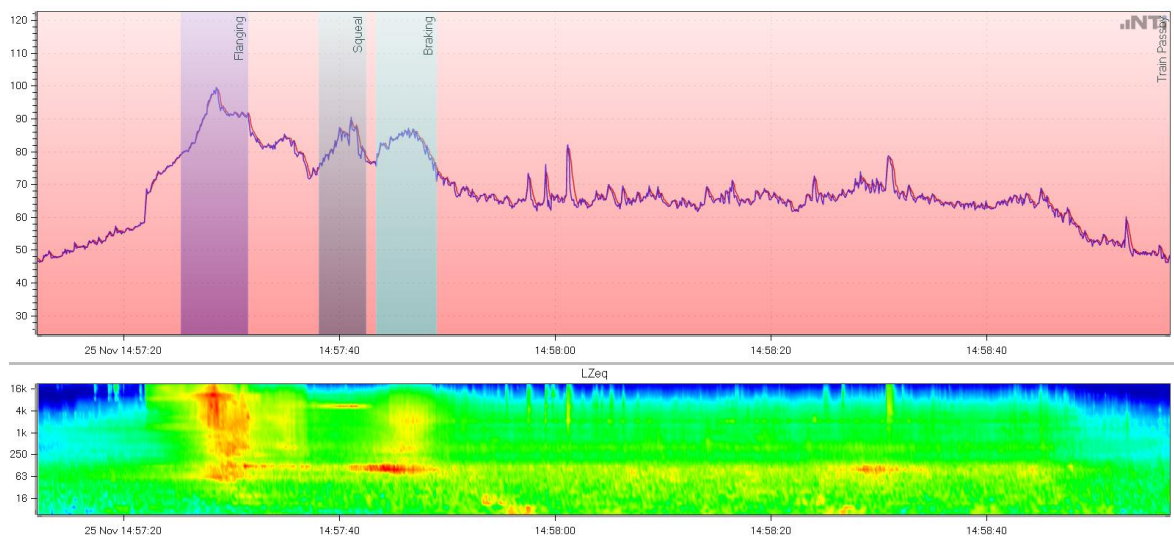
- Squealing - high frequency tonal noise events due to wheel squeal on curved sections
- Flanging – mid to high frequency noise events due to wheel flange and rail gauge face contact
- Braking – low frequency noise events due to the rubbing of brake components

An example of a passby marked up with squealing, flanging and braking events is shown in Figure 3.

Due to an absence of passbys, this report does not include noise measurement results for Curve 6.

Analysis of the noise measurement data was performed in accordance with ISO 3095 *Measurement of noise emitted by railbound vehicles* and the NSW EPA *Rail Infrastructure Noise Guideline* (RING). The measured noise levels were normalised to a reference distance of 15 m.

Figure 3 Example of a passby and associated events analysed using NTI Data Explorer Software



3 Results

3.1 Rail noise levels

Using the NTI Data Explorer software, the maximum A-weighted sound pressure level (L_{AFmax}) and the A-weighted sound exposure level (L_{AE}) were obtained for each passby. Using this data, the $L_{AFmax,95\%}$, and average L_{AE} levels for all passbys were calculated, normalised to a reference distance of 15 m. The results for each curve monitoring location are presented in Table 2.

Both the $L_{AFmax,95\%}$, and L_{AE} noise levels were slightly higher on Curves 1, 3 and 4. These are longer curves, compared to Curves 2 and 5, which are short.

Table 2 Overall passby noise levels at 15m reference distance – all passbys

Curve	Average passby L_{AE} dB(A)	Passby $L_{AFmax,95\%}$ dB(A)
1	102	104
2	101	101
3	103	106
4	105	104
5	102	101

The $L_{AFmax,95\%}$, and average L_{AE} noise levels for squealing, flanging and braking events were calculated, normalised to a reference distance of 15 m. The percentage of passbys that experienced at least one of these types of events was calculated. The results for each curve monitoring location are presented in Table 3.

The noise levels and occurrence of flanging events were highest, followed by squealing events and then braking.

Table 3 Overall passby noise levels at 15m reference distance and percentage of passbys affected by squealing, flanging and braking events

Curve	Squealing event dB(A)			Flanging event dB(A)			Braking event dB(A)		
	L_{AE}	$L_{AFmax,95\%}$	% of passbys	L_{AE}	$L_{AFmax,95\%}$	% of passbys	L_{AE}	$L_{AFmax,95\%}$	% of passbys
1	95	98	31%	100	103	50%	90	85	4%
2	98	99	17%	100	101	48%	92	89	14%
3	97	100	38%	100	102	73%	88	85	12%
4	99	100	45%	102	103	66%	-	-	0%
5	94	93	38%	101	101	48%	80	71	7%

Curve 4, which is the longest curve, had the highest noise levels and occurrence of wheel squeal. In contrast Curve 2 has the lowest occurrence of wheel squeal and Curve 5 had the lowest noise levels. Flanging noise levels were consistent for all curve monitoring locations and featured in least half of all passbys. Brake noise was caused by outbound trains on Curve 3 and inbound trains on Curves 2 and 5.

Detailed results for each passby and noise event are presented in APPENDIX C.

3.2 Effect of friction modifiers

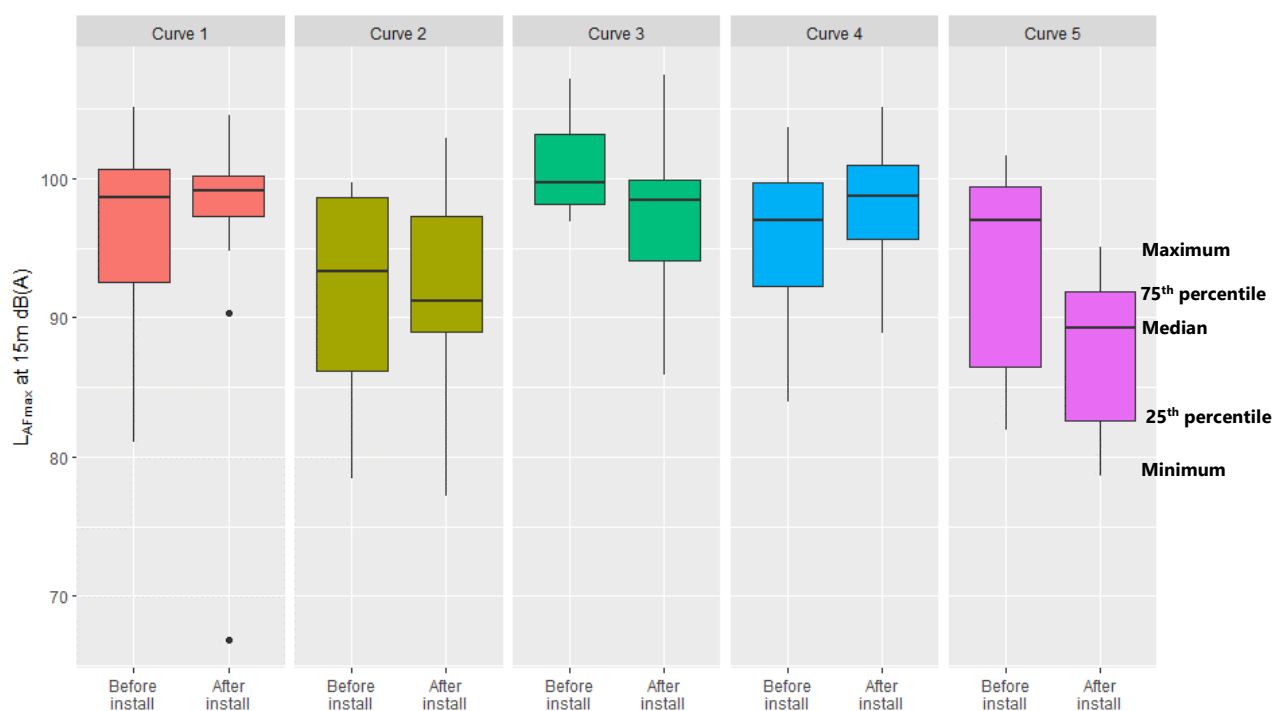
The noise levels at each curve were compared before and after the installation of two new friction modifiers. The distance normalised L_{AE} and L_{AFmax} levels are presented in Table 4 and the statistical distribution of the L_{AFmax} levels is shown in Figure 4.

The results do not show a significant reduction in noise levels after the implementation of the new friction modifiers. The change in median noise levels before and after installation was generally within 2 dB. Similarly, the noise levels and occurrence of wheel squeal events did not significantly reduce after the installation of the friction modifiers.

Table 4 Passby noise levels at 15m reference distance before and after installation of new friction modifiers on Curve 1 and between Curves 3 and 4

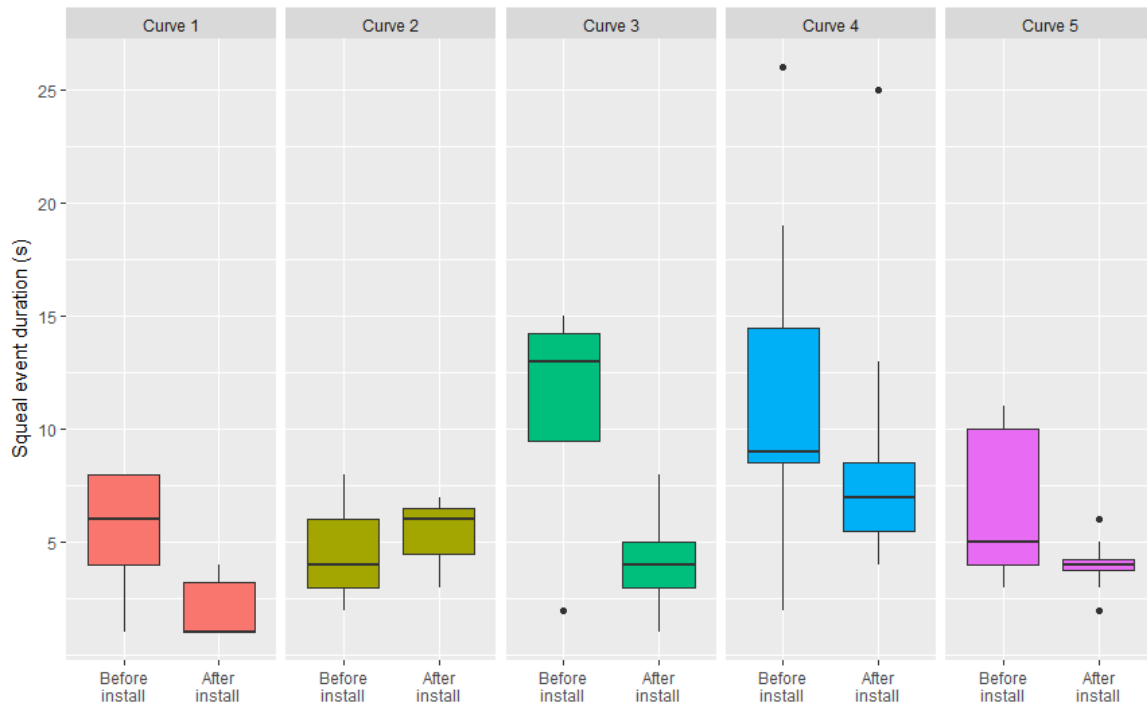
Curve	Median passby L_{AE} dB(A)		Median passby L_{AFmax} dB(A)	
	Before installation	After installation	Before installation	After installation
1	100	102	99	99
2	100	99	93	91
3	104	102	100	98
4	104	104	97	99
5	105	97	97	89

Figure 4 Overall L_{AFmax} passby noise levels at 15m reference distance before and after the installation of new friction modifiers on Curve 1 and between Curves 3 and 4



The duration of squealing events was found to be reduced after installation of the friction modifiers. The duration of squealing events was reduced at all locations except Curve 2 (which experienced the lowest rate of wheel squealing before and after installation).

Figure 5 Duration of wheel squeal noise events before and after the installation of new friction modifiers on Curve 1 and between Curves 3 and 4



4 Discussions

There was no significant difference in the rail noise levels at the five monitored curves and all measured noise levels were within a range of ± 5 dB.

The results demonstrate that wheel squeal is not a dominant source of noise on the curves of the MIMT Rail Link. The measured noise levels and rate of occurrence of squealing events shows that squealing noise did not contribute significantly to the overall L_{Aeq} and L_{AFmax} noise levels. Rail passby noise levels were controlled by wagon wheel-rail noise, locomotive noise and flanging noise. Between 48% and 73% of passbys experienced flanging noise and in many cases, flanging noise controlled the overall L_{AFmax} noise levels. Flanging noise was particularly evident on the locomotives, leading to high L_{AFmax} noise levels that included both flanging and engine noise.

Of the 29 passbys analysed, there was only one passby that experienced wheel squeal with a L_{AFmax} noise level greater than 120 dB(A) at 1.2 m from the near track (TfNSW's criteria for a "severe squeal event"¹).

The occurrence and severity of flanging and squealing events was slightly higher on Curves 1, 3 and 4 which are greater than 250 m long, compared to Curves 2 and 5 which are less than 100 m long.

There was no significant reduction in the overall rail noise levels after the installation of two new friction modifiers. A significant reduction in overall passby noise levels would not be expected as the dominant noise sources are wagon wheel-rail noise and locomotive noise, which are unaffected by the application of a friction modifier.

Squealing or flanging noise did not reduce after the installation of the new friction modifiers. However, the duration of squealing events was reduced at four of the five monitoring locations after the installation of two new friction modifiers. Note that the noise levels of wheel squeal events were already relatively low prior to the installation of the new systems. The friction modifiers may have been ineffective in reducing the noise levels and occurrence of wheel squeal and flanging because the lubricant was not being adequately spread along the rail and/or the systems were only applying the lubricant to one rail of the track.

No clear relationship was found between the measured noise levels or occurrence of squealing and weather conditions or time of day.

¹ Jiang J., Hanson D. & Dowell B., Wheel Squeal: Insights from Wayside Condition Monitoring, TfNSW, IWRN 12

5 Conclusion

This report presents the results of unattended noise monitoring conducted adjacent to the six curves on the Moorebank Intermodal Terminal rail link. Noise monitoring results from freight train passbys entering and leaving the terminal were analysed to quantify the overall noise levels and occurrences of wheel squeal, flanging and braking. The overall rail noise and squeal events were compared before and after the installation of two rail friction modifier systems to evaluate the effectiveness of the systems.

Wheel squeal did not contribute significantly to the overall passby noise levels and only one passby experienced severe squealing. Rail passby noise levels are controlled by wagon wheel-rail noise, locomotive noise and flanging noise.

The results of the unattended monitoring indicate that there is little variation in overall rail noise levels or squealing noise levels with the installation of the friction modifier systems. The new systems may have been effective in reducing the duration of squealing events.

APPENDIX A Glossary of terminology

The following provides a brief description of the technical terms used within this report to assist in understanding the technical issues presented.

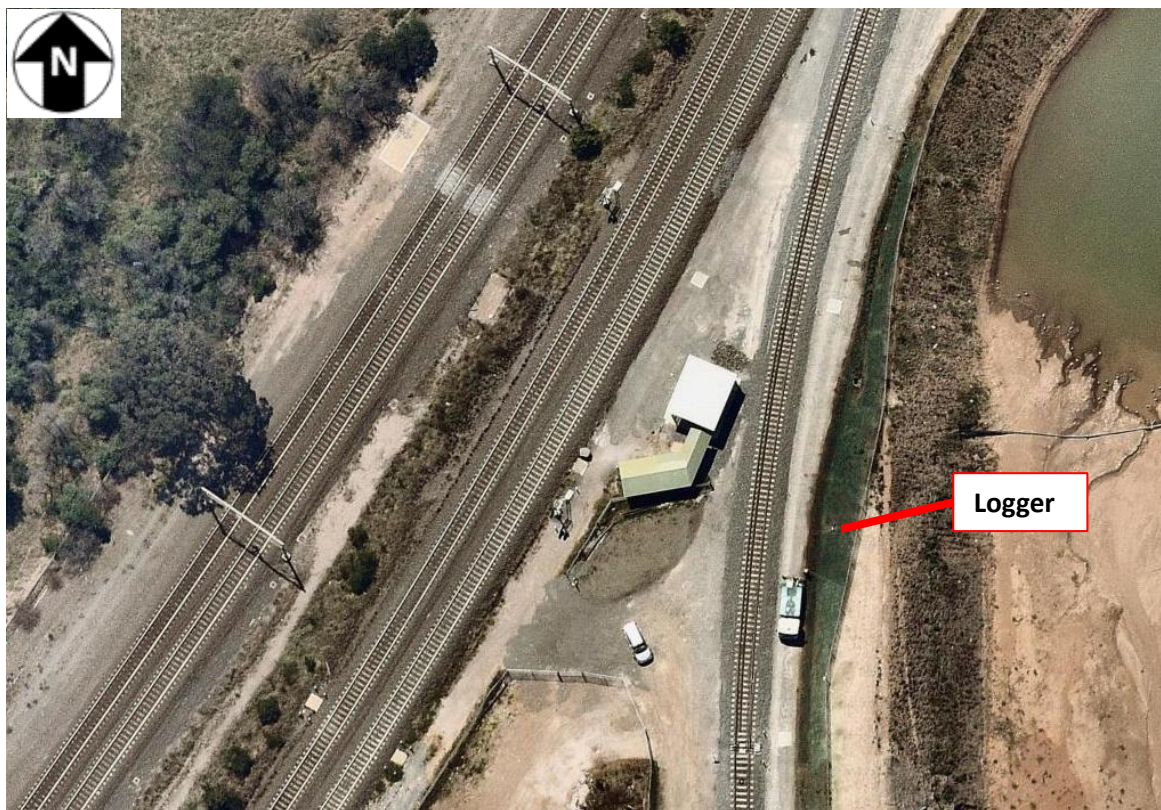
Technical Term	Description
Attenuation	A reduction in amplitude of noise or vibration due to increasing distance or other means such as noise barriers, materials or mitigation measures.
Adverse weather	Weather effects that enhance noise (that is, wind and temperature inversions) that occur at a site for a significant period (that is, wind occurring more than 30% of the time in any assessment period in any season and/or temperature inversions occurring more than 30% of the nights in winter).
Airborne noise	Noise that propagates through the air between source and receiver. Most relevant for noise from surface railway tracks or stationary facilities.
Alignment	The position of the railway tracks in three dimensions along their length.
Ambient noise	The all-encompassing noise within a given environment at a given time, usually composed of sound from all sources near and far.
Assessment period	The period in a day over which assessments are made. Assessment periods may be daytime, evening, night-time, 24-hour or busiest 1-hour period (when in use). Time periods associated with each assessment period are defined in the relevant section of this report and differ for rail operations and stationary facilities.
Assessment point	A point at which noise or vibration measurements are taken or calculated.
Background noise	Background noise is the term used to describe the underlying level of noise present in the ambient noise, measured in the absence of the noise under investigation, when extraneous noise is removed. It is described as the average of the minimum noise levels measured on a sound level meter and is measured statistically as the A-weighted noise level exceeded for ninety percent of a sample period. This is represented as the L_{90} noise level (see below).
Braking noise	Noise due to the rubbing of brake components of a rail vehicle
Chainage	Refers to the distance, along the railway tracks, from Central Station, usually given in kilometres or metres. Down direction refers to trains travelling away from Central Station. Up direction refers to trains travelling towards Central Station.
Decibel [dB]	A unit of measure commonly used to express noise and vibration. For sound, a reference level of 20 μPa is used. For vibration, a variety of reference levels are used. Vibration levels in this report use a reference level of 1 nm/s for vibration velocity and 1 $\mu\text{m/s}^2$ for vibration acceleration.

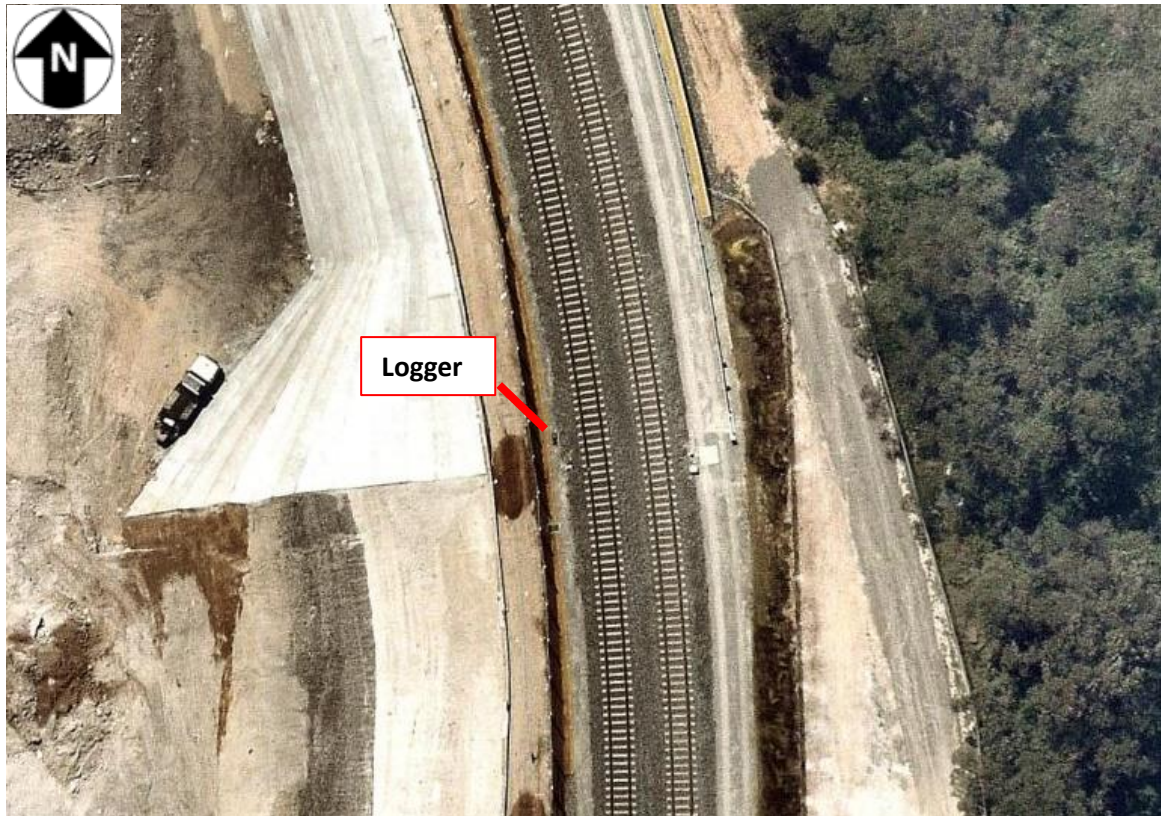
Technical Term	Description
dB(A)	A-weighted decibels. The ear is not as effective in hearing low frequency sounds as it is hearing high frequency sounds. That is, low frequency sounds of the same dB level are not heard as loud as high frequency sounds. The sound level meter replicates the human response of the ear by using an electronic filter which is called the "A" filter. A sound level measured with this filter switched on is denoted as dB(A). Practically all noise is measured using the A filter. The following are examples of the decibel readings of every day sounds: 0dB(A) The faintest sound we can hear 30dB(A) A quiet library or in a quiet location in the country 45dB(A) Typical office space. Ambience in the city at night 60dB(A) CBD mall at lunch time 70dB(A) The sound of a car passing on the street 80dB(A) Loud music played at home 90dB(A) The sound of a truck passing on the street 100dB(A) The sound of a rock band 115dB(A) Limit of sound permitted in industry 120dB(A) Deafening
EIS	Environmental Impact Statement
EPA	NSW Environmental Protection Authority
FEM	Finite element modelling
Flanging noise	Mid to high frequency noise due to contact between wheel flanges of a rail vehicle and the rail gauge face
Frequency	Frequency is synonymous to pitch. Sounds have a pitch which is peculiar to the nature of the sound generator. For example, the sound of a tiny bell has a high pitch and the sound of a bass drum has a low pitch. Frequency or pitch can be measured on a scale in units of Hertz or Hz.
GIS	Geographic Information System
HV	High Voltage
HVAC	Heating, Ventilation and Air-conditioning equipment
RING	Rail Noise Infrastructure Guideline
Impulsive noise or vibration	Having a high peak of short duration or a sequence of such peaks. A sequence of impulses in rapid succession is termed repetitive impulsive noise or vibration.
INP	NSW Industrial Noise Policy
Intermittent noise or vibration	The level suddenly drops to that of the background noise several times during the period of observation. The time during which the noise or vibration remains at levels different from that of the ambient is one second or more.
LAE	The A-weighted Sound Exposure Level (or SEL) is the constant sound level which, if maintained for a period of 1 second would have the same acoustic energy as the measured noise event. SEL noise measurements are useful as they can be converted to obtain Leq sound levels over any time period and can be used for predicting noise at various locations.
L _{Max}	The maximum sound pressure level measured over a given period.
L _{Min}	The minimum sound pressure level measured over a given period.
L ₁	The sound pressure level that is exceeded for 1% of the time for which the given sound is measured.
L ₁₀	The sound pressure level that is exceeded for 10% of the time for which the given sound is measured.
L ₉₀	The level of noise exceeded for 90% of the time. The bottom 10% of the sample is the L90 noise level expressed in units of dB(A).
Leq	The "equivalent noise level" is the summation of noise events and integrated over a selected period of time.

Technical Term	Description
Leq(9h)	Equivalent noise level for the 9 hour night-time period, defined as 10pm to 7am.
Leq(15h)	Equivalent noise level for the 15 hour daytime period, defined as 7am to 10pm.
LEP	Local environmental plan
LGA	Local government area
MEP	Mechanical and electrical plant
NCA	Noise catchment area
ONVR	Operational Noise and Vibration Review
RBL	Rating background level
Reflection	Sound wave changed in direction of propagation due to a solid object obscuring its path.
Receiver	A location or dwelling that is exposed to noise and/or vibration. A sensitive receiver refers to a building that has noise and/or vibration criteria that is required to be met.
SEL	Sound Exposure Level (SEL) is the constant sound level which, if maintained for a period of 1 second would have the same acoustic energy as the measured noise event. SEL noise measurements are useful as they can be converted to obtain Leq sound levels over any time period and can be used for predicting noise at various locations.
SI Unit	Units adopted as a standard for International use, for example, metres for distance, seconds for time, kilogram for mass, etc.
Sound	A fluctuation of air pressure which is propagated as a wave through air
Sound absorption	The ability of a material to absorb sound energy through its conversion into thermal energy
Sound level meter	An instrument consisting of a microphone, amplifier and indicating device, having a declared performance and designed to measure sound pressure levels
Sound pressure level	The level of noise, usually expressed in decibels, as measured by a standard sound level meter with a microphone
Sound power level	Ten times the logarithm to the base 10 of the ratio of the sound power of the source to the reference sound power
Source	Point from which noise and/or vibration is emitted
SSI	State Significant Infrastructure
TfNSW	Transport for NSW
Tonal noise	Containing a prominent frequency and characterised by a definite pitch
Track form	Consists of the rails, fasteners, sleepers, bed and foundations of the railway tracks
Wheel squeal	High frequency tonal noise that may occur when a rail vehicle negotiates a tight curve

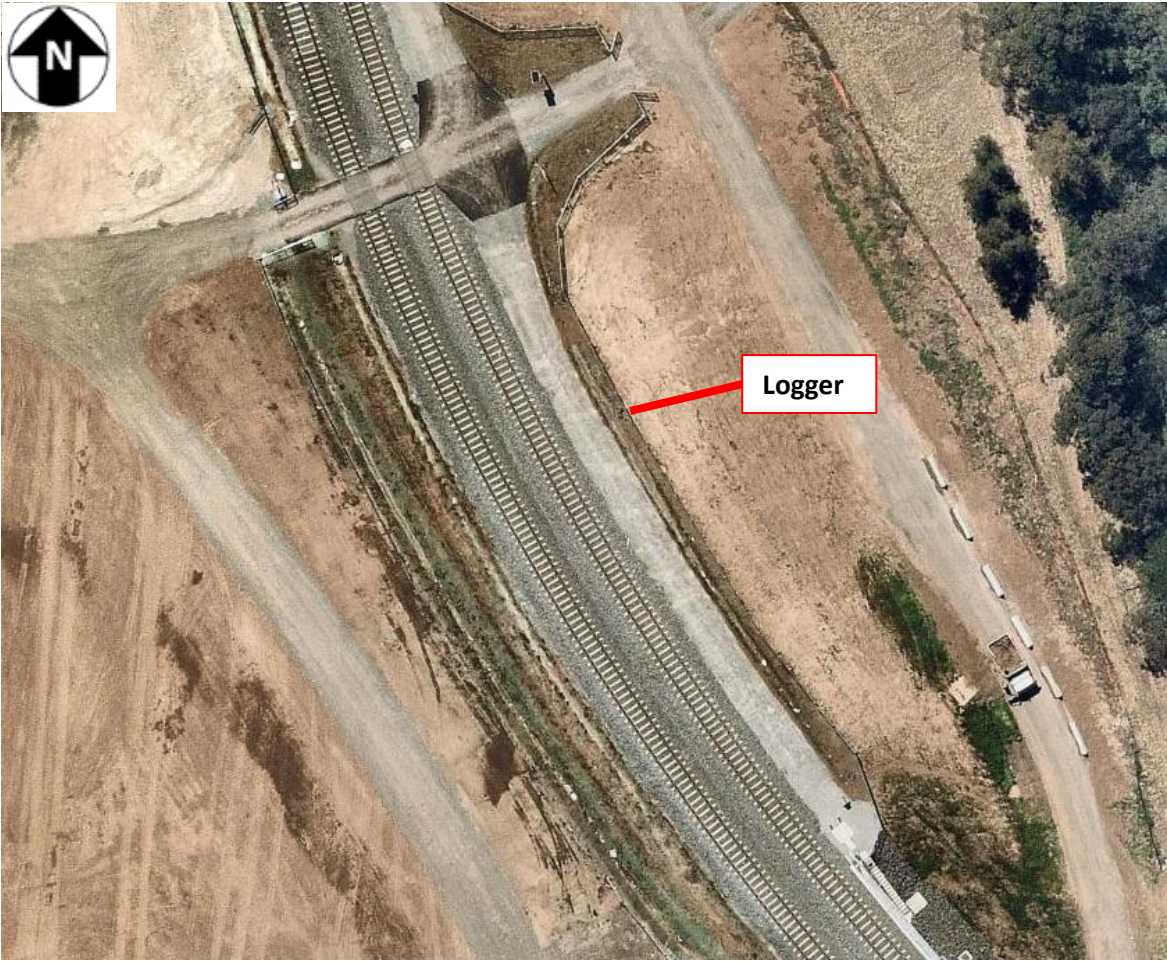
APPENDIX B Noise monitoring locations

B.1 Curve 1



B.2 Curve 2

B.3 Curve 3



B.4 Curve 4

B.5 Curve 5



B.6 Curve 6



APPENDIX C Detailed passby and noise event results

TL116-02F02 Curve noise monitoring report

TL116-02F02 Curve noise monitoring report

TL116-02F02 Curve noise monitoring report

B.15 Operational Road Traffic Noise Assessment - June 2021

Renzo Tonin Report TL116-05F14 Moorebank IMT Road Traffic (r1)

MOOREBANK LOGISTIC PARK - PRECINCT EAST

Operational Road Traffic Noise Assessment - June 2021

18 June 2021

Qube Property Management Services Pty Ltd c/- Tactical Group

TL116-05F14 Moorebank IMT Road Traffic (r1)

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1 Introduction

1.1 Project overview

The Sydney Intermodal Terminal Alliance (SIMTA) received approval for the construction and operation of Stages 1 and 2 of the Moorebank Precinct East (MPE) Project (SSD 6766 and SSD 7628, respectively), which together comprise the two stages of development under the MPE Concept Approval (MP10_0193).

This assessment has been conducted to assess the operational road traffic noise levels associated with MPE at the point in time when the site is 50% occupied.

Operational noise levels of road traffic on the public roads in proximity to the site are compared with the criteria and noise goals established in the NSW Road Noise Policy (RNP, EPA 2011). These are consistent with the road traffic noise goals established in the EIS.

This report addresses the following Approval Conditions. Additional details are provided in the compliance matrix (Table 1):

- SSD 6766

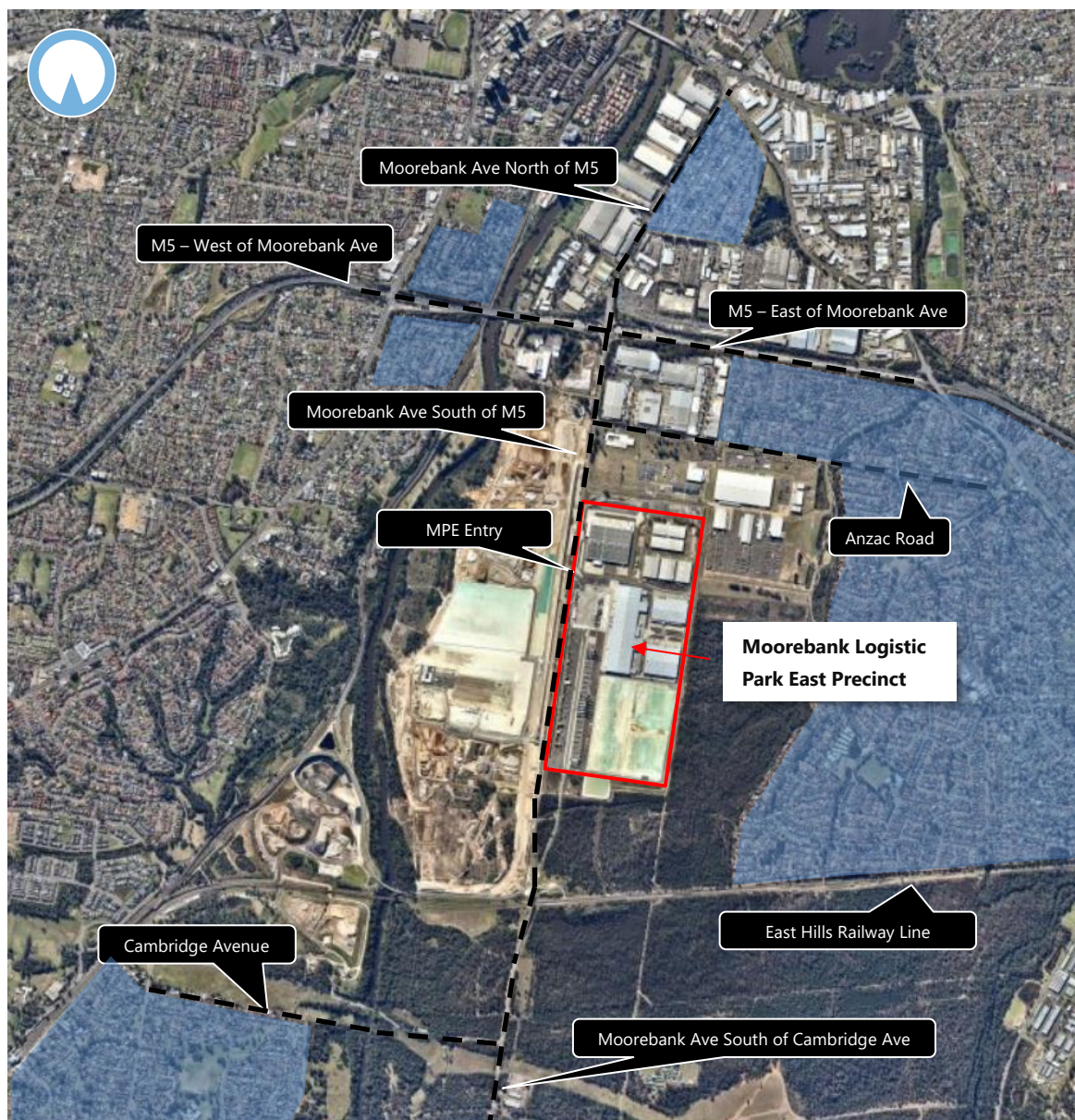
"Condition G15 – A review of the operational noise levels in terms of criteria and noise goals established in the NSW Road Noise Policy (EPA, 2011). Identification of additional feasible and reasonable measures that would be implemented with the objective of meeting the criteria outlined in the NSW Road Noise Policy (EPA, 2011)."

- SSD 7628

"Condition B86 – A validation by predictive modelling of the operational noise levels in terms of criteria and noise goals established in the NSW RNP (EPA, 2011). Any required recalibrations of the noise model taking into consideration factors such as actual traffic numbers and heavy vehicle proportions. Operational noise monitoring is required to assess compliance with the noise criteria at a point in time when the site is 50% occupied."

The location of Moorebank Precinct East (MPE) in relation to the nearest representative receivers and public roads is illustrated in Figure 1.

Figure 1 MPE Precinct, major roads and nearest sensitive receivers



Note: Blue shading represents residential land use areas adjacent to public roads in proximity to MPE.

1.2 Scope of assessment

Renzo Tonin & Associates (NSW) Pty Ltd has been engaged by Tactical to assess the potential noise impact associated with project-related road traffic travelling to and from MPE, in accordance with the approval conditions. This assessment includes attended noise measurements on Moorebank Avenue (north and south of the M5 Motorway), unattended noise monitoring at a representative residential receiver location on Moorebank Avenue (north of the M5 Motorway) and a review of traffic counting results.

The purpose of the assessment is to determine if the project-related road traffic noise for traffic travelling to and from MPE is within the RNP noise criteria.

A description of technical terms used within this report is provided in Appendix A.

2 Compliance Matrix

Table 1 provides a summary of the Approval Conditions which relate to operational road traffic noise on public roads.

Table 1 Compliance matrix

Condition ID	Condition	Comments on compliance	Reference for further information
SSD 6766			
G15	Within 12 months of the commencement of operation of the project, or as otherwise agreed by the Secretary, the Applicant shall undertake operational noise monitoring to compare actual noise performance of the project against noise performance predicted in the review of noise mitigation measures predicted in documents specified under condition A1 of this approval, and prepare an Operational Noise Report to document this monitoring. The Report shall include, but not necessarily be limited to:	This report includes operational road traffic noise modelling and prediction results. These are compared with the levels presented in the EIS and the criteria in the Planning Approval conditions.	n/a
G15 a)	noise monitoring to assess compliance with the operational noise levels predicted in documents specified under condition A1 of this approval;	Noise monitoring results are presented in Sections 4 and 6.	Sections 4 and 6
G15 b)	a review of the operational noise levels in terms of criteria and noise goals established in the NSW Road Noise Policy (EPA, 2011);	The applicable noise criteria are presented in Section 3.	Section 3.
G15 f)	any required recalibrations of the noise model taking into consideration factors such as actual traffic numbers and proportions;	All noise monitoring undertaken to date has complied with the operational noise limits. On this basis, recalibration of the noise models has not been required.	n/a
B86	Within 12 months of occupation of the first warehouse, 50% occupation of the site and 100% occupation of the site, or as otherwise agreed by the Secretary, the Applicant must undertake operational noise monitoring to compare actual noise performance of the project against predicted noise performance, and prepare an Operational Noise Report to document this monitoring. The Report must include, but not necessarily be limited to:	This report has been prepared at 50% site occupancy stage. Noise monitoring results are presented in Sections 4 and 6.	Sections 4 and 6
B86 b)	a validation by predictive modelling of the operational noise levels in terms of criteria and noise goals established in the NSW RNP (EPA, 2011);	A validation of the noise prediction model is provided in Section 4.	Section 4
B86 g)	any required recalibrations of the noise model taking into consideration factors such as actual traffic numbers and heavy vehicle proportions; and	All noise monitoring undertaken to date has complied with the operational noise limits. On this basis, recalibration of the noise models has not been required.	Sections 4, 5, 6 and 7

3 Summary of noise objectives

3.1 Applicable operation noise criteria

Noise impact from the potential increase in traffic on the roads surrounding the development is assessed against the NSW 'Road Noise Policy' (RNP). The RNP sets out noise criteria to be applied to particular types of road and land uses. These noise criteria are to be applied when assessing noise impact and determining mitigation measures for sensitive receivers that are potentially affected by road traffic noise associated with the subject development, with the aim of preserving the amenity appropriate to the land use.

The assessment considers the use of different types of vehicles entering and exiting the subject site through Moorebank Avenue and potential impacts upon nearby residences, in accordance with the relevant noise criteria. Vehicles associated with the subject site will travel along the following roads on the surrounding road network, consistent with the EIS. All roads are classified as motorways, arterial roads or sub-arterial roads, with the potential noise increase being assessed over the 15-hour day (7am to 10pm) and 9-hour night (10pm to 7am) periods, accordingly.

- Moorebank Avenue, north of the M5 Motorway
- Moorebank Avenue, south of the M5 Motorway (between M5 and MPE)
- Cambridge Avenue
- Moorebank Avenue, south of Cambridge Avenue
- Anzac Road
- M5 Motorway, east of Moorebank Avenue
- M5 Motorway, west of Moorebank Avenue

These roads are identified in Figure 1.

The RNP is used to assess the potential traffic noise impact from additional traffic generated by developments. The RNP provides criteria for residential type receivers impacted by the additional traffic generated by the project. All roads around the development are categorised as motorways, arterial roads or sub-arterial roads¹ and the appropriate assessment criteria are presented in Table 2.

Table 2 Road Traffic Noise Assessment Criteria for Residential Land Uses

Road category	Type of development	Assessment criteria, dB(A)	
		Day (7am - 10pm)	Night (10pm - 7am)
Freeway/ arterial/ sub-arterial roads	Existing residences affected by additional traffic on existing freeways/ arterial/ sub-arterial roads generated by land use developments	LAeq, (15 hour) 60 (external)	LAeq, (9 hour) 55 (external)

¹ Page 10 RNP, a "collector road" is classified in the same category as a sub-arterial road

Furthermore, the RNP states the following regarding increase in traffic noise on surrounding roads due to the subject development:

"For existing residences and other noise sensitive land uses affected by additional traffic on existing roads generated by land use development, any increase in the total traffic noise level should be limited to 2dB above that of the corresponding 'no build option'."

3.2 Summary of EIS noise assessment

Consistent with the operational noise criteria summarised in Section 3.1, the EIS noise and vibration assessment² identified that *"any increase in road traffic noise levels, at residential receivers, due to the SIMTA proposal should not exceed 2 dBA"*.

Assessment of the increase in road traffic noise levels along the M5 Motorway and Moorebank Avenue were calculated, using the Calculation of Road Traffic Noise (CoRTN) algorithm, and the following assumptions:

- Road traffic volume and mix
- Vehicle speeds (posted) of 100 km/h on the M5 Motorway and 60 km/h on Moorebank Avenue
- Typical receiver setback of 50 m along the M5 Motorway and 20 m along Moorebank Avenue.

Table 3 Road traffic volumes and mix (from EIS)

Location	Time	Current (no Development)		Current (with Development)	
		Volume	Mix	Volume	Mix
M5 Motorway East of Moorebank Avenue	Day (7.00am to 10.00pm)	91,500	10%	92,400	10%
	Night (10.00pm to 7.00am)	17,900	11%	18,200	10%
M5 Motorway West of Moorebank Avenue	Day (7.00am to 10.00pm)	107,200	10%	110,300	12%
	Night (10.00pm to 7.00am)	21,100	11%	21,700	12%
Moorebank Avenue North of M5 Motorway	Day (7.00am to 10.00pm)	26,700	10%	27,800	12%
	Night (10.00pm to 7.00am)	6,250	10%	6,410	10%
Moorebank Avenue South of M5 Motorway	Day (7.00am to 10.00pm)	14,400	6%	19,300	16%
	Night (10.00pm to 7.00am)	3,000	4%	4,100	10%

The study concluded that the project-related increase in road traffic noise levels along the M5 Motorway and along Moorebank Avenue, north of the M5 interchange are less than 2 dB(A) and therefore, comply with the relevant RNP criteria.

² Wilkinson Murray Report 12186-C – Sydney Intermodal Terminal Alliance Noise Assessment – Concept Plan, Section 6.3 Road Traffic Noise Assessment

In the area along Moorebank Avenue, south of the M5 interchange, road traffic noise levels were predicted to increase by approximately 3 dB(A). However, since there are no residential receivers in this area, no noise impact was expected.

4 Validation of road traffic noise model

Approval Condition B86 of SSD 7628 requires a validation of the operational road traffic prediction model. This has been performed in the current study via concurrent road traffic noise monitoring and road traffic counting at a representative residential receiver on Moorebank Avenue, north of the M5 interchange. The noise monitoring and road traffic counting were performed over a 14-day period between Thursday 27 May and Friday 11 June 2021.

An unattended noise logger was set up at a free-field location in the front yard of 62 Moorebank Avenue, 7.5 m from the edge of the nearside southbound lane. Moorebank Avenue comprises two southbound and two northbound lanes at this location.

The unattended noise monitoring was performed with a Type 1 sound level meter. A Type 1 microphone calibrator was utilised before and after the measurements to verify that the pre- and post-calibration levels were within 0.5 dB of the reference value. The noise measurements were performed in accordance with the requirements of the RNP.

Daily plots of the measured road traffic noise levels are provided in Appendix B. The noise logging results were processed to determine the $L_{Aeq(15\text{hour})}$ daytime and $L_{Aeq(9\text{hour})}$ night-time noise levels at the measurement position, averaged over the two-week survey period. Extraneous noise events during rain periods were excluded from the summary results. The noise monitoring results were also reviewed to identify 15-minute periods that contained siren noise from emergency services. These periods were also excluded from the summary results.

Road traffic counting was performed by Matrix Traffic and Transport Data at a position between Church Road and King Lane, along Moorebank Avenue. The traffic survey included full classification of heavy and light vehicles in both directions, summarised on an hourly basis over the 14-day survey period. The average vehicle speeds in each hour were also recorded.

A summary of the average road traffic volumes, speeds and percentage heavy vehicles is provided in Table 4.

Table 4 Summary of road traffic volumes (28 May to 10 June 2021) – Moorebank Avenue north of M5 interchange

Location	Daytime period (7am to 10pm)			Night-time period (10pm to 7am)		
	Northbound	Southbound	Total	Northbound	Southbound	Total
Number of vehicles per day	13,006	9,033	22,039	2,952	1,659	4,612
Percentage heavy vehicles	14%	16%	14%	16%	12%	15%
Average speed	59 km/h (daytime)			63 km/h (night-time)		

The average road traffic volumes, heavy vehicle mix and speeds were utilised in a CoRTN model to predict the daytime and night-time noise levels at the unattended noise logger position.

A comparison of the predicted and measured noise levels at the noise monitoring position is provided in Table 5.

Table 5 Summary of road traffic noise model validation – 62 Moorebank Avenue

Period	Measured $L_{Aeq(period)}$ noise level, dB(A)	Predicted $L_{Aeq(period)}$ noise level, dB(A)	Noise Level Difference, Predicted minus Measured, dB(A)
7.00am to 10.00pm daytime	71.3	71.6	0.3
10.00pm to 7.00am night-time	68.0	67.3	-0.7

The results in the above table identify that the difference between the measured noise levels and predicted noise levels at the noise monitoring location are within an acceptable tolerance of ± 1.0 dB(A).

This indicates that the CoRTN noise model is acceptable for predicting the overall noise levels and project-related noise increase at other representative locations near MPE.

5 MPE road traffic noise predictions

A Biannual Trip Origin and Destination Report (BTODR)³ was prepared by Ason Group for MPE, in accordance with the requirements of Approval Condition B28 of SSD 7628.

The report provides a summary of origin destination (OD) road traffic survey results to understand the distribution of MPE traffic on the surrounding road network. The measurement data is applicable for the reporting period between 1 November 2020 and 30 April 2021.

A summary of the average day / night traffic volumes (weekdays), derived from the BTODR data is provided in Table 6.

Table 6 Origin destination road traffic volumes and mix

Location	Time	Current (excluding MPE)		Current (including MPE)	
		Volume	Mix	Volume	Mix
M5 Motorway On/Off ramps to East ¹	Day (7.00am to 10.00pm)	15,237	9%	15,543	9%
	Night (10.00pm to 7.00am)	2,510	7%	2,551	7%
M5 Motorway On/Off ramps to West ¹	Day (7.00am to 10.00pm)	34,933	10%	35,378	10%
	Night (10.00pm to 7.00am)	5,240	9%	5,331	9%
Moorebank Avenue North of M5 Motorway	Day (7.00am to 10.00pm)	33,196	10%	33,405	10%
	Night (10.00pm to 7.00am)	5,074	9%	5,113	9%
Moorebank Avenue South of M5 Motorway	Day (7.00am to 10.00pm)	33,786	8%	34,827	9%
	Night (10.00pm to 7.00am)	5,193	6%	5,376	6%
Anzac Road	Day (7.00am to 10.00pm)	16,595	6%	16,684	6%
	Night (10.00pm to 7.00am)	1,983	5%	1,987	5%
Cambridge Avenue	Day (7.00am to 10.00pm)	22,661	6%	22,722	6%
	Night (10.00pm to 7.00am)	3,978	4%	3,983	4%
Moorebank Avenue South of Cambridge Avenue	Day (7.00am to 10.00pm)	1,976	4%	1,976	4%
	Night (10.00pm to 7.00am)	290	2%	290	2%
1. The BTODR did not include road traffic volumes for the M5 Motorway. For noise modelling purposes, road traffic volumes without MPE are based on the volumes in Table 3. The road traffic volumes with MPE are based on the including and excluding MPE traffic volumes in this table.					

Based on the above traffic volumes with and without the MPE traffic, calculations of road traffic noise using CoRTN have been performed at representative residential receivers along each section of road. The results are provided in Table 7.

³ Ason Group, Biannual Trip Origin Destination Report - November 2020 - April 2021- Report P1065r03v1

Table 7 Predicted MPE road traffic noise levels at representative residential receivers

Location	Time	Typical setback distance to residential receivers, m	Predicted $L_{Aeq(period)}$ noise level, dB(A) ¹		Predicted noise increase from MPE
			Without MPE	With MPE	
M5 Motorway East of Moorebank Ave	Day (7.00am to 10.00pm)	25	64.5	64.5	0.0
	Night (10.00pm to 7.00am)	25	59.8	59.8	0.0
M5 Motorway On/Off ramps to West	Day (7.00am to 10.00pm)	25	65.2	65.2	0.0
	Night (10.00pm to 7.00am)	25	60.5	60.5	0.0
Moorebank Avenue North of M5 Motorway	Day (7.00am to 10.00pm)	10	71.7	71.8	0.1
	Night (10.00pm to 7.00am)	10	65.9	66.0	0.1
Moorebank Avenue South of M5 Motorway	Day (7.00am to 10.00pm)	n/a	No nearby residential receivers		0.3
	Night (10.00pm to 7.00am)	n/a	No nearby residential receivers		0.2
Anzac Road	Day (7.00am to 10.00pm)	6	71.9	71.9	0.0
	Night (10.00pm to 7.00am)	6	64.5	64.5	0.0
Cambridge Avenue	Day (7.00am to 10.00pm)	145	55.3	55.4	0.1
	Night (10.00pm to 7.00am)	145	49.7	49.7	0.0
Moorebank Avenue South of Cambridge Avenue	Day (7.00am to 10.00pm)	n/a	No nearby residential receivers		0.0
	Night (10.00pm to 7.00am)	n/a	No nearby residential receivers		0.0

Note: Overall noise levels are shown to 1 decimal place for the purpose of indicating the change in noise levels from MPE traffic. The accuracy of the overall noise level predictions is approximately ± 1 dB(A).

The results in the above table identify that the project-related increase in road traffic noise levels from MPE is 0.1 dB(A) or less at the nearest residential receivers.

The highest predicted increase of 0.3 dB(A) occurs in the area between the MPE site entry and the M5 interchange. It is noted that there are no residential receivers in this area.

6 Attended noise measurements

Attended noise measurements were performed at two locations on 27 May 2021 for the purpose of quantifying the noise levels of heavy vehicles entering / exiting MPE. The measurements were performed between 8:30 am and 10:30 am at the following locations.

- Near the MPE entry / exit on Moorebank Avenue (south of the M5 interchange) – opposite Target Warehouse
- Moorebank Avenue (north of the M5 interchange) – near King Lane

At each location, continuous noise measurements of road traffic noise were made. Video cameras were set up to provide a visual record of road traffic movements. These were time-synchronised with the noise recordings. The video recordings were reviewed to positively identify MPE heavy vehicles that entered / exited MPE and also passed by the Moorebank Avenue residential area, north of the M5 interchange.

The noise measurement results were post-processed to determine the noise contribution of MPE heavy vehicles in relation to non-MPE road traffic noise.

During the two-hour noise survey, 48 heavy vehicles were observed to enter / exit the MPE facility. Nine (9) MPE heavy vehicles were observed to pass the Moorebank Avenue residential area, north of the M5 interchange. The noise levels of these passbys were analysed and compared with the prevailing road traffic noise levels during the two-hour survey period and the noise increase from MPE heavy vehicles was determined to be 0.1 dB(A).

The measured traffic noise level increase of 0.1 dB(A) from MPE trucks in the residential area adjacent to Moorebank Avenue, north of the M5 interchange is consistent with the calculated 0.1 dB(A) increase presented in Table 7 and less than the 2 dB(A) allowance stipulated in Section 3.1.

7 Conclusion

The assessment presented in this report has been conducted to address the requirements of Approval Condition B86 of SSD 7628 and Approval Condition G15 of SSD 6766, and assesses the operational road traffic noise levels associated with MPE at the point in time when the subject site is 50% occupied.

This report presents the results of road traffic noise measurements and calculations at representative residential receiver locations along public roads in proximity to MPE. The measured and calculated increase in project-related road traffic noise have been compared with the 2 dB(A) allowance, derived from the NSW RNP.

Approval Condition B86 of SSD 7628 requires a validation of the operational road traffic prediction model. This has been performed in this current study via concurrent road traffic noise monitoring and road traffic counting at a representative residential receiver on Moorebank Avenue, north of the M5 interchange. The difference between the measured and predicted noise levels was less than the acceptable tolerance of ± 1.0 dB(A).

This validated noise model was subsequently utilised in conjunction with the Biannual Trip Origin and Destination Report, to understand the distribution of MPE traffic on the surrounding road network, and to predict the project-related increase in road traffic noise levels.

The project-related increase in road traffic noise levels from MPE was calculated to be 0.1 dB(A) or less at the nearest residential receivers. The highest calculated increase of 0.3 dB(A) occurs in the area between the MPE site entry and M5 interchange where there are no residential receivers in this area.

Attended noise measurements were performed in conjunction with visual observations of trucks entering / exiting MPE to directly measure the noise increase of MPE trucks over a two-hour period in the residential area on Moorebank Avenue, north of the M5 interchange. The measured noise level increase from MPE trucks was 0.1 dB(A), consistent with the noise model calculations.

It is concluded that the project-related increase in road traffic noise levels related to MPE is less than the 2 dB(A) allowance in the NSW RNP. Therefore, no re-calibration of the road traffic noise model and/or consideration of additional mitigation measures are required at this stage.

APPENDIX A Description of technical terms

The following is a brief description of the technical terms used to describe noise to assist in understanding the technical issues presented.

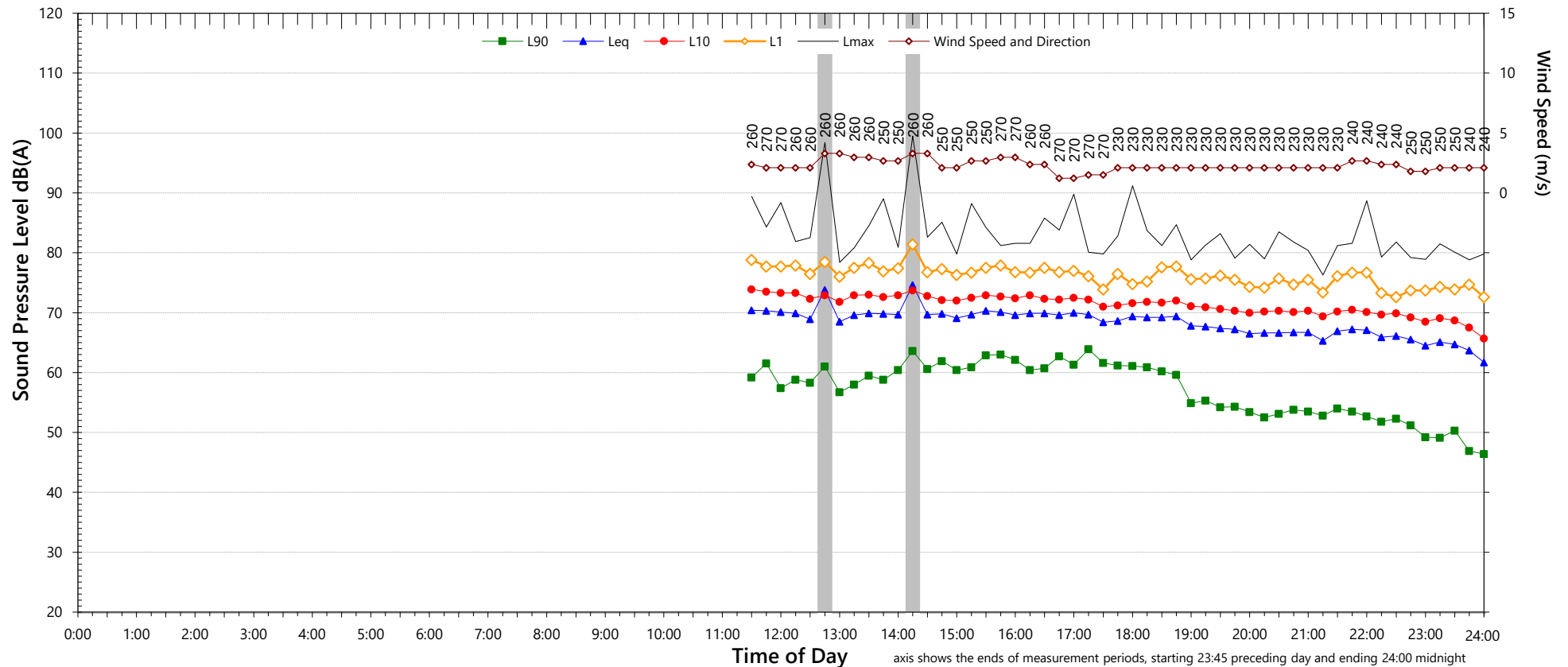
Adverse weather	Weather effects that enhance noise (that is, wind and temperature inversions) that occur at a site for a significant period of time (that is, wind occurring more than 30% of the time in any assessment period in any season and/or temperature inversions occurring more than 30% of the nights in winter).
Ambient noise	The all-encompassing noise associated within a given environment at a given time, usually composed of sound from all sources near and far.
Assessment period	The period in a day over which assessments are made.
Assessment point	A point at which noise measurements are taken or estimated. A point at which noise measurements are taken or estimated.
Background noise	Background noise is the term used to describe the underlying level of noise present in the ambient noise, measured in the absence of the noise under investigation, when extraneous noise is removed. It is described as the average of the minimum noise levels measured on a sound level meter and is measured statistically as the A-weighted noise level exceeded for ninety percent of a sample period. This is represented as the L90 noise level (see below).
Decibel [dB]	The units that sound is measured in. The following are examples of the decibel readings of every day sounds: 0dB The faintest sound we can hear 30dB A quiet library or in a quiet location in the country 45dB Typical office space. Ambience in the city at night 60dB CBD mall at lunch time 70dB The sound of a car passing on the street 80dB Loud music played at home 90dB The sound of a truck passing on the street 100dB The sound of a rock band 115dB Limit of sound permitted in industry 120dB Deafening
dB(A)	A-weighted decibels. The A- weighting noise filter simulates the response of the human ear at relatively low levels, where the ear is not as effective in hearing low frequency sounds as it is in hearing high frequency sounds. That is, low frequency sounds of the same dB level are not heard as loud as high frequency sounds. The sound level meter replicates the human response of the ear by using an electronic filter which is called the "A" filter. A sound level measured with this filter switched on is denoted as dB(A). Practically all noise is measured using the A filter.
dB(C)	C-weighted decibels. The C-weighting noise filter simulates the response of the human ear at relatively high levels, where the human ear is nearly equally effective at hearing from mid-low frequency (63Hz) to mid-high frequency (4kHz), but is less effective outside these frequencies.
Frequency	Frequency is synonymous to pitch. Sounds have a pitch which is peculiar to the nature of the sound generator. For example, the sound of a tiny bell has a high pitch and the sound of a bass drum has a low pitch. Frequency or pitch can be measured on a scale in units of Hertz or Hz.
Impulsive noise	Having a high peak of short duration or a sequence of such peaks. A sequence of impulses in rapid succession is termed repetitive impulsive noise.
Intermittent noise	The level suddenly drops to that of the background noise several times during the period of observation. The time during which the noise remains at levels different from that of the ambient is one second or more.
LMax	The maximum sound pressure level measured over a given period.
LMin	The minimum sound pressure level measured over a given period.

APPENDIX B Unattended noise monitoring results

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Thursday, 27 May 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	-	53	45
L _{Aeq}	-	67	66

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	79	to	93
L _{AFMax} - L _{Aeq} (Range)	15	to	23

Notes:

1. Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

3. "Evening" is the period from 6pm till 10pm

6. Graphed data measured in free-field; tabulated results facade corrected

4. "Night" relates to the remaining periods

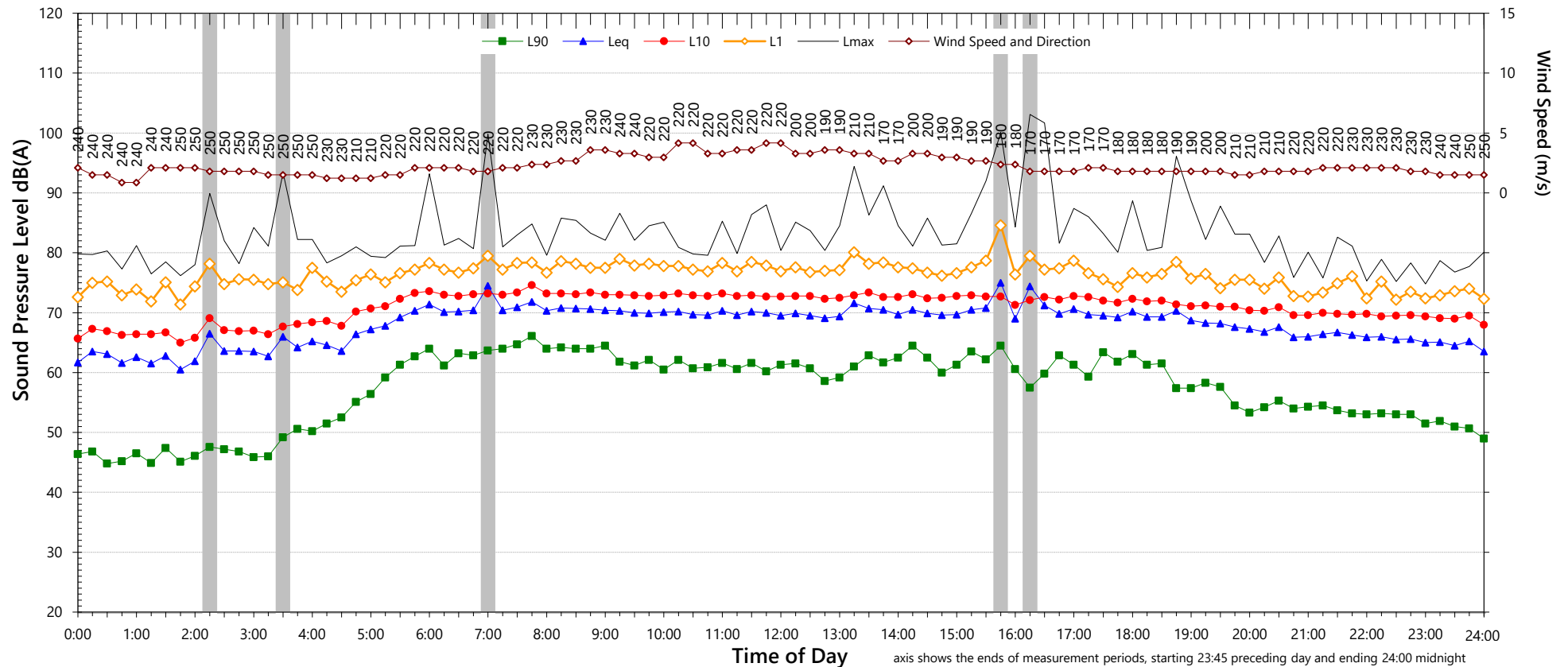
7. 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	-	-
L _{Aeq} 1hr upper 10 percentile	-	-
L _{Aeq} 1hr lower 10 percentile	-	-

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Friday, 28 May 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	60	53	45
L _{Aeq}	70	68	64

Night Time Maximum Noise Levels (see note 7)			
L _{AFMax} (Range)	80	to	86
L _{AFMax} - L _{Aeq} (Range)	15	to	23

Notes:

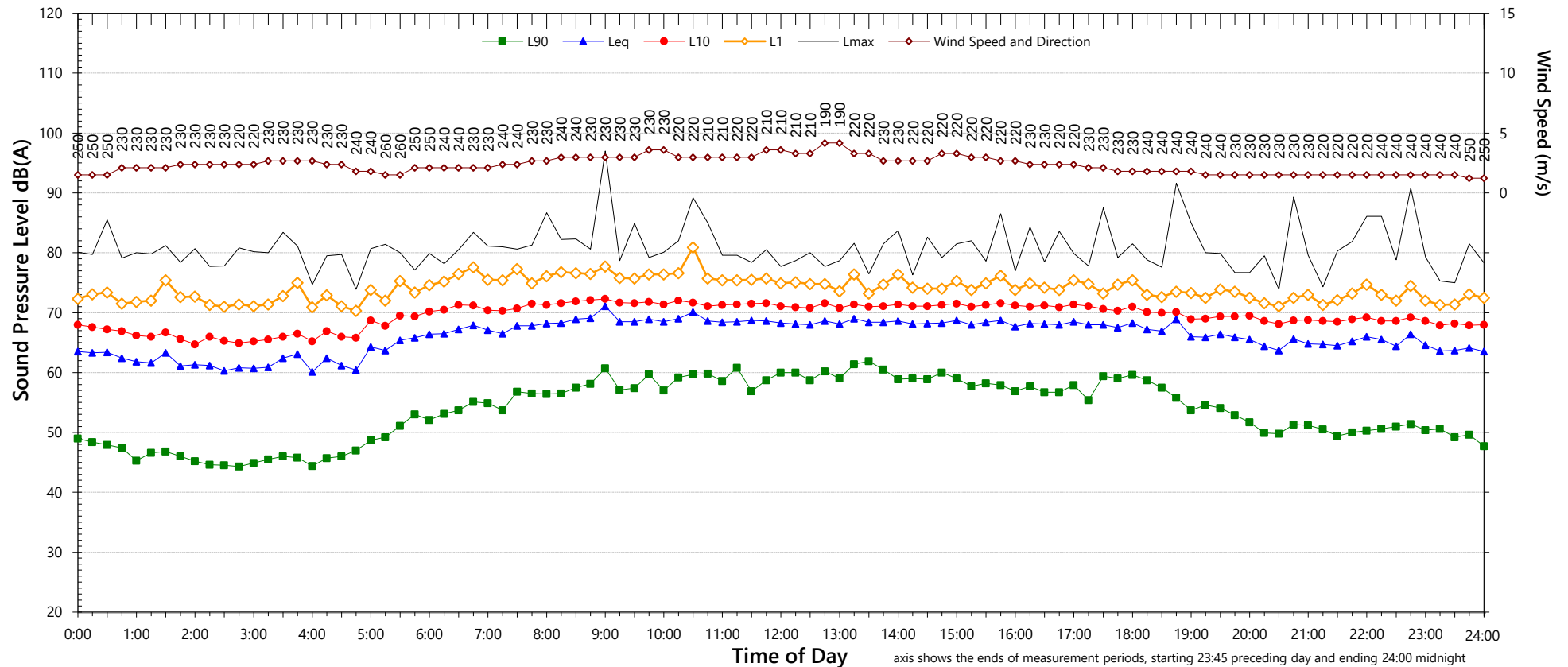
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	72	67
L _{Aeq} 1hr upper 10 percentile	73	68
L _{Aeq} 1hr lower 10 percentile	70	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Saturday, 29 May 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	57	50	43
L _{Aeq}	68	66	63

Night Time Maximum Noise Levels (see note 7)			
L _{AFMax} (Range)	78	to	91
L _{AFMax} - L _{Aeq} (Range)	16	to	26

Notes:

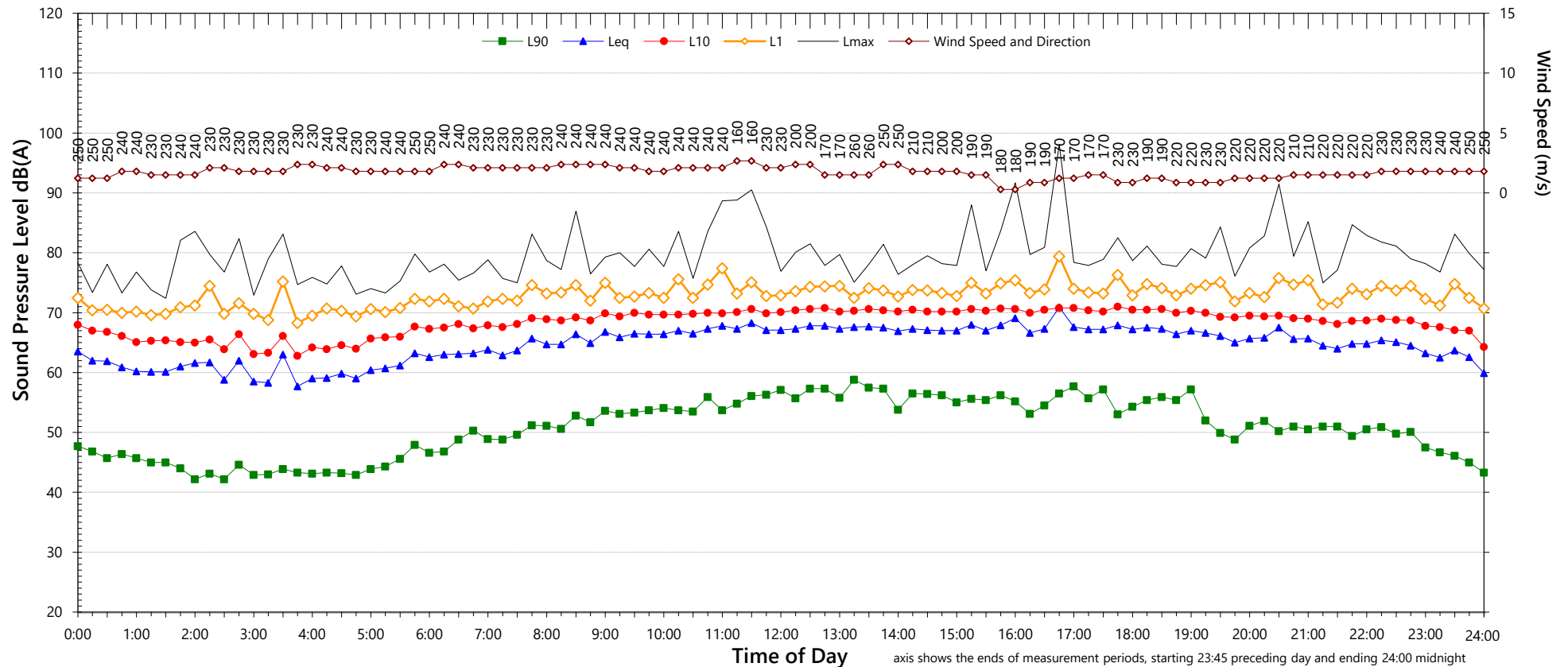
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	70	65
L _{Aeq} 1hr upper 10 percentile	71	67
L _{Aeq} 1hr lower 10 percentile	68	62

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Sunday, 30 May 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	53	50	40
L _{Aeq}	67	66	65

Night Time Maximum Noise Levels (see note 7)			
L _{AFMax} (Range)	81	to	88
L _{AFMax} - L _{Aeq} (Range)	17	to	23

Notes:

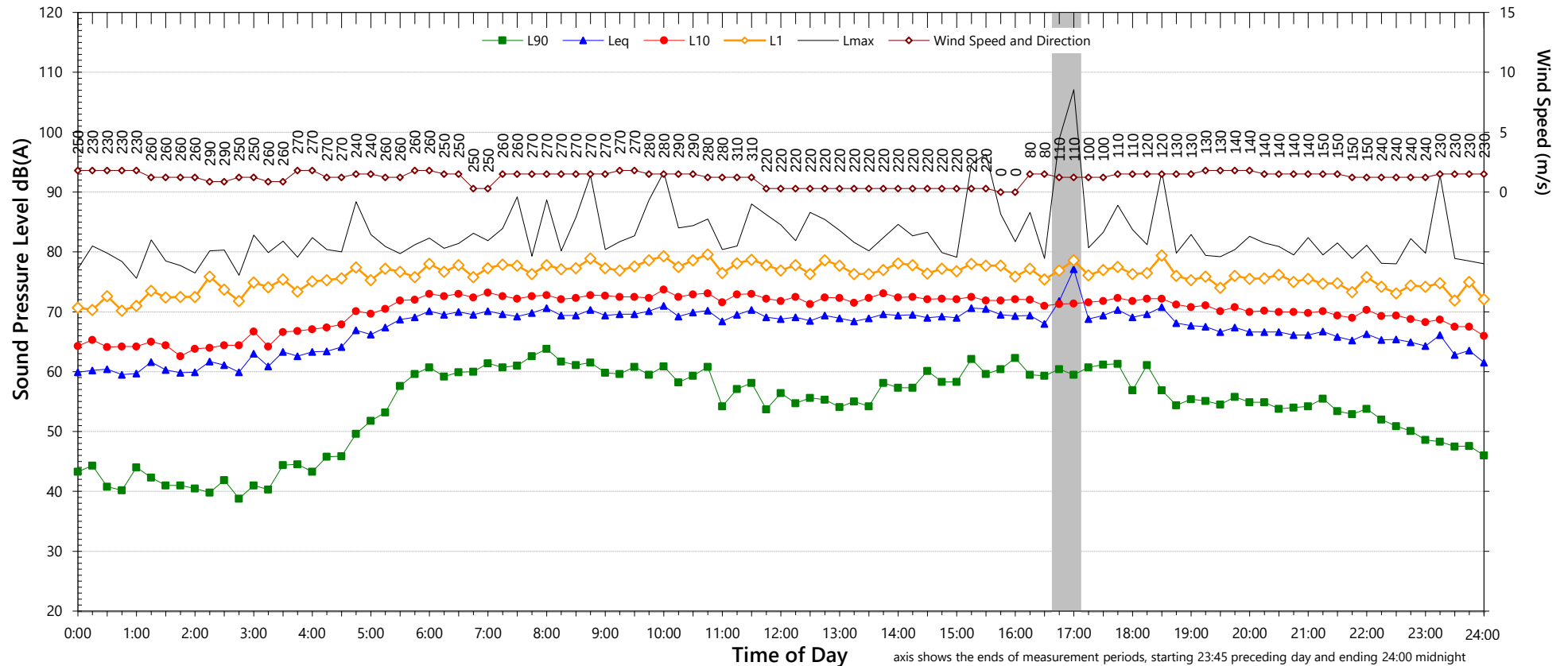
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	69	68
L _{Aeq} 1hr upper 10 percentile	70	72
L _{Aeq} 1hr lower 10 percentile	68	63

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Monday, 31 May 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	55	54	41
L _{Aeq}	70	67	66

Night Time Maximum Noise Levels (see note 7)			
L _{AFMax} (Range)	81	to	93
L _{AFMax} - L _{Aeq} (Range)	17	to	29

Notes:

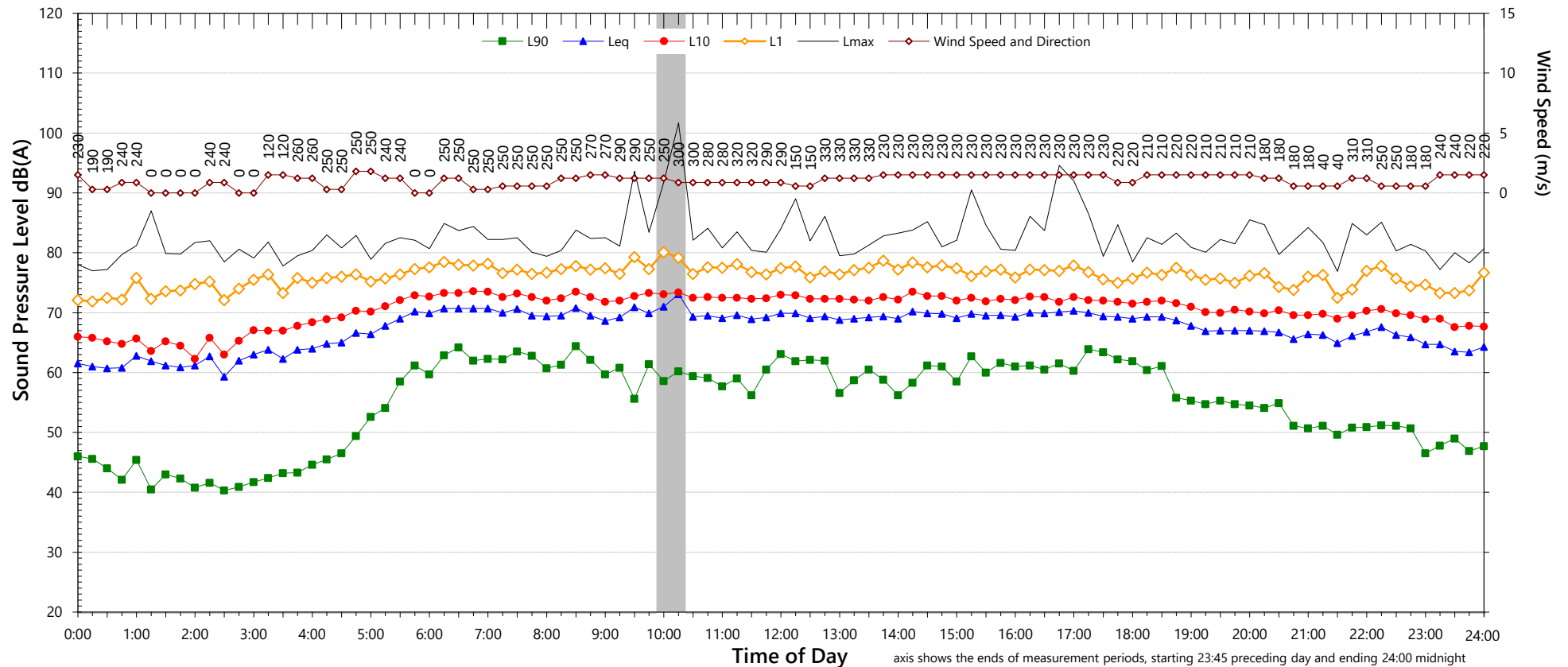
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	72	69
L _{Aeq} 1hr upper 10 percentile	72	72
L _{Aeq} 1hr lower 10 percentile	69	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Tuesday, 1 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	58	51	41
L _{Aeq}	70	67	66

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	81	to	88
L _{AFMax} - L _{Aeq} (Range)	17	to	22

Notes:

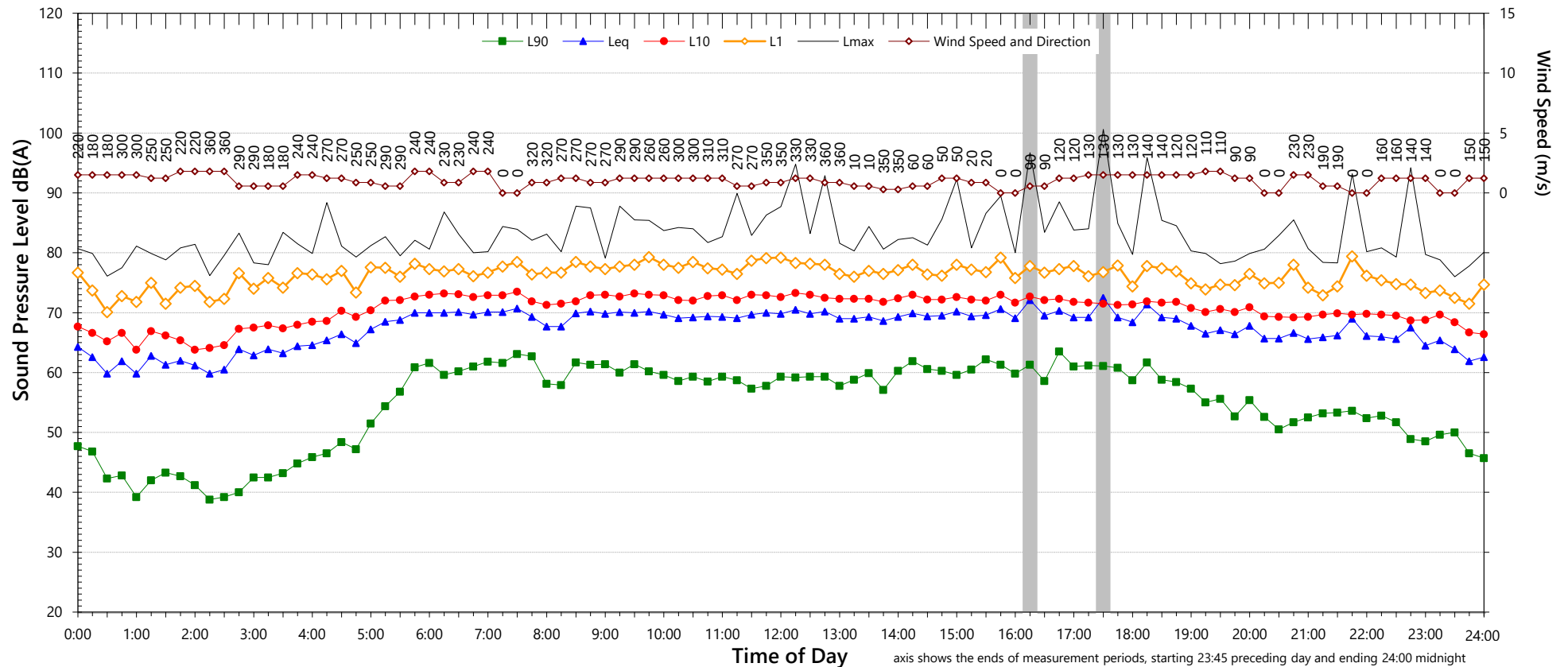
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	72	69
L _{Aeq} 1hr upper 10 percentile	72	72
L _{Aeq} 1hr lower 10 percentile	69	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Wednesday, 2 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	58	52	43
L _{Aeq}	70	68	66

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	80	to	94
L _{AFMax} - L _{Aeq} (Range)	16	to	28

Notes:

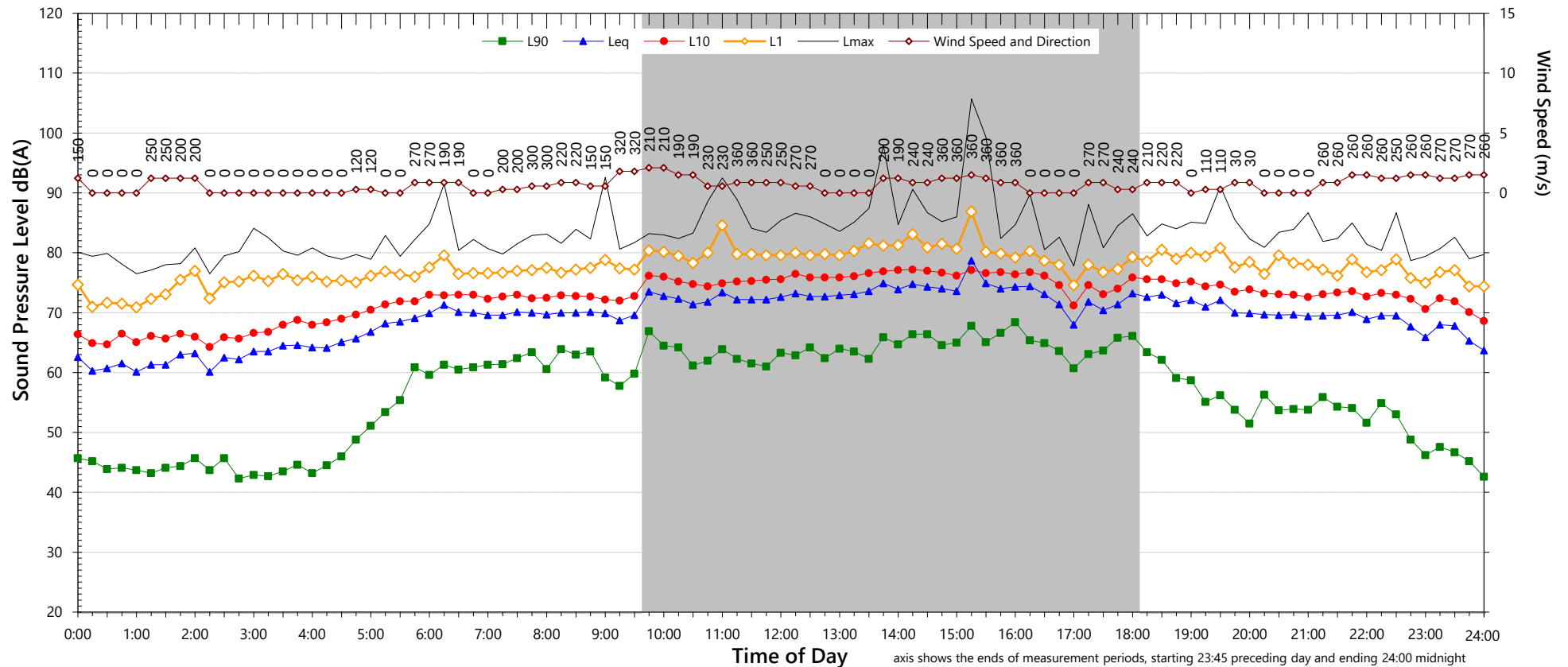
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	72	68
L _{Aeq} 1hr upper 10 percentile	72	72
L _{Aeq} 1hr lower 10 percentile	69	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Thursday, 3 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	-	53	44
L _{Aeq}	-	71	69

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	81	to	91
L _{AFMax} - L _{Aeq} (Range)	16	to	23

Notes:

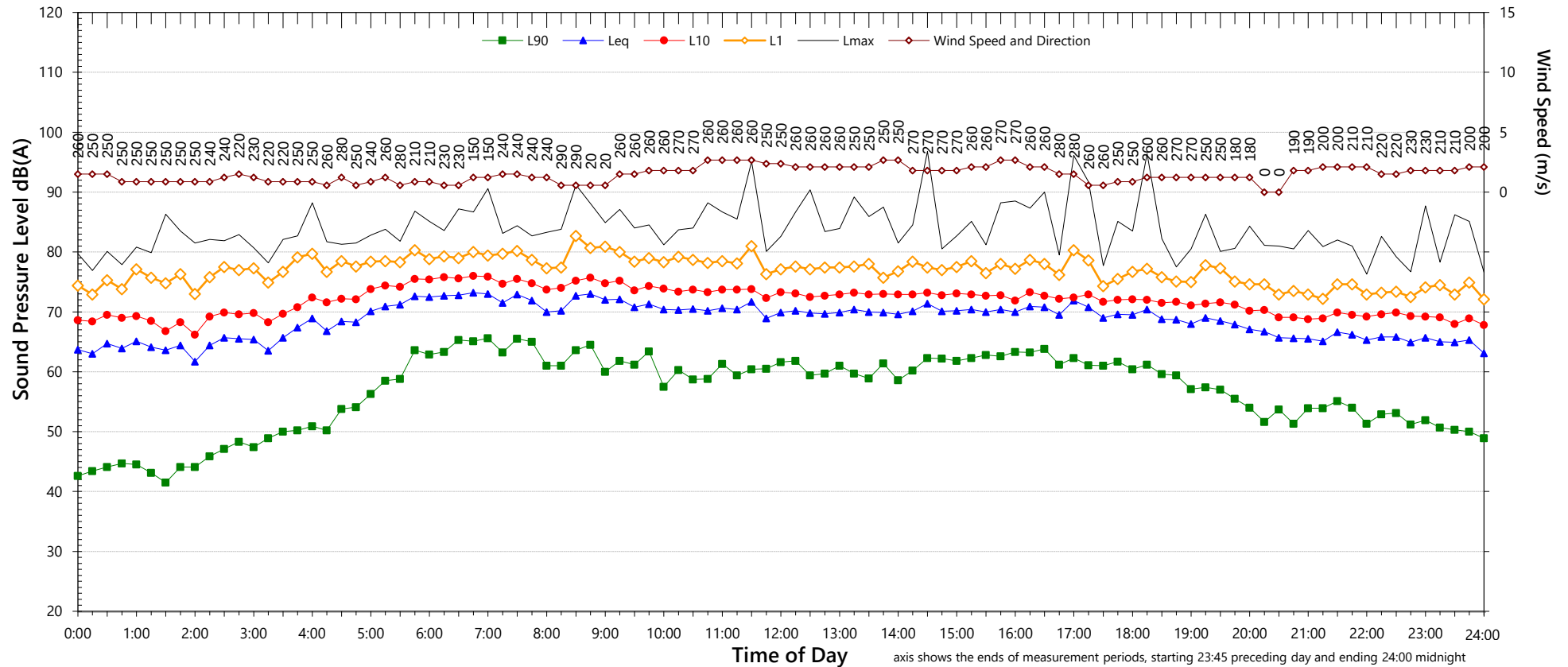
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- "Night" relates to period from 10pm on this graph to morning on the following graph.
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	73	71
L _{Aeq} 1hr upper 10 percentile	74	75
L _{Aeq} 1hr lower 10 percentile	72	67

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Friday, 4 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	59	51	46
L _{Aeq}	71	67	64

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	78	to	93
L _{AFMax} - L _{Aeq} (Range)	15	to	30

Notes:

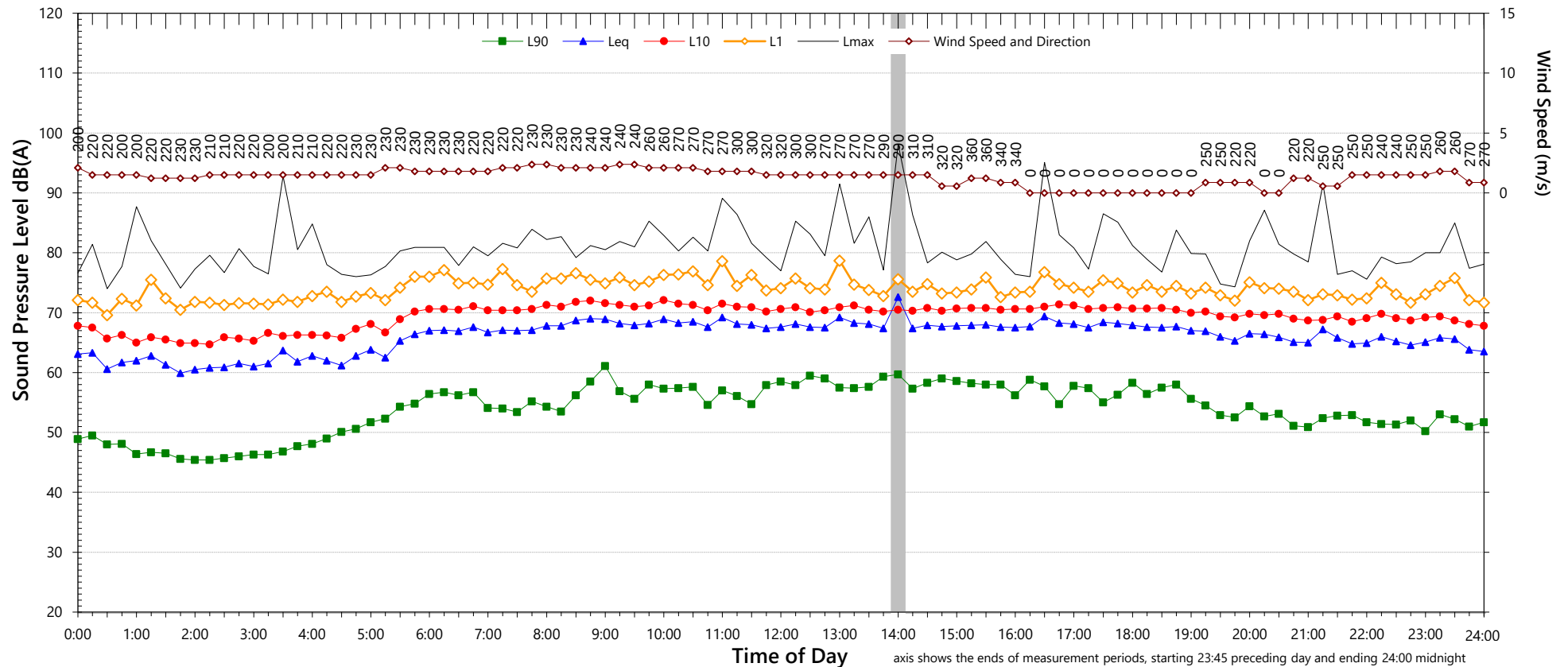
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	73	67
L _{Aeq} 1hr upper 10 percentile	74	68
L _{Aeq} 1hr lower 10 percentile	69	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Saturday, 5 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	55	51	44
L _{Aeq}	68	66	63

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	78	to	90
L _{AFMax} - L _{Aeq} (Range)	15	to	29

Notes:

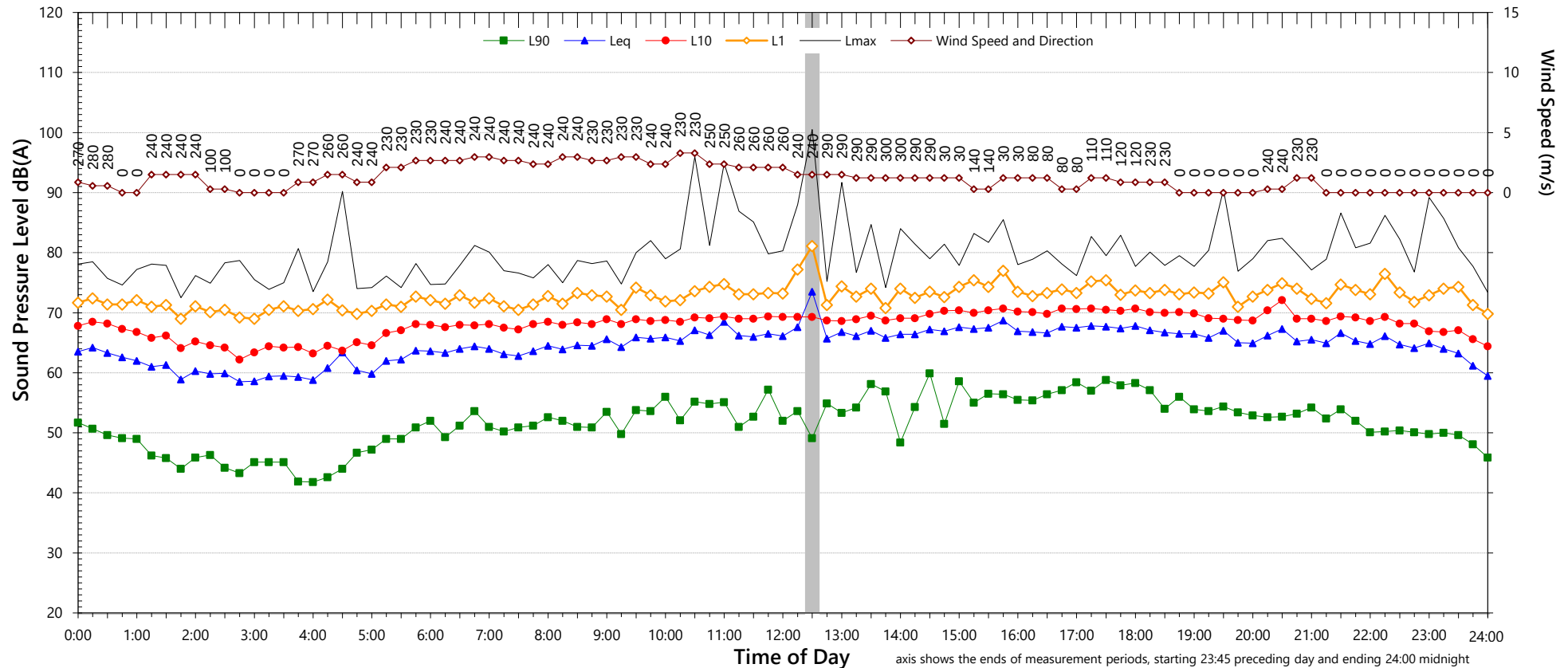
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	70	65
L _{Aeq} 1hr upper 10 percentile	71	67
L _{Aeq} 1hr lower 10 percentile	68	62

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Sunday, 6 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	51	52	44
L _{Aeq}	67	66	65

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	79	to	91
L _{AFMax} - L _{Aeq} (Range)	18	to	24

Notes:

1. Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

3. "Evening" is the period from 6pm till 10pm

6. Graphed data measured in free-field; tabulated results facade corrected

4. "Night" relates to the remaining periods

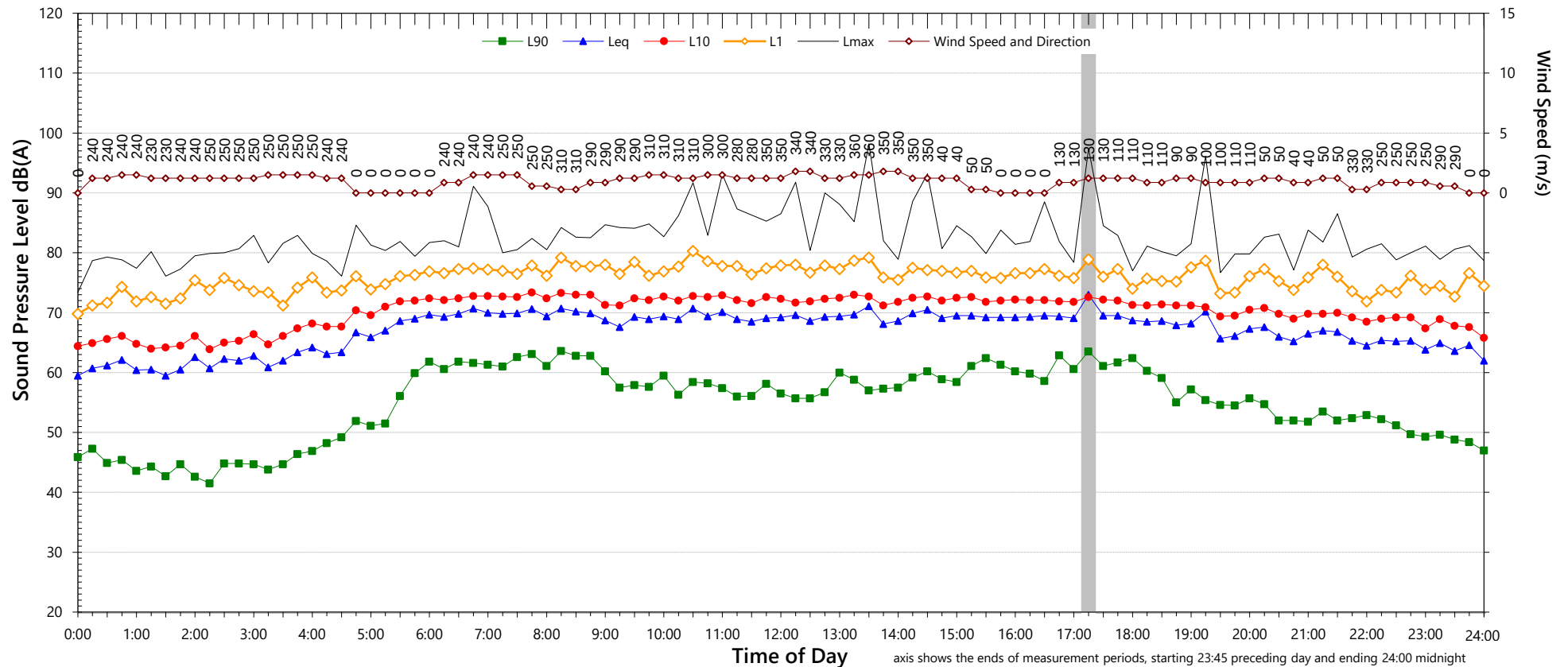
7. 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	69	68
L _{Aeq} 1hr upper 10 percentile	70	71
L _{Aeq} 1hr lower 10 percentile	68	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Monday, 7 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	56	52	47
L _{Aeq}	69	67	66

Night Time Maximum Noise Levels (see note 7)			
L _{AFMax} (Range)	79	to	90
L _{AFMax} - L _{Aeq} (Range)	17	to	20

Notes:

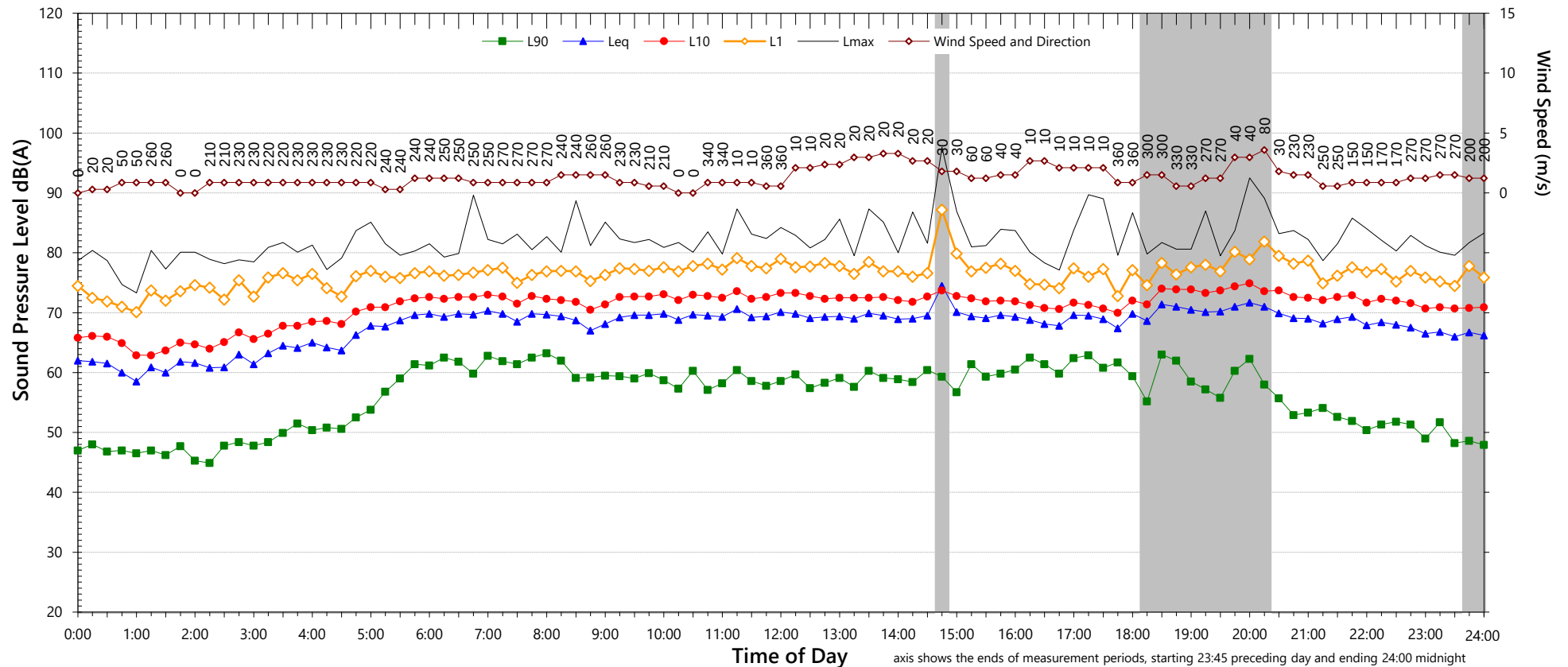
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	71	68
L _{Aeq} 1hr upper 10 percentile	72	72
L _{Aeq} 1hr lower 10 percentile	69	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Tuesday, 8 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	58	-	41
L _{Aeq}	69	-	69

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	81	to	94
L _{AFMax} - L _{Aeq} (Range)	15	to	28

Notes:

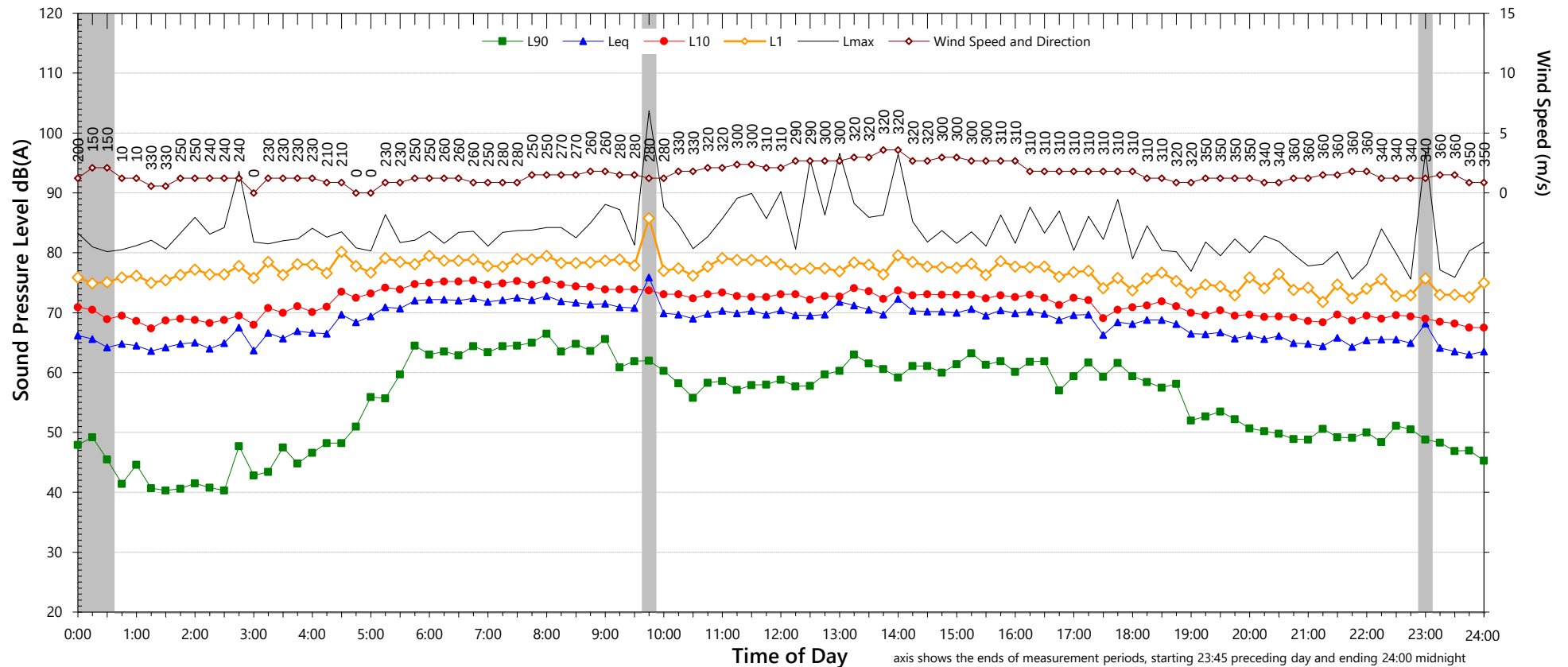
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	72	71
L _{Aeq} 1hr upper 10 percentile	72	74
L _{Aeq} 1hr lower 10 percentile	71	67

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Wednesday, 9 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	58	49	42
L _{Aeq}	70	66	66

Night Time Maximum Noise Levels (see note 7)			
L _{AFMax} (Range)	80	to	92
L _{AFMax} - L _{Aeq} (Range)	17	to	23

Notes:

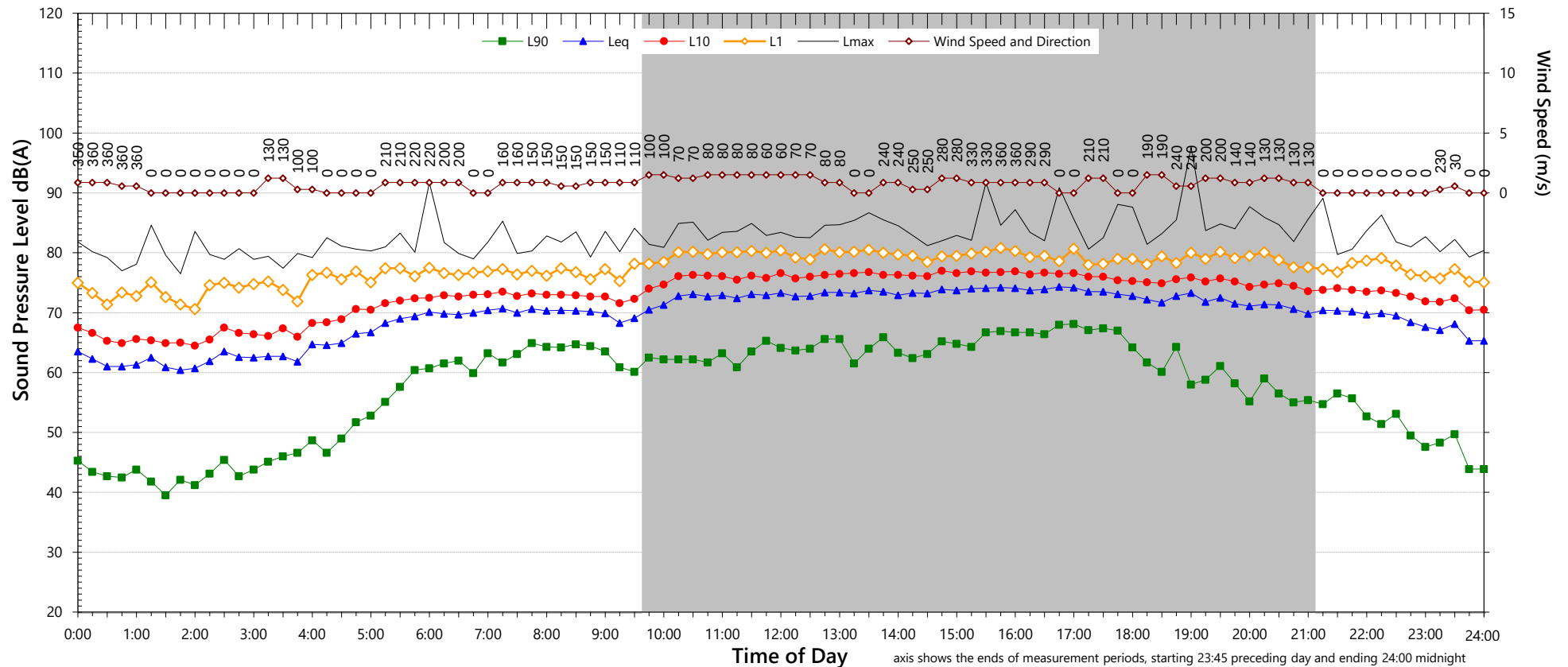
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	72	68
L _{Aeq} 1hr upper 10 percentile	74	72
L _{Aeq} 1hr lower 10 percentile	68	64

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Thursday, 10 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	-	-	42
L _{Aeq}	-	-	69

Night Time Maximum Noise Levels		(see note 7)	
L _{AFMax} (Range)	82	to	97
L _{AFMax} - L _{Aeq} (Range)	16	to	28

Notes:

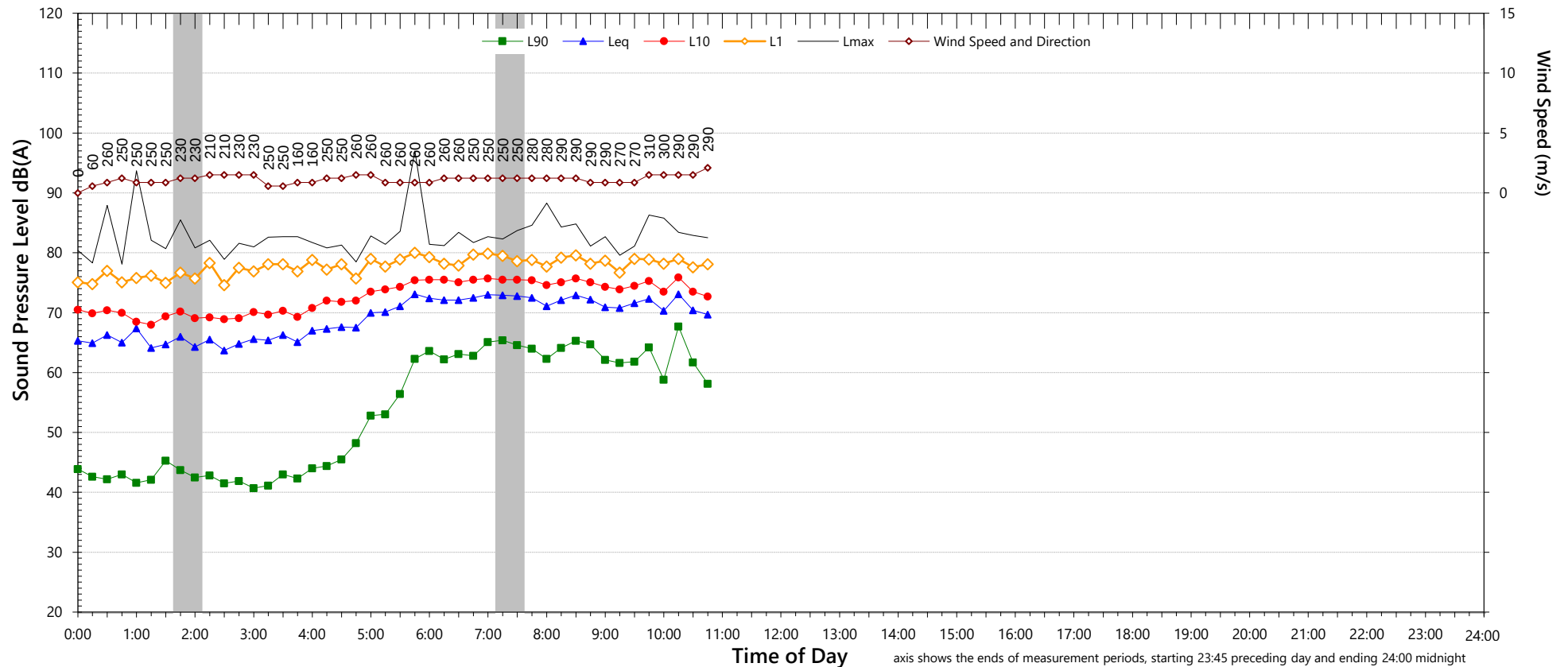
- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- "Night" relates to period from 10pm on this graph to morning on the following graph.
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	73	71
L _{Aeq} 1hr upper 10 percentile	73	74
L _{Aeq} 1hr lower 10 percentile	72	67

Unattended Noise Monitoring Results

62 Moorebank Avenue - Front Yard

Friday, 11 June 2021



NSW Noise Policy for Industry (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4,5}
L _{A90} ABL	-	-	-
L _{Aeq}	-	-	-

Night Time Maximum Noise Levels (see note 7)			
L _{AFMax} (Range)	-	to	-
L _{AFMax} - L _{Aeq} (Range)	-	to	-

Notes:

- Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.
- "Day" is the period from 8am till 6pm on Sundays and 7am till 6pm on other days
- "Evening" is the period from 6pm till 10pm
- "Night" relates to the remaining periods
- Graphed data measured in free-field; tabulated results facade corrected
- 1-hour values for L_{AFMax} are shown only where L_{AFMax} > 65dB(A) and where L_{AFMax} - L_{Aeq} ≥ 15dB(A)

NSW Road Noise Policy (1m from facade) (see note 6)		
Descriptor	Day	Night ⁵
	7am-10pm	10pm-7am
L _{Aeq} 15 hr and L _{Aeq} 9 hr	-	-
L _{Aeq} 1hr upper 10 percentile	-	-
L _{Aeq} 1hr lower 10 percentile	-	-