MOVEMENT SUMMARY
Site: I-06 2030 MIMT \& SIMTA PM

Network: 2030 MIMT \&
SIMTA PM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo V | Demand Flows |  | Arrival Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  | Total | HV |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1010 | 2.9 | 894 | 3.0 | 0.510 | 22.5 | LOS B | 13.3 | 95.4 | 0.57 | 0.75 | 39.9 |
| 3 R2 | 976 | 11.8 | 868 | 12.3 | 1.145 | 188.7 | LOS F | 16.6 | 130.6 | 1.00 | 1.42 | 15.9 |
| Approach | 1986 | 7.3 | 1762 N1 | 7.6 | 1.145 | 104.4 | LOS F | 16.6 | 130.6 | 0.78 | 1.08 | 20.7 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1280 | 7.8 | 1280 | 7.8 | 1.124 | 204.6 | LOS F | 82.4 | 625.2 | 1.00 | 1.34 | 14.2 |
| 5 T1 | 1373 | 4.8 | 1373 | 4.8 | 0.923 | 51.1 | LOS D | 42.7 | 311.4 | 1.00 | 1.04 | 43.3 |
| Approach | 2653 | 6.3 | 2653 | 6.3 | 1.124 | 125.1 | LOS F | 82.4 | 625.2 | 1.00 | 1.18 | 24.6 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1129 | 4.0 | 1129 | 4.0 | 0.442 | 9.3 | LOS A | 14.6 | 105.8 | 0.50 | 0.45 | 62.9 |
| 12 R2 | 1120 | 2.8 | 1120 | 2.8 | 1.202 | 235.3 | LOS F | 75.3 | 539.6 | 1.00 | 1.47 | 8.1 |
| Approach | 2249 | 3.4 | 2249 | 3.4 | 1.202 | 121.9 | LOS F | 75.3 | 539.6 | 0.75 | 0.96 | 22.3 |
| All Vehicles | 6888 | 5.6 | 6665 N1 | 5.8 | 1.202 | 118.5 | LOS F | 82.4 | 625.2 | 0.86 | 1.08 | 22.9 |

## PHASING SUMMARY

Site: I-06 2030 MIMT \& SIMTA PM
\$ ${ }^{\phi}$ Network: 2030 MIMT \&
SIMTA PM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=116$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | C | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 44 | 76 |
| Green Time (sec) | 38 | 26 | 34 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 44 | 32 | 40 |
| Phase Split | $38 \%$ | $28 \%$ | $34 \%$ |

## I-07 Intersection of Moorebank Avenue and Heathcote Road

## MOVEMENT SUMMARY

Site: I-07 2030 MIMT \& SIMTA AM
\$ Network: 2030 MIMT \& SIMTA AM
Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand <br> Total | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Arrival Total | Flows HV | Deg. Satn | Average Delay | Level of Service | 95\% Bac <br> Vehicles | of Queue Distance | Prop. Queued | Effective Stop Rate | Average Speed |
|  | veh/h | \% | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1958 | 7.5 | 1760 | 7.6 | 1.159 | 190.5 | LOS F | 58.2 | 440.6 | 1.00 | 1.83 | 5.0 |
| 3 R2 | 23 | 18.2 | 21 | 18.4 | 0.188 | 71.8 | LOS F | 1.3 | 10.9 | 0.98 | 0.71 | 30.6 |
| Approach | 1981 | 7.6 | 1781 N1 | 7.7 | 1.159 | 189.1 | LOS F | 58.2 | 440.6 | 1.00 | 1.82 | 5.2 |
| East: Heathcote Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 29 | 57.1 | 29 | 57.1 | 1.444 | 484.6 | LOS F | 103.0 | 775.7 | 1.00 | 1.95 | 6.8 |
| 6 R2 | 952 | 5.9 | 952 | 5.9 | 1.444 | 484.5 | LOS F | 103.0 | 775.7 | 1.00 | 1.96 | 6.7 |
| Approach | 981 | 7.4 | 981 | 7.4 | 1.444 | 484.5 | LOS F | 103.0 | 775.7 | 1.00 | 1.96 | 6.7 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 795 | 7.9 | 612 | 9.0 | 0.379 | 10.7 | LOS A | 12.2 | 91.7 | 0.54 | 0.71 | 51.4 |
| 8 T1 | 833 | 19.3 | 653 | 21.6 | 0.384 | 21.5 | LOS B | 12.9 | 108.7 | 0.66 | 0.58 | 13.1 |
| Approach | 1628 | 13.7 | $1266{ }^{\text {N1 }}$ | 15.5 | 0.384 | 16.3 | LOS B | 12.9 | 108.7 | 0.60 | 0.64 | 40.9 |
| All Vehicles | 4591 | 9.7 | $4028{ }^{\text {N1 }}$ | 11.1 | 1.444 | 206.7 | LOS F | 103.0 | 775.7 | 0.87 | 1.48 | 8.5 |

PHASING SUMMARY
Site: I-07 2030 MIMT \& SIMTA AM
蜔 Network: 2030 MIMT \& SIMTA AM
Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am Signals - Fixed Time Cycle Time $=133$ seconds (User-Given Phase Times)

Phase Timing Results

| Phase | B | A | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 15 | 88 |
| Green Time (sec) | 9 | 67 | 39 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 15 | 73 | 45 |
| Phase Split | $11 \%$ | $55 \%$ | $34 \%$ |

MOVEMENT SUMMARY
Site: I-07 2030 MIMT \& SIMTA PM

Network: 2030 MIMT \& SIMTA PM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo V | Demand Flows Total HV veh/h <br> \% |  | Arrival Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1204 | 9.6 |  |  |  | 1204 | 9.6 | 0.957 | 65.1 | LOS E | 53.3 | 408.1 | 0.98 | 1.23 | 12.6 |
| $3 \quad \mathrm{R} 2$ | 48 | 8.7 | 48 | 8.7 | 0.401 | 64.7 | LOS E | 2.8 | 20.9 | 1.00 | 0.74 | 32.2 |
| Approach | 1252 | 9.5 | 1252 | 9.5 | 0.957 | 65.1 | LOS E | 53.3 | 408.1 | 0.98 | 1.21 | 13.9 |
| East: Heathcote Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 76 | 19.4 | 76 | 19.4 | 1.426 | 440.1 | LOS F | 93.9 | 698.6 | 1.00 | 2.00 | 7.3 |
| 6 R2 | 812 | 5.2 | 812 | 5.2 | 1.426 | 439.3 | LOS F | 93.9 | 698.6 | 1.00 | 2.01 | 7.4 |
| Approach | 887 | 6.4 | 887 | 6.4 | 1.426 | 439.4 | LOS F | 93.9 | 698.6 | 1.00 | 2.01 | 7.4 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 884 | 3.7 | 762 | 3.7 | 0.359 | 7.5 | LOS A | 5.0 | 36.5 | 0.24 | 0.61 | 53.8 |
| 8 T1 | 1491 | 6.5 | 1286 | 6.6 | 0.670 | 6.3 | LOS A | 11.8 | 88.1 | 0.35 | 0.32 | 29.3 |
| Approach | 2375 | 5.5 | $2048{ }^{\text {N1 }}$ | 5.5 | 0.670 | 6.7 | LOS A | 11.8 | 88.1 | 0.31 | 0.43 | 48.4 |
| All Vehicles | 4514 | 6.8 | 4188 N1 | 7.3 | 1.426 | 115.8 | LOS F | 93.9 | 698.6 | 0.66 | 1.00 | 13.3 |

## PHASING SUMMARY

Site: I-07 2030 MIMT \& SIMTA PM

蛆 Network: 2030 MIMT \& SIMTA PM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=116$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | B | A | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 14 | 80 |
| Green Time (sec) | 8 | 60 | 30 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 14 | 66 | 36 |
| Phase Split | $12 \%$ | $57 \%$ | $31 \%$ |

Phase B

## I-08 Intersection of Moorebank Avenue and Industry Park Access

## MOVEMENT SUMMARY

Site: I-08 2030 MIMT \& SIMTA AM
\$ゆ Network: 2030 MIMT \& SIMTA AM
Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=133$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | $\begin{aligned} & \text { Demand Flows } \\ & \text { Total HV } \end{aligned}$ | Arrival Total | Flows HV | Deg. Satn | Average Delay | Level of Service | 95\% Bac <br> Vehicles | of Queue Distance | Prop. Queued | Effective Stop Rate | Average Speed |
|  | veh/h \% | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | $91 \quad 3.5$ | 91 | 3.5 | 0.056 | 6.1 | LOS A | 0.4 | 2.6 | 0.12 | 0.58 | 43.1 |
| 2 T1 | 19396.9 | 1939 | 6.9 | 1.268 | 303.8 | LOS F | 172.8 | 1301.0 | 1.00 | 2.26 | 5.4 |
| Approach | 20306.8 | 2030 | 6.8 | 1.268 | 290.5 | LOS F | 172.8 | 1301.0 | 0.96 | 2.19 | 5.7 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 74518.9 | 583 | 20.9 | 0.208 | 2.5 | LOS A | 3.8 | 32.4 | 0.22 | 0.20 | 56.9 |
| 9 R2 | $65 \quad 38.7$ | 52 | 41.6 | 0.992 | 106.2 | LOS F | 4.3 | 41.1 | 1.00 | 1.02 | 12.5 |
| Approach | 81020.5 | 635 N1 | 22.6 | 0.992 | 11.0 | LOS A | 4.3 | 41.1 | 0.29 | 0.26 | 47.3 |
| West: Industry Park Access (W) |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3462.5 | 34 | 62.5 | 0.415 | 64.9 | LOS E | 2.3 | 24.3 | 0.95 | 0.73 | 9.6 |
| 12 R2 | 5872.9 | 58 | 72.9 | 0.415 | 68.1 | LOS E | 2.7 | 31.5 | 0.98 | 0.73 | 19.8 |
| Approach | 9269.1 | 92 | 69.1 | 0.415 | 66.9 | LOS E | 2.7 | 31.5 | 0.97 | 0.73 | 16.8 |
| All Vehicles | 293212.5 | 2757 N1 | 13.3 | 1.268 | 218.7 | LOS F | 172.8 | 1301.0 | 0.81 | 1.69 | 8.0 |

## PHASING SUMMARY

Site: I-08 2030 MIMT \& SIMTA AM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=133$ seconds (User-Given Phase Times)

| Phase Timing Results |  |  |
| :--- | :---: | :---: |
| Phase | A | C |
| Reference Phase | Yes | No |
| Phase Change Time (sec) | 0 | 116 |
| Green Time (sec) | 110 | 11 |
| Yellow Time (sec) | 4 | 4 |
| All-Red Time (sec) | 2 | 2 |
| Phase Time (sec) | 116 | 17 |
| Phase Split | $87 \%$ | $13 \%$ |

Phase A

## MOVEMENT SUMMARY

Site: I-08 2030 MIMT \& SIMTA PM

Network: 2030 MIMT \&
SIMTA PM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=65$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo V | Demand Flows Total HV veh/h \% |  | Arrival Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 30.3 |  |  |  | 11 | 30.3 | 0.010 | 6.8 | LOS A | 0.0 | 0.4 | 0.22 | 0.57 | 42.7 |
| 2 T1 | 1173 | 8.9 | 1173 | 8.9 | 0.500 | 5.1 | LOS A | 9.5 | 72.0 | 0.51 | 0.45 | 51.3 |
| Approach | 1184 | 9.1 | 1184 | 9.1 | 0.500 | 5.1 | LOS A | 9.5 | 72.0 | 0.50 | 0.46 | 51.1 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1564 | 6.1 | 1342 | 6.1 | 0.521 | 5.2 | LOS A | 10.2 | 76.4 | 0.52 | 0.47 | 53.9 |
| 9 R2 | 25 | 62.5 | 22 | 62.3 | 0.131 | 15.0 | LOS B | 0.4 | 4.0 | 0.52 | 0.67 | 32.5 |
| Approach | 1589 | 7.0 | $1364{ }^{\text {N1 }}$ | 7.0 | 0.521 | 5.3 | LOS A | 10.2 | 76.4 | 0.52 | 0.47 | 53.6 |
| West: Industry Park Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 34 | 15.6 | 34 | 15.6 | 0.081 | 4.3 | LOS A | 0.3 | 2.4 | 0.38 | 0.44 | 26.2 |
| 12 R2 | 190 | 10.1 | 190 | 10.1 | 0.447 | 32.4 | LOS C | 3.0 | 22.9 | 0.97 | 0.76 | 28.1 |
| Approach | 223 | 11.0 | 223 | 11.0 | 0.447 | 28.2 | LOS B | 3.0 | 22.9 | 0.88 | 0.71 | 28.0 |
| All Vehicles | 2997 | 8.1 | 2771 N1 | 8.8 | 0.521 | 7.1 | LOS A | 10.2 | 76.4 | 0.54 | 0.48 | 49.1 |

## PHASING SUMMARY

Site: I-08 2030 MIMT \& SIMTA PM
\$ ${ }^{\phi}$ Network: 2030 MIMT \&

## SIMTA PM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=65$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | C |
| :--- | :---: | :---: |
| Reference Phase | Yes | No |
| Phase Change Time (sec) | 0 | 51 |
| Green Time (sec) | 45 | 8 |
| Yellow Time (sec) | 4 | 4 |
| All-Red Time (sec) | 2 | 2 |
| Phase Time (sec) | 51 | 14 |
| Phase Split | $78 \%$ | $22 \%$ |



## I-09 Intersection of Moorebank Avenue and Church Road

## MOVEMENT SUMMARY

## Site: I-09 2030 MIMT \& SIMTA AM

Moorebank Avenue / Church Road
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| $2 \quad$ T1 | 2141 | 8.2 | 0.797 | 8.3 | LOS A | 12.4 | 94.2 | 0.15 | 0.11 | 52.2 |
| $3 \quad \mathrm{R} 2$ | 285 | 8.8 | 0.797 | 31.7 | LOS C | 12.4 | 94.2 | 1.00 | 0.74 | 37.6 |
| Approach | 2427 | 8.3 | 0.996 | 11.0 | NA | 12.4 | 94.2 | 0.25 | 0.18 | 49.9 |
| East: Church Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 205 | 16.1 | 0.270 | 7.7 | LOS A | 1.1 | 8.9 | 0.52 | 0.74 | 47.1 |
| 6 R2 | 7 | 0.0 | 0.945 | 803.3 | LOS F | 2.3 | 16.4 | 1.00 | 1.07 | 4.1 |
| Approach | 212 | 15.6 | 0.945 | 35.4 | LOS C | 2.3 | 16.4 | 0.53 | 0.76 | 34.7 |
| North: Moorebank Avenue ( N ) |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 37 | 0.0 | 0.242 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.05 | 57.7 |
| 8 T1 | 775 | 24.2 | 0.242 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.03 | 59.6 |
| Approach | 812 | 23.1 | 0.242 | 0.3 | NA | 0.0 | 0.0 | 0.00 | 0.03 | 59.5 |
| All Vehicles | 3450 | 12.2 | 0.996 | 10.0 | NA | 12.4 | 94.2 | 0.21 | 0.18 | 50.4 |

## MOVEMENT SUMMARY

Site: I-09 2030 MIMT \& SIMTA PM
Moorebank Avenue / Church Road
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1210 | 12.5 | 0.676 | 0.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 59.6 |
| 3 R2 | 112 | 14.2 | 0.711 | 54.5 | LOS D | 3.4 | 27.4 | 0.96 | 1.18 | 29.7 |
| Approach | 1322 | 12.6 | 0.711 | 4.8 | NA | 3.4 | 27.4 | 0.08 | 0.10 | 54.8 |
| East: Church Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 428 | 5.2 | 1.395 | 413.3 | LOS F | 91.9 | 676.1 | 1.00 | 5.42 | 7.5 |
| 6 R2 | 1 | 0.0 | 0.195 | 657.7 | LOS F | 0.5 | 3.3 | 1.00 | 1.00 | 5.0 |
| Approach | 429 | 5.2 | 1.395 | 413.9 | LOS F | 91.9 | 676.1 | 1.00 | 5.41 | 7.5 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 14 | 7.7 | 0.940 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 54.1 |
| 8 T1 | 1728 | 6.8 | 0.940 | 2.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 55.5 |
| Approach | 1741 | 6.8 | 0.940 | 2.4 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 55.5 |
| All Vehicles | 3492 | 8.8 | 1.395 | 53.8 | NA | 91.9 | 676.1 | 0.15 | 0.70 | 30.6 |

## I-10 Intersection of Heathcote Road and Nuwarra Road

## MOVEMENT SUMMARY

Site: I-10 2030 MIMT \& SIMTA AM
Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=131$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| SouthEast: Heathcote Road (SE) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 263 | 1.2 | 0.182 | 8.3 | LOS A | 3.5 | 25.0 | 0.27 | 0.63 | 48.2 |
| 5 T1 | 2073 | 5.3 | 1.258 | 288.3 | LOS F | 162.6 | 1189.8 | 1.00 | 2.15 | 10.3 |
| 6 R2 | 647 | 3.3 | 1.268 | 267.3 | LOS F | 42.9 | 308.4 | 1.00 | 1.54 | 11.2 |
| Approach | 2983 | 4.5 | 1.268 | 259.1 | LOS F | 162.6 | 1189.8 | 0.94 | 1.89 | 11.0 |
| NorthEast: Nuwarra Road (NE) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 416 | 4.8 | 0.484 | 24.5 | LOS B | 16.5 | 120.1 | 0.71 | 0.78 | 42.4 |
| 8 T1 | 264 | 8.0 | 0.423 | 53.3 | LOS D | 7.7 | 57.2 | 0.94 | 0.76 | 26.2 |
| 9 R2 | 508 | 5.8 | 1.436 | 477.0 | LOS F | 49.8 | 365.8 | 1.00 | 1.93 | 6.6 |
| Approach | 1188 | 5.9 | 1.436 | 224.6 | LOS F | 49.8 | 365.8 | 0.89 | 1.27 | 11.9 |
| NorthWest: Heathcote Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 254 | 11.6 | 0.334 | 21.5 | LOS B | 7.8 | 60.1 | 0.70 | 0.76 | 42.7 |
| 11 T1 | 1044 | 11.3 | 0.957 | 54.9 | LOS D | 42.9 | 329.5 | 0.90 | 0.97 | 31.2 |
| 12 R 2 | 235 | 6.3 | 0.786 | 75.4 | LOS F | 8.0 | 59.1 | 1.00 | 0.89 | 19.9 |
| Approach | 1532 | 10.6 | 0.957 | 52.5 | LOS D | 42.9 | 329.5 | 0.88 | 0.92 | 30.8 |
| SouthWest: Wattle Grove Drive (SW) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 639 | 2.1 | 0.849 | 51.8 | LOS D | 31.9 | 227.1 | 0.99 | 1.15 | 24.8 |
| 2 T1 | 543 | 4.5 | 0.817 | 61.8 | LOS E | 19.6 | 142.7 | 1.00 | 0.94 | 23.7 |
| 3 R 2 | 263 | 4.0 | 1.277 | 332.6 | LOS F | 42.3 | 306.5 | 1.00 | 1.80 | 6.6 |
| Approach | 1445 | 3.4 | 1.277 | 106.7 | LOS F | 42.3 | 306.5 | 0.99 | 1.19 | 16.1 |
| All Vehicles | 7148 | 5.8 | 1.436 | 178.3 | LOS F | 162.6 | 1189.8 | 0.93 | 1.44 | 13.9 |

## PHASING SUMMARY

Site: I-10 2030 MIMT \& SIMTA AM
Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 131 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | D | E | G |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No | No |
| Phase Change Time (sec) | 0 | 54 | 67 | 86 | 114 |
| Green Time (sec) | 48 | 7 | 13 | 22 | 11 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 54 | 13 | 19 | 28 | 17 |
| Phase Split | $41 \%$ | $10 \%$ | $15 \%$ | $21 \%$ | $13 \%$ |

PhaseA

## MOVEMENT SUMMARY

## Site: I-10 2030 MIMT \& SIMTA PM

Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=139$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective <br> Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| SouthEast: Heathcote Road (SE) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 337 | 2.5 | 0.282 | 15.4 | LOS B | 8.9 | 63.6 | 0.45 | 0.70 | 42.4 |
| 5 T1 | 1331 | 5.4 | 0.992 | 77.8 | LOS F | 59.5 | 436.2 | 0.93 | 1.13 | 26.0 |
| 6 R2 | 469 | 3.1 | 1.197 | 269.1 | LOS F | 34.2 | 246.1 | 1.00 | 1.49 | 11.2 |
| Approach | 2137 | 4.5 | 1.197 | 110.0 | LOS F | 59.5 | 436.2 | 0.87 | 1.14 | 20.5 |
| NorthEast: Nuwarra Road (NE) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 646 | 2.8 | 0.950 | 79.5 | LOS F | 47.1 | 337.5 | 1.00 | 1.22 | 26.0 |
| 8 T1 | 621 | 1.4 | 0.996 | 96.4 | LOS F | 29.6 | 209.3 | 1.00 | 1.17 | 18.0 |
| 9 R2 | 556 | 7.0 | 1.120 | 181.1 | LOS F | 35.9 | 266.2 | 1.00 | 1.30 | 14.7 |
| Approach | 1823 | 3.6 | 1.120 | 116.3 | LOS F | 47.1 | 337.5 | 1.00 | 1.23 | 18.9 |
| NorthWest: Heathcote Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 258 | 6.1 | 0.232 | 21.3 | LOS B | 8.5 | 62.5 | 0.53 | 0.73 | 43.0 |
| 11 T1 | 1701 | 2.7 | 1.170 | 222.2 | LOS F | 119.3 | 855.0 | 1.00 | 1.79 | 12.7 |
| 12 R 2 | 467 | 2.0 | 1.103 | 167.2 | LOS F | 28.6 | 203.5 | 1.00 | 1.24 | 11.1 |
| Approach | 2427 | 3.0 | 1.170 | 190.3 | LOS F | 119.3 | 855.0 | 0.95 | 1.57 | 13.5 |
| SouthWest: Wattle Grove Drive (SW) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 305 | 1.7 | 0.387 | 33.9 | LOS C | 14.1 | 100.1 | 0.76 | 0.85 | 30.6 |
| 2 T1 | 343 | 1.2 | 0.486 | 57.7 | LOS E | 10.6 | 75.1 | 0.96 | 0.79 | 24.7 |
| 3 R2 | 370 | 1.1 | 1.372 | 425.7 | LOS F | 69.2 | 489.1 | 1.00 | 1.93 | 5.3 |
| Approach | 1018 | 1.3 | 1.372 | 184.3 | LOS F | 69.2 | 489.1 | 0.91 | 1.22 | 10.7 |
| All Vehicles | 7405 | 3.3 | 1.372 | 148.1 | LOS F | 119.3 | 855.0 | 0.93 | 1.31 | 15.9 |

## PHASING SUMMARY

Site: I-10 2030 MIMT \& SIMTA PM
Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 139 seconds (User-Given Phase Times)
Phase Timing Results


## I-11 Intersection of Newbridge Road and Nuwarra Road

## MOVEMENT SUMMARY

Site: I-11 2030 MIMT \& SIMTA AM
Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Nuwarra Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 37 | 8.6 | 0.885 | 63.8 | LOS E | 26.8 | 190.9 | 0.91 | 0.97 | 33.4 |
| 2 T1 | 352 | 1.5 | 0.885 | 60.8 | LOS E | 26.8 | 190.9 | 0.91 | 0.97 | 28.1 |
| 3 R2 | 852 | 6.2 | 1.232 | 301.9 | LOS F | 72.5 | 534.1 | 1.00 | 1.53 | 11.1 |
| Approach | 1240 | 4.9 | 1.232 | 226.5 | LOS F | 72.5 | 534.1 | 0.97 | 1.36 | 13.8 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 353 | 16.7 | 0.649 | 28.2 | LOS B | 22.7 | 180.3 | 0.74 | 0.79 | 44.8 |
| 5 T1 | 1300 | 12.1 | 0.649 | 23.8 | LOS B | 23.3 | 181.4 | 0.69 | 0.64 | 50.9 |
| Approach | 1653 | 13.1 | 0.649 | 24.7 | LOS B | 23.3 | 181.4 | 0.70 | 0.67 | 49.6 |
| North: Nuwarra Road (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 8 | 0.0 | 0.995 | 114.7 | LOS F | 11.8 | 83.1 | 1.00 | 1.25 | 21.7 |
| 8 T1 | 156 | 0.7 | 1.244 | 158.6 | LOS F | 28.1 | 203.6 | 1.00 | 1.38 | 17.1 |
| $9 \quad \mathrm{R} 2$ | 142 | 5.2 | 1.244 | 308.8 | LOS F | 28.1 | 203.6 | 1.00 | 1.80 | 11.6 |
| Approach | 306 | 2.7 | 1.244 | 226.9 | LOS F | 28.1 | 203.6 | 1.00 | 1.57 | 13.9 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 305 | 2.1 | 1.166 | 220.5 | LOS F | 121.1 | 907.0 | 1.00 | 1.65 | 15.2 |
| 11 T1 | 2315 | 10.2 | 1.241 | 247.6 | LOS F | 145.7 | 1121.8 | 1.00 | 1.91 | 14.6 |
| Approach | 2620 | 9.2 | 1.241 | 244.4 | LOS F | 145.7 | 1121.8 | 1.00 | 1.88 | 14.6 |
| All Vehicles | 5820 | 9.1 | 1.244 | 177.3 | LOS F | 145.7 | 1121.8 | 0.91 | 1.41 | 18.0 |

## PHASING SUMMARY

Site: I-11 2030 MIMT \& SIMTA AM
Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 72 | 89 |
| Green Time (sec) | 66 | 11 | 45 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 72 | 17 | 51 |
| Phase Split | $51 \%$ | $12 \%$ | $36 \%$ |



## MOVEMENT SUMMARY

## 目 Site: I-11 2030 MIMT \& SIMTA PM

Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Deman | Fows | Deg. Satn | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
| v | Total | HV |  |  |  | Vehicles | Distance |  |  |  |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Nuwarra Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 58 | 7.3 | 0.783 | 71.7 | LOS F | 15.1 | 108.2 | 1.00 | 0.90 | 31.7 |
| 2 T1 | 159 | 0.7 | 0.783 | 67.3 | LOS E | 15.1 | 108.2 | 1.00 | 0.90 | 28.8 |
| 3 R 2 | 574 | 6.2 | 1.027 | 132.8 | LOS F | 29.1 | 214.6 | 1.00 | 1.15 | 20.6 |
| Approach | 791 | 5.2 | 1.027 | 115.2 | LOS F | 29.1 | 214.6 | 1.00 | 1.08 | 22.5 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 766 | 3.8 | 0.792 | 18.4 | LOS B | 33.7 | 245.5 | 0.60 | 0.79 | 50.1 |
| 5 T1 | 2239 | 6.4 | 0.792 | 16.7 | LOS B | 41.2 | 306.8 | 0.67 | 0.65 | 55.4 |
| Approach | 3006 | 5.8 | 0.792 | 17.1 | LOS B | 41.2 | 306.8 | 0.65 | 0.69 | 54.0 |
| North: Nuwarra Road (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 18 | 0.0 | 0.876 | 76.8 | LOS F | 18.0 | 127.2 | 1.00 | 1.02 | 28.9 |
| 8 T1 | 296 | 1.1 | 1.094 | 100.2 | LOS F | 33.9 | 240.3 | 1.00 | 1.11 | 23.6 |
| $9 \quad \mathrm{R} 2$ | 213 | 1.5 | 1.094 | 190.2 | LOS F | 33.9 | 240.3 | 1.00 | 1.39 | 17.1 |
| Approach | 526 | 1.2 | 1.094 | 135.8 | LOS F | 33.9 | 240.3 | 1.00 | 1.22 | 20.4 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 103 | 0.0 | 0.551 | 21.6 | LOS B | 17.8 | 132.7 | 0.51 | 0.52 | 48.4 |
| 11 T1 | 1695 | 8.6 | 0.626 | 14.8 | LOS B | 20.7 | 156.5 | 0.51 | 0.47 | 56.8 |
| Approach | 1798 | 8.1 | 0.626 | 15.2 | LOS B | 20.7 | 156.5 | 0.51 | 0.48 | 56.3 |
| All Vehicles | 6121 | 6.0 | 1.094 | 39.4 | LOS C | 41.2 | 306.8 | 0.68 | 0.72 | 41.7 |

## PHASING SUMMARY

Site: I-11 2030 MIMT \& SIMTA PM
Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 84 | 112 |
| Green Time (sec) | 78 | 22 | 22 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 84 | 28 | 28 |
| Phase Split | $60 \%$ | $20 \%$ | $20 \%$ |

Phase $A$

## I-12 Intersection of Newbridge Road and Governor Macquarie Drive

## MOVEMENT SUMMARY

Site: I-12 2030 MIMT \& SIMTA AM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Brickmakers Drive (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 0.0 | 0.909 | 84.6 | LOS F | 17.3 | 122.1 | 1.00 | 1.07 | 24.1 |
| 2 T1 | 207 | 1.0 | 0.909 | 80.3 | LOS F | 17.3 | 122.1 | 1.00 | 1.07 | 23.8 |
| 3 R 2 | 720 | 1.2 | 1.239 | 301.6 | LOS F | 55.9 | 395.6 | 1.00 | 1.68 | 12.6 |
| Approach | 941 | 1.1 | 1.239 | 249.7 | LOS F | 55.9 | 395.6 | 1.00 | 1.53 | 13.8 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 242 | 3.0 | 0.178 | 7.9 | LOS A | 2.2 | 15.7 | 0.19 | 0.64 | 58.1 |
| 5 T1 | 1486 | 11.6 | 0.436 | 14.0 | LOS A | 16.9 | 131.3 | 0.55 | 0.50 | 59.8 |
| 6 R2 | 683 | 9.9 | 1.050 | 154.1 | LOS F | 36.1 | 274.4 | 1.00 | 1.16 | 23.9 |
| Approach | 2411 | 10.3 | 1.050 | 53.1 | LOS D | 36.1 | 274.4 | 0.64 | 0.70 | 41.6 |
| North: Governor Macquarie Drive (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 765 | 7.8 | 0.725 | 52.8 | LOS D | 23.4 | 174.6 | 0.96 | 0.86 | 40.2 |
| 8 T1 | 135 | 2.3 | 0.546 | 64.2 | LOS E | 8.8 | 62.9 | 0.99 | 0.79 | 27.0 |
| $9 \quad \mathrm{R} 2$ | 179 | 31.8 | 1.033 | 140.2 | LOS F | 18.4 | 163.5 | 1.00 | 1.19 | 20.3 |
| Approach | 1079 | 11.1 | 1.033 | 68.7 | LOS E | 23.4 | 174.6 | 0.97 | 0.91 | 34.3 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 132 | 29.9 | 1.230 | 272.6 | LOS F | 162.7 | 1251.6 | 1.00 | 1.93 | 12.8 |
| 11 T1 | 3017 | 7.7 | 1.230 | 265.2 | LOS F | 167.1 | 1257.9 | 1.00 | 1.97 | 16.6 |
| 12 R 2 | 5 | 20.0 | 0.046 | 33.1 | LOS C | 0.2 | 1.8 | 0.60 | 0.68 | 37.8 |
| Approach | 3155 | 8.6 | 1.230 | 265.1 | LOS F | 167.1 | 1257.9 | 1.00 | 1.97 | 16.4 |
| All Vehicles | 7585 | 8.6 | 1.239 | 167.9 | LOS F | 167.1 | 1257.9 | 0.88 | 1.36 | 21.9 |

## PHASING SUMMARY

Site: I-12 2030 MIMT \& SIMTA AM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)


## MOVEMENT SUMMARY

## Site: I-12 2030 MIMT \& SIMTA PM

Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand | Flows | Deg. Satn | Average | Level of | 95\% Bac | of Queue | Prop. | Effective | Average |
|  | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Brickmakers Drive (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 0.0 | 0.554 | 70.4 | LOS E | 7.2 | 52.4 | 1.00 | 0.79 | 26.8 |
| 2 T1 | 97 | 5.4 | 0.554 | 66.3 | LOS E | 7.2 | 52.4 | 1.00 | 0.79 | 26.5 |
| 3 R2 | 271 | 0.8 | 0.641 | 70.4 | LOS E | 9.1 | 64.3 | 1.00 | 0.81 | 32.5 |
| Approach | 378 | 1.9 | 0.641 | 69.3 | LOS E | 9.1 | 64.3 | 1.00 | 0.81 | 31.0 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 688 | 1.4 | 0.484 | 9.5 | LOS A | 8.3 | 58.5 | 0.29 | 0.70 | 57.0 |
| 5 T1 | 2771 | 5.2 | 0.935 | 33.0 | LOS C | 56.1 | 412.9 | 0.76 | 0.79 | 50.0 |
| 6 R2 | 744 | 10.3 | 1.124 | 214.3 | LOS F | 48.3 | 368.3 | 1.00 | 1.29 | 19.1 |
| Approach | 4204 | 5.5 | 1.124 | 61.3 | LOS E | 56.1 | 412.9 | 0.73 | 0.87 | 39.1 |
| North: Governor Macquarie Drive (N) |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 614 | 7.9 | 0.463 | 46.7 | LOS D | 16.6 | 124.4 | 0.86 | 0.81 | 42.0 |
| 8 T1 | 314 | 1.7 | 1.055 | 145.7 | LOS F | 32.6 | 231.3 | 1.00 | 1.33 | 16.2 |
| $9 \quad \mathrm{R} 2$ | 306 | 36.0 | 1.608 | 636.0 | LOS F | 70.5 | 648.6 | 1.00 | 2.02 | 6.1 |
| Approach | 1233 | 13.3 | 1.608 | 218.1 | LOS F | 70.5 | 648.6 | 0.93 | 1.25 | 16.2 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 175 | 15.4 | 0.862 | 46.2 | LOS D | 45.6 | 343.3 | 0.94 | 0.89 | 39.0 |
| 11 T1 | 2076 | 5.9 | 0.862 | 38.2 | LOS C | 46.2 | 341.9 | 0.92 | 0.87 | 47.7 |
| 12 R2 | 4 | 0.0 | 0.071 | 56.2 | LOS D | 0.2 | 1.7 | 0.81 | 0.69 | 29.8 |
| Approach | 2255 | 6.6 | 0.862 | 38.9 | LOS C | 46.2 | 343.3 | 0.92 | 0.87 | 47.0 |
| All Vehicles | 8070 | 6.8 | 1.608 | 79.3 | LOS F | 70.5 | 648.6 | 0.82 | 0.92 | 33.9 |

## PHASING SUMMARY

Site: I-12 2030 MIMT \& SIMTA PM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 140 seconds (User-Given Phase Times)
Phase Timing Results


## I-13 Intersection of Moorebank Avenue and M5 Motorway

## MOVEMENT SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 1 AM
Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA Opt 1 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 74 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Total veh/h | lows HV \% | Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 422 | 39.9 | 0.471 | 10.7 | LOS A | 5.4 | 58.4 | 0.50 | 0.72 | 48.3 |
| 2 T1 | 727 | 11.8 | 0.897 | 43.1 | LOS D | 16.2 | 130.3 | 1.00 | 1.12 | 33.7 |
| 3 R2 | 322 | 7.1 | 0.470 | 33.6 | LOS C | 5.8 | 43.9 | 0.91 | 0.79 | 36.6 |
| Approach | 1471 | 18.8 | 0.897 | 31.7 | LOS C | 16.2 | 130.3 | 0.84 | 0.93 | 37.6 |
| East: M5 Motorway on\&off ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 307 | 17.6 | 0.410 | 11.7 | LOS A | 4.4 | 37.6 | 0.61 | 0.74 | 48.3 |
| 6 R2 | 237 | 6.2 | 0.246 | 28.8 | LOS C | 3.4 | 25.1 | 0.82 | 0.76 | 40.4 |
| Approach | 543 | 12.6 | 0.410 | 19.2 | LOS B | 4.4 | 37.6 | 0.70 | 0.74 | 44.3 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 51 | 47.9 | 0.050 | 7.9 | LOS A | 0.4 | 3.5 | 0.29 | 0.60 | 51.1 |
| 8 T1 | 246 | 22.8 | 0.328 | 26.4 | LOS B | 3.8 | 34.1 | 0.88 | 0.70 | 40.6 |
| 9 R2 | 454 | 25.5 | 0.772 | 37.8 | LOS C | 10.0 | 85.2 | 0.97 | 0.88 | 36.3 |
| Approach | 750 | 26.1 | 0.772 | 32.0 | LOS C | 10.0 | 85.2 | 0.90 | 0.80 | 38.3 |
| West: M5 Motorway on\&off ramp (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1722 | 7.5 | 0.977 | 8.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.50 | 51.2 |
| 12 R2 | 640 | 24.9 | 0.804 | 39.2 | LOS C | 12.4 | 117.7 | 0.99 | 0.96 | 34.5 |
| Approach | 2362 | 12.2 | 0.977 | 16.6 | LOS B | 12.4 | 117.7 | 0.27 | 0.62 | 45.6 |
| All Vehicles | 5125 | 16.2 | 0.977 | 23.4 | LOS B | 16.2 | 130.3 | 0.57 | 0.75 | 41.9 |

## PHASING SUMMARY

## Site: I-13 2030 MIMT \& SIMTA AM

Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=74$ seconds (User-Given Phase Times)

| Phase Timing Results | A | E | F |
| :--- | :---: | :---: | :---: |
| Phase | Yes | No | No |
| Reference Phase | 0 | 24 | 51 |
| Phase Change Time (sec) | 17 | 20 | 16 |
| Green Time (sec) | 4 | 4 | 4 |
| Yellow Time (sec) | 3 | 3 | 3 |
| All-Red Time (sec) | 24 | 27 | 23 |
| Phase Time (sec) | $32 \%$ | $36 \%$ | $31 \%$ |
| Phase Split |  |  |  |



## MOVEMENT SUMMARY

## Site: I-13 2030 MIMT \& SIMTA PM

Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=94$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  | Total | HV |  |  |  | Vehicles | Distance |  |  |  |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 558 | 26.8 | 0.882 | 39.6 | LOS C | 26.4 | 255.6 | 0.98 | 1.00 | 34.2 |
| 2 T1 | 232 | 18.8 | 0.935 | 64.8 | LOS E | 6.7 | 58.0 | 1.00 | 1.09 | 27.6 |
| 3 R2 | 382 | 13.7 | 0.356 | 29.3 | LOS C | 7.1 | 59.0 | 0.77 | 0.77 | 38.2 |
| Approach | 1172 | 20.9 | 0.935 | 41.2 | LOS C | 26.4 | 255.6 | 0.91 | 0.94 | 33.8 |
| East: M5 Motorway on\&off ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 466 | 8.6 | 0.601 | 18.7 | LOS B | 10.5 | 81.4 | 0.74 | 0.83 | 44.1 |
| 6 R2 | 97 | 21.7 | 0.177 | 42.7 | LOS D | 2.0 | 16.2 | 0.89 | 0.73 | 34.9 |
| Approach | 563 | 10.8 | 0.601 | 22.8 | LOS B | 10.5 | 81.4 | 0.77 | 0.81 | 42.1 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 139 | 6.1 | 0.115 | 7.5 | LOS A | 1.2 | 8.7 | 0.28 | 0.62 | 52.6 |
| 8 T1 | 767 | 8.7 | 0.865 | 46.1 | LOS D | 19.7 | 152.7 | 1.00 | 1.03 | 32.7 |
| 9 R2 | 1488 | 7.0 | 0.920 | 43.0 | LOS D | 34.3 | 254.6 | 1.00 | 1.06 | 34.8 |
| Approach | 2394 | 7.5 | 0.920 | 42.0 | LOS C | 34.3 | 254.6 | 0.96 | 1.03 | 34.8 |
| West: M5 Motorway on\&off ramp (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 620 | 13.8 | 0.367 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 54.4 |
| 12 R2 | 400 | 38.7 | 0.895 | 63.3 | LOS E | 11.3 | 122.5 | 1.00 | 1.06 | 27.4 |
| Approach | 1020 | 23.6 | 0.895 | 28.3 | LOS B | 11.3 | 122.5 | 0.39 | 0.73 | 40.0 |
| All Vehicles | 5150 | 14.1 | 0.935 | 37.0 | LOS C | 34.3 | 255.6 | 0.82 | 0.93 | 36.2 |

## PHASING SUMMARY

## Site: I-13 2030 MIMT \& SIMTA PM

Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 94 seconds (User-Given Phase Times)
Phase Timing Results


## I-14 Intersection of M5 Motorway and Hume Highway

## MOVEMENT SUMMARY

Site: I-14 2030 MIMT \& SIMTA AM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=159$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 4256 | 4.6 | 1.027 | 59.4 | LOS E | 152.3 | 1108.5 | 1.00 | 1.21 | 33.2 |
| 3 R2 | 665 | 4.1 | 0.916 | 46.9 | LOS D | 19.1 | 138.5 | 1.00 | 0.93 | 36.6 |
| Approach | 4921 | 4.5 | 1.027 | 57.7 | LOS E | 152.3 | 1108.5 | 1.00 | 1.17 | 33.6 |
| East: M5 Motorway on\&off-ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 338 | 5.9 | 0.134 | 30.5 | LOS C | 4.8 | 35.4 | 0.60 | 0.71 | 41.9 |
| 6 R2 | 1218 | 6.9 | 1.300 | 368.7 | LOS F | 75.9 | 573.8 | 1.00 | 1.55 | 7.1 |
| Approach | 1556 | 6.7 | 1.300 | 295.3 | LOS F | 75.9 | 573.8 | 0.91 | 1.37 | 9.3 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 770 | 10.7 | 0.617 | 13.6 | LOS A | 24.1 | 189.6 | 0.52 | 0.73 | 46.0 |
| 8 T1 | 1208 | 6.7 | 0.490 | 28.5 | LOS B | 17.8 | 131.7 | 0.62 | 0.55 | 43.3 |
| Approach | 1978 | 8.3 | 0.617 | 22.7 | LOS B | 24.1 | 189.6 | 0.58 | 0.62 | 44.1 |
| All Vehicles | 8455 | 5.8 | 1.300 | 93.3 | LOS F | 152.3 | 1108.5 | 0.89 | 1.08 | 25.2 |

## PHASING SUMMARY

Site: I-14 2030 MIMT \& SIMTA AM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)

## Phase Timing Results

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | No | No | No | Yes |
| Phase Change Time (sec) | 20 | 97 | 123 | 0 |
| Green Time (sec) | 70 | 19 | 29 | 13 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 | 3 |
| Phase Time (sec) | 77 | 26 | 36 | 20 |
| Phase Split | $48 \%$ | $16 \%$ | $23 \%$ | $13 \%$ |

Phase A

## MOVEMENT SUMMARY

## Site: I-14 2030 MIMT \& SIMTA PM

M5 Motorway / Hume Highway
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 2555 | 3.9 | 0.624 | 2.2 | LOS A | 7.1 | 51.1 | 0.12 | 0.11 | 58.3 |
| 3 R2 | 401 | 1.8 | 1.023 | 122.1 | LOS F | 20.4 | 145.1 | 1.00 | 1.07 | 22.6 |
| Approach | 2956 | 3.6 | 1.023 | 18.4 | LOS B | 20.4 | 145.1 | 0.24 | 0.24 | 48.0 |
| East: M5 Motorway on\&off-ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1487 | 3.4 | 1.119 | 230.2 | LOS F | 93.0 | 670.0 | 1.00 | 1.30 | 14.5 |
| 6 R2 | 1245 | 6.7 | 1.267 | 340.5 | LOS F | 76.0 | 573.3 | 1.00 | 1.51 | 7.6 |
| Approach | 2733 | 4.9 | 1.267 | 280.5 | LOS F | 93.0 | 670.0 | 1.00 | 1.40 | 10.9 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 895 | 6.9 | 0.712 | 14.9 | LOS B | 28.0 | 213.6 | 0.62 | 0.82 | 45.3 |
| 8 T1 | 2837 | 2.4 | 0.870 | 20.5 | LOS B | 51.6 | 368.7 | 0.78 | 0.73 | 47.0 |
| Approach | 3732 | 3.5 | 0.870 | 19.2 | LOS B | 51.6 | 368.7 | 0.74 | 0.75 | 46.7 |
| All Vehicles | 9421 | 3.9 | 1.267 | 94.7 | LOS F | 93.0 | 670.0 | 0.66 | 0.78 | 25.0 |

## PHASING SUMMARY

Site: I-14 2030 MIMT \& SIMTA PM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)

Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 97 | 121 |
| Green Time (sec) | 90 | 17 | 31 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 |
| Phase Time (sec) | 97 | 24 | 38 |
| Phase Split | $61 \%$ | $15 \%$ | $24 \%$ |

Phase A

## I-15 Intersection of Cambridge Avenue and Canterbury Road MOVEMENT SUMMARY

Site: I-15 2030 MIMT \& SIMTA OPT 1 AM
Canterbury Road / Cambridge Avenue / Glenfield Road 2030 MIMT \& SIMTA Opt 1 AM PEAK 7:45 am - 8:45 am
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Canterbury Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 449 | 3.5 | 0.498 | 6.0 | LOS A | 3.1 | 22.3 | 0.59 | 0.68 | 52.9 |
| 2 T1 | 8 | 0.0 | 0.859 | 9.3 | LOS A | 13.9 | 98.6 | 0.90 | 0.90 | 49.9 |
| $3 \quad \mathrm{R} 2$ | 1058 | 2.0 | 0.859 | 14.7 | LOS B | 13.9 | 98.6 | 0.90 | 0.90 | 50.0 |
| Approach | 1516 | 2.4 | 0.859 | 12.1 | LOS A | 13.9 | 98.6 | 0.81 | 0.84 | 50.7 |
| East: Cambridge Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 307 | 3.1 | 0.163 | 3.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.43 | 56.5 |
| 5 T1 | 81 | 7.8 | 0.084 | 5.2 | LOS A | 0.5 | 3.6 | 0.52 | 0.57 | 53.4 |
| 6 R2 | 54 | 9.8 | 0.084 | 10.5 | LOS A | 0.5 | 3.6 | 0.52 | 0.59 | 53.7 |
| Approach | 442 | 4.8 | 0.163 | 4.6 | LOS A | 0.5 | 3.6 | 0.16 | 0.48 | 55.6 |
| North: Railway Parade (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 328 | 0.6 | 0.801 | 39.4 | LOS C | 10.1 | 70.9 | 1.00 | 1.36 | 36.3 |
| 8 T1 | 3 | 0.0 | 0.578 | 26.9 | LOS B | 4.4 | 31.1 | 0.98 | 1.13 | 40.6 |
| 9 R2 | 168 | 1.9 | 0.578 | 32.3 | LOS C | 4.4 | 31.1 | 0.98 | 1.13 | 38.8 |
| Approach | 499 | 1.1 | 0.801 | 36.9 | LOS C | 10.1 | 70.9 | 0.99 | 1.28 | 37.1 |
| West: Glenfield Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 399 | 6.3 | 1.327 | 185.9 | LOS F | 59.8 | 442.6 | 1.00 | 2.78 | 13.3 |
| 11 T1 | 215 | 7.8 | 1.327 | 186.6 | LOS F | 59.8 | 442.6 | 1.00 | 2.71 | 13.4 |
| 12 R2 | 367 | 6.9 | 1.327 | 193.7 | LOS F | 49.0 | 363.8 | 1.00 | 2.55 | 13.5 |
| Approach | 981 | 6.9 | 1.327 | 189.0 | LOS F | 59.8 | 442.6 | 1.00 | 2.68 | 13.4 |
| All Vehicles | 3438 | 3.8 | 1.327 | 65.2 | LOS E | 59.8 | 442.6 | 0.81 | 1.38 | 28.5 |

## MOVEMENT SUMMARY

$\theta$ Site: I-15 2030 MIMT \& SIMTA OPT 1 PM
Canterbury Road / Cambridge Avenue / Glenfield Road 2030 MIMT \& SIMTA Opt 1 PM PEAK 4:30 pm - 5:30 pm
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Deman Total veh/h | $\begin{array}{r} \text { Iows } \\ \text { HV } \\ \hline \end{array}$ | Deg. Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue <br> Distance <br> m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Canterbury Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 338 | 2.2 | 0.479 | 9.0 | LOS A | 3.1 | 22.2 | 0.79 | 0.93 | 50.8 |
| 2 T1 | 6 | 0.0 | 0.408 | 7.4 | LOS A | 2.5 | 18.0 | 0.77 | 0.92 | 51.2 |
| 3 R2 | 334 | 1.3 | 0.408 | 12.8 | LOS A | 2.5 | 18.0 | 0.77 | 0.92 | 51.3 |
| Approach | 678 | 1.7 | 0.479 | 10.8 | LOS A | 3.1 | 22.2 | 0.78 | 0.93 | 51.1 |
| East: Cambridge Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1170 | 2.2 | 0.617 | 3.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.43 | 56.3 |
| 5 T1 | 302 | 7.7 | 0.464 | 7.3 | LOS A | 3.7 | 26.9 | 0.76 | 0.76 | 51.9 |
| 6 R2 | 339 | 0.9 | 0.464 | 12.5 | LOS A | 3.7 | 26.9 | 0.82 | 0.80 | 52.2 |
| Approach | 1811 | 2.8 | 0.617 | 5.9 | LOS A | 3.7 | 26.9 | 0.28 | 0.55 | 54.8 |
| North: Railway Parade (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 125 | 1.7 | 0.191 | 7.9 | LOS A | 1.0 | 6.8 | 0.69 | 0.80 | 52.8 |
| 8 T1 | 0 | 0.0 | 0.000 | 0.0 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.0 |
| 9 R2 | 240 | 8.3 | 0.295 | 12.7 | LOS A | 1.7 | 12.7 | 0.72 | 0.86 | 50.0 |
| Approach | 365 | 6.1 | 0.295 | 11.0 | LOS A | 1.7 | 12.7 | 0.71 | 0.84 | 51.0 |
| West: Glenfield Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 271 | 4.7 | 0.433 | 8.7 | LOS A | 2.9 | 20.7 | 0.76 | 0.85 | 51.1 |
| 11 T1 | 54 | 0.0 | 0.433 | 8.5 | LOS A | 2.9 | 20.7 | 0.76 | 0.85 | 53.0 |
| 12 R2 | 451 | 3.7 | 0.504 | 13.9 | LOS A | 4.0 | 28.6 | 0.80 | 0.91 | 49.3 |
| Approach | 775 | 3.8 | 0.504 | 11.7 | LOS A | 4.0 | 28.6 | 0.78 | 0.89 | 50.1 |
| All Vehicles | 3629 | 3.2 | 0.617 | 8.6 | LOS A | 4.0 | 28.6 | 0.52 | 0.72 | 52.7 |

## 5. On the wider road network - 2030 cumulative scenario 2

## I-01 Intersection of the Hume Highway and Orange Grove Road

## MOVEMENT SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Total | flows HV | Deg. Satn | Average Delay | Level of Service | 95\% Bac Vehicles | of Queue Distance | Prop. Queued | Effective Stop Rate | Average Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| NorthEast: Hume Highway (NE) |  |  |  |  |  |  |  |  |  |  |
| 25 T1 | 973 | 11.0 | 0.696 | 24.5 | LOS B | 20.1 | 154.2 | 0.85 | 0.77 | 35.6 |
| 26 R2 | 389 | 10.0 | 0.907 | 85.9 | LOS F | 16.8 | 127.3 | 1.00 | 0.92 | 23.9 |
| Approach | 1362 | 10.7 | 0.907 | 42.1 | LOS C | 20.1 | 154.2 | 0.89 | 0.81 | 30.0 |
| NorthWest: Orange Grove Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 602 | 6.5 | 0.712 | 18.8 | LOS B | 19.5 | 144.4 | 0.54 | 0.81 | 44.8 |
| 29 R2 | 1355 | 8.4 | 1.008 | 104.2 | LOS F | 43.9 | 334.0 | 1.00 | 1.02 | 18.6 |
| Approach | 1957 | 7.8 | 1.061 | 77.9 | LOS F | 43.9 | 334.0 | 0.86 | 0.95 | 23.3 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 1280 | 8.6 | 0.462 | 11.7 | LOS A | 14.5 | 110.3 | 0.34 | 0.70 | 50.1 |
| 31 T1 | 2186 | 4.9 | 0.805 | 22.9 | LOS B | 39.5 | 287.9 | 0.71 | 0.65 | 40.2 |
| Approach | 3467 | 6.3 | 0.805 | 18.7 | LOS B | 39.5 | 287.9 | 0.57 | 0.67 | 44.0 |
| All Vehicles | 6786 | 7.6 | 1.061 | 40.5 | LOS C | 43.9 | 334.0 | 0.72 | 0.78 | 31.7 |

## PHASING SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)
Phase times specified by the user
Sequence: TCS 866 AM - Modified
Movement Class: All Movement Classes
Input Sequence: A, B, C
Output Sequence: A, B, C

| Phase Timing Results | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase | Yes | No | No |
| Reference Phase | 0 | 84 | 108 |
| Phase Change Time (sec) | 77 | 17 | 36 |
| Green Time (sec) | 5 | 4 | 5 |
| Yellow Time (sec) | 2 | 2 | 2 |
| All-Red Time (sec) | 84 | 23 | 43 |
| Phase Time (sec) | $56 \%$ | $15 \%$ | $29 \%$ |
| Phase Split |  |  |  |



## MOVEMENT SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 2 PM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| NorthEast: Hume Highway (NE) |  |  |  |  |  |  |  |  |  |  |
| 25 T1 | 1766 | 3.5 | 0.921 | 42.2 | LOS C | 48.3 | 348.3 | 0.91 | 0.96 | 27.6 |
| 26 R2 | 816 | 2.8 | 0.958 | 61.5 | LOS E | 22.8 | 163.7 | 1.00 | 1.00 | 29.2 |
| Approach | 2581 | 3.3 | 0.958 | 48.3 | LOS D | 48.3 | 348.3 | 0.94 | 0.97 | 28.2 |
| NorthWest: Orange Grove Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 391 | 4.3 | 0.393 | 14.2 | LOS A | 8.3 | 60.0 | 0.33 | 0.65 | 48.0 |
| 29 R2 | 1384 | 4.9 | 1.087 | 119.2 | LOS F | 50.2 | 371.0 | 1.00 | 1.07 | 17.0 |
| Approach | 1775 | 4.8 | 1.087 | 96.1 | LOS F | 50.2 | 371.0 | 0.85 | 0.98 | 20.2 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 1322 | 4.7 | 0.787 | 19.7 | LOS B | 21.0 | 155.1 | 0.80 | 0.84 | 44.7 |
| 31 T1 | 1112 | 5.4 | 1.000 | 88.1 | LOS F | 37.4 | 274.4 | 1.00 | 1.10 | 18.1 |
| Approach | 2435 | 5.0 | 1.000 | 51.0 | LOS D | 37.4 | 274.4 | 0.89 | 0.96 | 28.5 |
| All Vehicles | 6791 | 4.3 | 1.087 | 61.7 | LOS E | 50.2 | 371.0 | 0.90 | 0.97 | 25.4 |

## PHASING SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 2 PM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)
Phase times specified by the user
Sequence: TCS 866 PM - Modified
Movement Class: All Movement Classes
Input Sequence: A, B, C, D
Output Sequence: A, B, C, D
Phase Timing Results

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 53 | 80 | 124 |
| Green Time (sec) | 47 | 20 | 38 | 19 |
| Yellow Time (sec) | 5 | 4 | 5 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 54 | 26 | 45 | 25 |
| Phase Split | $36 \%$ | $17 \%$ | $30 \%$ | $17 \%$ |



## I-02 Intersection of the Hume Highway and Elizabeth Drive

## MOVEMENT SUMMARY

Site: I-02 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) per pren |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 137 | 5.4 | 0.155 | 22.6 | LOS B | 3.7 | 27.3 | 0.40 | 0.68 | 36.5 |
| 2 T1 | 2384 | 7.6 | 0.969 | 61.5 | LOS E | 68.0 | 511.2 | 0.99 | 1.03 | 19.7 |
| Approach | 2521 | 7.4 | 0.988 | 59.4 | LOS E | 68.0 | 511.2 | 0.95 | 1.01 | 20.3 |
| East: Elizabeth Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 39 | 5.4 | 0.426 | 59.6 | LOS E | 10.5 | 77.4 | 0.91 | 0.82 | 18.6 |
| 5 T1 | 502 | 5.7 | 0.426 | 55.8 | LOS D | 11.9 | 87.2 | 0.90 | 0.82 | 23.7 |
| 6 R2 | 156 | 2.7 | 0.754 | 78.1 | LOS F | 11.7 | 83.5 | 1.00 | 0.87 | 14.8 |
| Approach | 697 | 5.0 | 0.754 | 61.0 | LOS E | 11.9 | 87.2 | 0.92 | 0.83 | 21.1 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 82 | 2.6 | 0.654 | 25.9 | LOS B | 24.5 | 186.1 | 0.61 | 0.58 | 31.5 |
| 8 T1 | 1777 | 10.0 | 0.654 | 19.8 | LOS B | 24.8 | 190.4 | 0.60 | 0.55 | 35.9 |
| 9 R2 | 353 | 9.6 | 1.170 | 171.2 | LOS F | 19.8 | 149.6 | 1.00 | 1.15 | 10.5 |
| Approach | 2212 | 9.6 | 1.170 | 44.2 | LOS D | 24.8 | 190.4 | 0.66 | 0.65 | 24.6 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 627 | 5.2 | 1.011 | 93.3 | LOS F | 57.3 | 419.3 | 1.00 | 1.01 | 16.3 |
| 11 T1 | 1089 | 3.0 | 1.050 | 107.6 | LOS F | 52.2 | 375.0 | 1.00 | 1.18 | 14.2 |
| 12 R2 | 518 | 7.0 | 1.296 | 227.7 | LOS F | 33.4 | 249.3 | 1.00 | 1.26 | 8.3 |
| Approach | 2235 | 4.5 | 1.296 | 131.4 | LOS F | 57.3 | 419.3 | 1.00 | 1.15 | 12.5 |
| All Vehicles | 7665 | 7.0 | 1.296 | 76.2 | LOS F | 68.0 | 511.2 | 0.88 | 0.93 | 17.7 |

## PHASING SUMMARY

Site: I-02 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | D | F | A | E |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 66 | 89 | 131 |
| Green Time (sec) | 60 | 17 | 36 | 13 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 66 | 23 | 42 | 19 |
| Phase Split | $44 \%$ | $15 \%$ | $28 \%$ | $13 \%$ |

Phase D

## MOVEMENT SUMMARY

Site: I-02 2030 MIMT \& SIMTA OPT 2 PM
Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Demand | Flows | Deg. Satn | Average | Level of | 95\% Bac | of Queue | Prop. | Effective | Average |
| v | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 324 | 5.2 | 0.479 | 39.9 | LOS C | 15.3 | 112.5 | 0.70 | 0.78 | 28.3 |
| 2 T1 | 1567 | 6.4 | 0.945 | 68.9 | LOS E | 44.7 | 334.3 | 0.98 | 1.02 | 18.2 |
| Approach | 1892 | 6.2 | 0.945 | 64.0 | LOS E | 44.7 | 334.3 | 0.93 | 0.98 | 19.6 |
| East: Elizabeth Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 128 | 0.8 | 0.984 | 98.9 | LOS F | 31.7 | 225.4 | 1.00 | 1.08 | 12.9 |
| 5 T1 | 1082 | 2.3 | 0.984 | 94.6 | LOS F | 40.3 | 287.5 | 1.00 | 1.10 | 16.3 |
| 6 R2 | 172 | 0.0 | 1.066 | 131.4 | LOS F | 17.1 | 119.5 | 1.00 | 1.12 | 9.9 |
| Approach | 1382 | 1.9 | 1.066 | 99.6 | LOS F | 40.3 | 287.5 | 1.00 | 1.10 | 15.0 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 66 | 4.8 | 0.874 | 25.5 | LOS B | 43.4 | 316.9 | 0.74 | 0.72 | 32.1 |
| 8 T1 | 2474 | 4.1 | 0.874 | 19.6 | LOS B | 44.1 | 322.3 | 0.74 | 0.71 | 36.2 |
| 9 R2 | 961 | 3.0 | 0.917 | 75.8 | LOS F | 37.4 | 268.2 | 1.00 | 0.94 | 19.6 |
| Approach | 3501 | 3.8 | 0.917 | 35.1 | LOS C | 44.1 | 322.3 | 0.81 | 0.78 | 28.5 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 325 | 5.8 | 0.434 | 34.2 | LOS C | 13.6 | 100.2 | 0.62 | 0.76 | 29.6 |
| 11 T1 | 529 | 4.4 | 0.698 | 61.8 | LOS E | 17.6 | 127.6 | 0.96 | 0.82 | 20.9 |
| 12 R2 | 309 | 2.4 | 0.978 | 105.6 | LOS F | 13.7 | 98.2 | 1.00 | 1.00 | 15.4 |
| Approach | 1164 | 4.2 | 0.978 | 65.7 | LOS E | 17.6 | 127.6 | 0.88 | 0.85 | 20.6 |
| All Vehicles | 7939 | 4.1 | 1.066 | 57.7 | LOS E | 44.7 | 334.3 | 0.88 | 0.89 | 21.5 |

## PHASING SUMMARY

## Site: I-02 2030 MIMT \& SIMTA OPT 2 PM

Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | D | F | A | E |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 53 | 72 | 108 |
| Green Time (sec) | 47 | 13 | 30 | 36 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 53 | 19 | 36 | 42 |
| Phase Split | $35 \%$ | $13 \%$ | $24 \%$ | $28 \%$ |



## I-03 Intersection of the Hume Highway and Memorial Avenue

## MOVEMENT SUMMARY

Site: I-03 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 157 | 1.3 | 0.976 | 67.5 | LOS E | 68.5 | 511.8 | 1.00 | 1.06 | 27.0 |
| 2 T1 | 2129 | 8.3 | 0.976 | 59.1 | LOS E | 69.8 | 528.2 | 0.94 | 1.01 | 25.4 |
| 3 R2 | 267 | 0.0 | 1.137 | 158.3 | LOS F | 29.3 | 204.9 | 1.00 | 1.12 | 12.4 |
| Approach | 2553 | 7.0 | 1.137 | 70.0 | LOS E | 69.8 | 528.2 | 0.95 | 1.03 | 23.1 |
| East: Memorial Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 29 | 28.6 | 1.264 | 214.3 | LOS F | 21.6 | 165.9 | 1.00 | 1.33 | 9.8 |
| 5 T1 | 164 | 7.7 | 1.264 | 209.5 | LOS F | 21.6 | 165.9 | 1.00 | 1.33 | 9.6 |
| 6 R2 | 134 | 18.1 | 1.264 | 214.6 | LOS F | 19.4 | 155.3 | 1.00 | 1.32 | 6.9 |
| Approach | 327 | 13.8 | 1.264 | 212.0 | LOS F | 21.6 | 165.9 | 1.00 | 1.33 | 8.6 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 121 | 6.1 | 0.103 | 12.4 | LOS A | 2.6 | 19.4 | 0.36 | 0.64 | 39.4 |
| 8 T1 | 1787 | 12.5 | 0.768 | 28.7 | LOS C | 33.4 | 261.9 | 0.75 | 0.68 | 36.2 |
| 9 R2 | 101 | 3.1 | 0.439 | 72.0 | LOS F | 7.0 | 50.1 | 0.97 | 0.79 | 21.4 |
| Approach | 2009 | 11.7 | 0.768 | 29.9 | LOS C | 33.4 | 261.9 | 0.74 | 0.68 | 35.1 |
| West: Memorial Avenue (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 128 | 3.3 | 1.183 | 159.2 | LOS F | 36.3 | 259.0 | 1.00 | 1.27 | 12.6 |
| 11 T1 | 460 | 1.6 | 1.183 | 162.1 | LOS F | 46.5 | 332.1 | 1.00 | 1.31 | 11.7 |
| 12 R2 | 166 | 3.2 | 1.183 | 173.8 | LOS F | 46.5 | 332.1 | 1.00 | 1.34 | 14.6 |
| Approach | 755 | 2.2 | 1.183 | 164.2 | LOS F | 46.5 | 332.1 | 1.00 | 1.31 | 12.5 |
| All Vehicles | 5644 | 8.4 | 1.264 | 76.6 | LOS F | 69.8 | 528.2 | 0.88 | 0.96 | 21.4 |

## PHASING SUMMARY

Site: I-03 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E | F |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 75 | 108 | 125 |
| Green Time (sec) | 69 | 27 | 11 | 19 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 75 | 33 | 17 | 25 |
| Phase Split | $50 \%$ | $22 \%$ | $11 \%$ | $17 \%$ |



## MOVEMENT SUMMARY

## Site: I-03 2030 MIMT \& SIMTA OPT 2 PM

Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 123 | 0.9 | 0.839 | 48.8 | LOS D | 38.8 | 287.8 | 0.92 | 0.89 | 31.7 |
| 2 T1 | 1678 | 6.8 | 0.839 | 40.6 | LOS C | 39.7 | 297.6 | 0.89 | 0.83 | 30.9 |
| 3 R2 | 116 | 0.0 | 0.779 | 84.4 | LOS F | 8.9 | 62.5 | 1.00 | 0.86 | 19.4 |
| Approach | 1917 | 6.0 | 0.839 | 43.8 | LOS D | 39.7 | 297.6 | 0.89 | 0.84 | 30.0 |
| East: Memorial Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 55 | 0.0 | 1.228 | 195.7 | LOS F | 34.9 | 247.9 | 1.00 | 1.40 | 10.7 |
| 5 T1 | 289 | 2.2 | 1.228 | 191.2 | LOS F | 34.9 | 247.9 | 1.00 | 1.39 | 10.3 |
| 6 R2 | 211 | 6.0 | 1.228 | 196.2 | LOS F | 32.3 | 235.9 | 1.00 | 1.32 | 7.5 |
| Approach | 555 | 3.4 | 1.228 | 193.5 | LOS F | 34.9 | 247.9 | 1.00 | 1.37 | 9.3 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 152 | 2.8 | 0.090 | 8.4 | LOS A | 2.0 | 14.7 | 0.24 | 0.61 | 43.5 |
| 8 T1 | 2955 | 3.8 | 0.937 | 19.6 | LOS B | 63.8 | 463.9 | 0.68 | 0.68 | 41.4 |
| $9 \quad \mathrm{R} 2$ | 214 | 2.0 | 0.729 | 42.6 | LOS D | 9.2 | 65.2 | 1.00 | 0.83 | 28.2 |
| Approach | 3320 | 3.6 | 0.937 | 20.6 | LOS B | 63.8 | 463.9 | 0.68 | 0.69 | 40.2 |
| West: Memorial Avenue (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 82 | 1.3 | 0.947 | 89.9 | LOS F | 17.2 | 121.7 | 1.00 | 1.08 | 18.9 |
| 11 T1 | 209 | 1.0 | 0.947 | 86.8 | LOS F | 21.4 | 150.2 | 1.00 | 1.06 | 18.0 |
| 12 R2 | 171 | 0.0 | 0.947 | 93.9 | LOS F | 21.4 | 150.2 | 1.00 | 1.03 | 21.9 |
| Approach | 462 | 0.7 | 0.947 | 90.0 | LOS F | 21.4 | 150.2 | 1.00 | 1.05 | 19.7 |
| All Vehicles | 6254 | 4.1 | 1.228 | 48.2 | LOS D | 63.8 | 463.9 | 0.80 | 0.82 | 27.9 |

## PHASING SUMMARY

## Site: I-03 2030 MIMT \& SIMTA OPT 2 PM

Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)

## Phase Timing Results

| Phase | A | C | D | E | F |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No | No |
| Phase Change Time (sec) | 0 | 67 | 81 | 108 | 132 |
| Green Time (sec) | 61 | 8 | 21 | 18 | 12 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 67 | 14 | 27 | 24 | 18 |
| Phase Split | $45 \%$ | $9 \%$ | $18 \%$ | $16 \%$ | $12 \%$ |

## I-04 Intersection of the Hume Highway and Hoxton Park Drive

## MOVEMENT SUMMARY

Site: I-04 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Hoxton Park Road / Macquarie Street
2030 MIMT \& SIMTA AM Option 2 PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 109 | 12.7 | 0.096 | 8.8 | LOS A | 0.9 | 7.2 | 0.13 | 0.57 | 50.6 |
| 2 T1 | 2153 | 6.3 | 0.847 | 31.0 | LOS C | 43.8 | 326.0 | 0.83 | 0.77 | 38.1 |
| 3 R 2 | 1213 | 1.9 | 1.038 | 98.4 | LOS F | 46.4 | 330.1 | 1.00 | 1.09 | 17.7 |
| Approach | 3474 | 4.9 | 1.038 | 53.8 | LOS D | 46.4 | 330.1 | 0.87 | 0.88 | 28.7 |
| East: Macquarie Street (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 361 | 5.8 | 0.230 | 21.3 | LOS B | 5.5 | 40.4 | 0.66 | 0.73 | 39.0 |
| 5 T1 | 545 | 4.6 | 1.080 | 130.0 | LOS F | 27.8 | 202.5 | 1.00 | 1.19 | 16.2 |
| Approach | 906 | 5.1 | 1.080 | 86.7 | LOS F | 27.8 | 202.5 | 0.86 | 1.01 | 20.6 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 236 | 15.6 | 1.022 | 53.1 | LOS D | 45.4 | 353.1 | 1.00 | 1.01 | 28.0 |
| 8 T1 | 1501 | 9.8 | 1.022 | 86.5 | LOS F | 56.7 | 436.0 | 1.00 | 1.10 | 23.0 |
| 9 R2 | 246 | 19.2 | 1.257 | 211.1 | LOS F | 30.8 | 251.3 | 1.00 | 1.27 | 13.2 |
| Approach | 1984 | 11.6 | 1.257 | 98.0 | LOS F | 56.7 | 436.0 | 1.00 | 1.11 | 21.2 |
| West: Hoxton Park Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 345 | 18.0 | 0.583 | 47.3 | LOS D | 20.3 | 164.2 | 0.87 | 0.83 | 32.5 |
| 11 T1 | 1372 | 4.8 | 1.131 | 164.8 | LOS F | 55.8 | 406.4 | 1.00 | 1.34 | 13.5 |
| 12 R2 | 393 | 4.6 | 1.148 | 140.7 | LOS F | 23.6 | 172.9 | 1.00 | 1.10 | 16.9 |
| Approach | 2109 | 6.9 | 1.148 | 141.1 | LOS F | 55.8 | 406.4 | 0.98 | 1.21 | 15.9 |
| All Vehicles | 8473 | 7.0 | 1.257 | 89.4 | LOS F | 56.7 | 436.0 | 0.92 | 1.03 | 21.6 |

## PHASING SUMMARY

## Site: I-04 2030 MIMT \& SIMTA OPT 2 AM

Hume Highway / Hoxton Park Road / Macquarie Street 2030 MIMT \& SIMTA AM Option 2 PEAK 7:45 am - 8:45 am Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

## Phase Timing Results

| Phase | A | C | E | D | F |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No | No |
| Phase Change Time (sec) | 0 | 49 | 77 | 100 | 126 |
| Green Time (sec) | 43 | 22 | 17 | 20 | 18 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 49 | 28 | 23 | 26 | 24 |
| Phase Split | $33 \%$ | $19 \%$ | $15 \%$ | $17 \%$ | $16 \%$ |



## MOVEMENT SUMMARY

## Site: I-04 2030 MIMT \& SIMTA OPT 2 PM

Hume Highway / Hoxton Park Road / Macquarie Street
2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 202 | 6.5 | 0.171 | 9.6 | LOS A | 2.1 | 15.4 | 0.16 | 0.59 | 50.2 |
| 2 T1 | 1634 | 6.8 | 0.655 | 24.3 | LOS B | 26.0 | 195.0 | 0.65 | 0.58 | 41.4 |
| 3 R2 | 448 | 1.2 | 0.934 | 93.1 | LOS F | 18.7 | 132.4 | 1.00 | 0.96 | 18.4 |
| Approach | 2284 | 5.7 | 0.934 | 36.5 | LOS C | 26.0 | 195.0 | 0.67 | 0.66 | 35.0 |
| East: Macquarie Street (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 785 | 1.5 | 1.024 | 141.2 | LOS F | 35.3 | 250.1 | 0.98 | 1.03 | 13.6 |
| 5 T1 | 706 | 3.3 | 1.087 | 125.9 | LOS F | 35.4 | 254.8 | 1.00 | 1.19 | 16.5 |
| Approach | 1492 | 2.3 | 1.087 | 133.9 | LOS F | 35.4 | 254.8 | 0.99 | 1.10 | 14.9 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 101 | 5.2 | 0.966 | 33.5 | LOS C | 74.4 | 541.1 | 0.94 | 0.98 | 36.3 |
| 8 T1 | 2838 | 3.5 | 0.966 | 28.3 | LOS B | 75.8 | 550.8 | 0.83 | 0.86 | 39.3 |
| $9 \quad \mathrm{R} 2$ | 283 | 6.3 | 1.406 | 276.3 | LOS F | 39.8 | 293.6 | 1.00 | 1.37 | 10.6 |
| Approach | 3222 | 3.8 | 1.406 | 50.3 | LOS D | 75.8 | 550.8 | 0.85 | 0.91 | 31.1 |
| West: Hoxton Park Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 252 | 4.2 | 0.395 | 44.4 | LOS D | 13.7 | 99.2 | 0.80 | 0.80 | 33.6 |
| 11 T1 | 717 | 4.3 | 0.439 | 46.6 | LOS D | 14.2 | 102.8 | 0.87 | 0.73 | 30.4 |
| 12 R2 | 387 | 3.5 | 1.258 | 176.8 | LOS F | 26.1 | 189.9 | 1.00 | 1.18 | 14.3 |
| Approach | 1356 | 4.0 | 1.258 | 83.4 | LOS F | 26.1 | 189.9 | 0.89 | 0.87 | 23.0 |
| All Vehicles | 8353 | 4.1 | 1.406 | 66.8 | LOS E | 75.8 | 550.8 | 0.83 | 0.87 | 26.0 |

## PHASING SUMMARY

## Site: I-04 2030 MIMT \& SIMTA OPT 2 PM

Hume Highway / Hoxton Park Road / Macquarie Street 2030 MIMT \& SIMTA Option 2 PM PEAK 4:30 pm - 5:30 pm Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

## Phase Timing Results

| Phase | A | E | D | F |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 78 | 98 | 127 |
| Green Time (sec) | 72 | 14 | 23 | 17 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 78 | 20 | 29 | 23 |
| Phase Split | $52 \%$ | $13 \%$ | $19 \%$ | $15 \%$ |

Phase $A$

## I-05 Intersection of the Hume Highway and Reilly Street

## MOVEMENT SUMMARY

Site: I-05 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Hignway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 80 | 2.6 | 0.943 | 32.3 | LOS C | 72.0 | 526.9 | 0.86 | 0.88 | 36.1 |
| 2 T1 | 3174 | 4.5 | 0.943 | 25.9 | LOS B | 72.0 | 526.9 | 0.79 | 0.81 | 35.8 |
| 3 R2 | 14 | 7.7 | 0.112 | 24.3 | LOS B | 0.5 | 3.8 | 0.51 | 0.68 | 36.2 |
| Approach | 3268 | 4.5 | 0.943 | 26.1 | LOS B | 72.0 | 526.9 | 0.79 | 0.81 | 35.8 |
| East: Congressional Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 49 | 2.1 | 0.263 | 59.1 | LOS E | 5.9 | 42.6 | 0.89 | 0.74 | 24.5 |
| 5 T1 | 46 | 4.5 | 0.263 | 54.5 | LOS D | 5.9 | 42.6 | 0.89 | 0.74 | 24.0 |
| 6 R2 | 91 | 4.7 | 0.428 | 67.2 | LOS E | 6.1 | 44.6 | 0.95 | 0.79 | 18.7 |
| Approach | 186 | 4.0 | 0.428 | 61.9 | LOS E | 6.1 | 44.6 | 0.92 | 0.76 | 21.6 |
| North: Hume Hignway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 32 | 3.3 | 0.569 | 18.2 | LOS B | 22.6 | 172.1 | 0.53 | 0.57 | 39.2 |
| 8 T1 | 1891 | 8.9 | 0.569 | 11.2 | LOS A | 25.8 | 196.7 | 0.51 | 0.49 | 46.4 |
| 9 R2 | 99 | 1.1 | 0.772 | 60.2 | LOS E | 6.1 | 43.1 | 1.00 | 0.93 | 22.6 |
| Approach | 2022 | 8.4 | 0.772 | 13.7 | LOS A | 25.8 | 196.7 | 0.53 | 0.52 | 44.0 |
| West: Reilly Street (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 120 | 3.5 | 0.274 | 50.3 | LOS D | 7.6 | 55.2 | 0.83 | 0.76 | 24.5 |
| 11 T1 | 14 | 7.7 | 0.274 | 45.7 | LOS D | 7.6 | 55.2 | 0.83 | 0.76 | 25.6 |
| 12 R2 | 237 | 1.3 | 1.039 | 127.9 | LOS F | 23.6 | 167.1 | 1.00 | 1.10 | 16.2 |
| Approach | 371 | 2.3 | 1.039 | 99.7 | LOS F | 23.6 | 167.1 | 0.94 | 0.98 | 18.1 |
| All Vehicles | 5846 | 5.7 | 1.039 | 27.6 | LOS B | 72.0 | 526.9 | 0.72 | 0.72 | 34.8 |

## PHASING SUMMARY

Site: I-05 2030 MIMT \& SIMTA OPT 2 AM
Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E2 |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 100 | 138 |
| Green Time (sec) | 94 | 32 | 6 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 100 | 38 | 12 |
| Phase Split | $67 \%$ | $25 \%$ | $8 \%$ |

Phase A

## MOVEMENT SUMMARY

## Site: I-05 2030 MIMT \& SIMTA OPT 2 PM

Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Hignway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 226 | 0.5 | 0.682 | 19.9 | LOS B | 27.3 | 199.8 | 0.54 | 0.58 | 41.7 |
| 2 T1 | 2097 | 6.0 | 0.682 | 11.9 | LOS A | 27.3 | 199.8 | 0.47 | 0.46 | 45.5 |
| 3 R 2 | 21 | 5.0 | 0.391 | 30.4 | LOS C | 1.0 | 7.5 | 0.62 | 0.73 | 33.4 |
| Approach | 2345 | 5.4 | 0.682 | 12.8 | LOS A | 27.3 | 199.8 | 0.48 | 0.47 | 44.8 |
| East: Congressional Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 42 | 2.5 | 0.205 | 61.9 | LOS E | 4.2 | 29.6 | 0.90 | 0.73 | 23.8 |
| 5 T1 | 24 | 0.0 | 0.205 | 57.3 | LOS E | 4.2 | 29.6 | 0.90 | 0.73 | 23.3 |
| 6 R2 | 52 | 0.0 | 0.236 | 65.6 | LOS E | 3.4 | 23.6 | 0.92 | 0.75 | 19.1 |
| Approach | 118 | 0.9 | 0.236 | 62.6 | LOS E | 4.2 | 29.6 | 0.91 | 0.74 | 21.7 |
| North: Hume Hignway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 67 | 0.0 | 0.986 | 31.7 | LOS C | 89.4 | 645.9 | 0.79 | 0.86 | 30.9 |
| 8 T1 | 3696 | 3.0 | 0.986 | 27.1 | LOS B | 89.4 | 645.9 | 0.60 | 0.69 | 35.2 |
| $9 \quad \mathrm{R} 2$ | 178 | 1.2 | 0.813 | 59.5 | LOS E | 11.7 | 82.4 | 1.00 | 1.01 | 22.7 |
| Approach | 3941 | 2.9 | 0.986 | 28.6 | LOS C | 89.4 | 645.9 | 0.62 | 0.70 | 34.3 |
| West: Reilly Street (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 65 | 0.0 | 0.235 | 56.1 | LOS D | 5.8 | 40.6 | 0.86 | 0.74 | 23.5 |
| 11 T1 | 32 | 0.0 | 0.235 | 51.6 | LOS D | 5.8 | 40.6 | 0.86 | 0.74 | 24.5 |
| 12 R2 | 261 | 1.6 | 1.120 | 156.3 | LOS F | 28.6 | 203.3 | 1.00 | 1.17 | 14.1 |
| Approach | 358 | 1.2 | 1.120 | 128.8 | LOS F | 28.6 | 203.3 | 0.96 | 1.06 | 15.5 |
| All Vehicles | 6762 | 3.7 | 1.120 | 29.0 | LOS C | 89.4 | 645.9 | 0.59 | 0.64 | 34.1 |

## PHASING SUMMARY

## Site: I-05 2030 MIMT \& SIMTA OPT 2 PM

Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E2 |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 98 | 133 |
| Green Time (sec) | 92 | 29 | 11 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 98 | 35 | 17 |
| Phase Split | $65 \%$ | $23 \%$ | $11 \%$ |

## I-06 Intersection of Newbridge Road and Moorebank Avenue

## MOVEMENT SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 2 AM

Network: 2030 MIMT \& SIMTA OPT 2 AM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV veh/h |  | Arrival Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1535 | 3.2 |  |  |  | 1232 | 3.2 | 0.636 | 19.0 | LOS B | 13.7 | 98.3 | 0.57 | 0.82 | 42.3 |
| 3 R2 | 1402 | 11.4 | 1128 | 11.7 | 0.683 | 15.2 | LOS B | 14.4 | 113.1 | 0.43 | 0.69 | 52.4 |
| Approach | 2937 | 7.1 | 2360 N1 | 7.3 | 0.683 | 17.2 | LOS B | 14.4 | 113.1 | 0.50 | 0.76 | 47.8 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 721 | 21.2 | 721 | 21.2 | 0.659 | 19.5 | LOS B | 9.7 | 81.4 | 0.77 | 0.82 | 51.2 |
| 5 T1 | 965 | 5.1 | 965 | 5.1 | 1.260 | 311.5 | LOS F | 77.3 | 564.9 | 1.00 | 1.91 | 14.7 |
| Approach | 1686 | 12.0 | 1686 | 12.0 | 1.260 | 186.6 | LOS F | 77.3 | 564.9 | 0.90 | 1.44 | 19.0 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1581 | 6.5 | 1581 | 6.5 | 0.852 | 12.4 | LOS A | 30.8 | 227.8 | 0.63 | 0.60 | 60.9 |
| 12 R2 | 889 | 7.6 | 889 | 7.6 | 1.716 | 701.0 | LOS F | 104.1 | 777.5 | 1.00 | 2.02 | 3.0 |
| Approach | 2471 | 6.9 | 2471 | 6.9 | 1.716 | 260.3 | LOS F | 104.1 | 777.5 | 0.77 | 1.11 | 13.8 |
| All Vehicles | 7094 | 8.2 | 6517 N1 | 8.9 | 1.716 | 153.2 | LOS F | 104.1 | 777.5 | 0.70 | 1.07 | 19.3 |

## PHASING SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 2 AM

Network: 2030 MIMT \& SIMTA OPT 2 AM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)
Phase Timing Results


## MOVEMENT SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 2 PM

中 ${ }^{\text {¢ }}$ Network: 2030 MIMT \& SIMTA OPT 2 PM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Arrival Flows Deg. Satn Total HV Total HV |  |  |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1022 | 2.9 | 903 | 3.0 | 0.515 | 22.6 | LOS B | 13.5 | 96.8 | 0.57 | 0.75 | 39.8 |
| 3 R2 | 981 | 11.2 | 870 | 11.6 | 1.142 | 186.3 | LOS F | 16.7 | 130.6 | 1.00 | 1.42 | 16.1 |
| Approach | 2003 | 6.9 | 1774 N1 | 7.2 | 1.142 | 102.9 | LOS F | 16.7 | 130.6 | 0.78 | 1.08 | 20.9 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1272 | 7.2 | 1272 | 7.2 | 1.116 | 197.7 | LOS F | 80.5 | 607.2 | 1.00 | 1.32 | 14.6 |
| 5 T1 | 1373 | 4.8 | 1373 | 4.8 | 0.923 | 51.1 | LOS D | 42.7 | 311.4 | 1.00 | 1.04 | 43.3 |
| Approach | 2644 | 6.0 | 2644 | 6.0 | 1.116 | 121.6 | LOS F | 80.5 | 607.2 | 1.00 | 1.17 | 25.1 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1129 | 4.0 | 1129 | 4.0 | 0.442 | 9.3 | LOS A | 14.6 | 105.8 | 0.50 | 0.45 | 62.9 |
| 12 R2 | 1120 | 2.8 | 1120 | 2.8 | 1.206 | 238.9 | LOS F | 76.0 | 544.9 | 1.00 | 1.48 | 8.0 |
| Approach | 2249 | 3.4 | 2249 | 3.4 | 1.206 | 123.6 | LOS F | 76.0 | 544.9 | 0.75 | 0.97 | 22.1 |
| All Vehicles | 6897 | 5.4 | 6667 N1 | 5.6 | 1.206 | 117.3 | LOS F | 80.5 | 607.2 | 0.86 | 1.08 | 23.1 |

## PHASING SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 2 PM
\$中 Network: 2030 MIMT \& SIMTA OPT 2 PM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=116$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | C | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 44 | 76 |
| Green Time (sec) | 38 | 26 | 34 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 44 | 32 | 40 |
| Phase Split | $38 \%$ | $28 \%$ | $34 \%$ |

I-07 Intersection of Moorebank Avenue and Heathcote Road

## MOVEMENT SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 2 AM

Network: 2030 MIMT \& SIMTA OPT 2 AM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows <br> Total HV veh/h |  | Arrival Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1948 | 7.0 |  |  |  | 1769 | 7.1 | 1.168 | 198.5 | LOS F | 58.4 | 440.6 | 1.00 | 1.86 | 4.8 |
| 3 R2 | 23 | 18.2 | 21 | 18.4 | 0.190 | 71.8 | LOS F | 1.4 | 11.0 | 0.98 | 0.71 | 30.6 |
| Approach | 1972 | 7.2 | 1790 N1 | 7.2 | 1.168 | 197.0 | LOS F | 58.4 | 440.6 | 1.00 | 1.85 | 5.0 |
| East: Heathcote Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 29 | 57.1 | 29 | 57.1 | 1.444 | 484.0 | LOS F | 102.4 | 771.5 | 1.00 | 1.95 | 6.8 |
| 6 R2 | 952 | 5.9 | 952 | 5.9 | 1.444 | 483.8 | LOS F | 102.4 | 771.5 | 1.00 | 1.95 | 6.8 |
| Approach | 981 | 7.4 | 981 | 7.4 | 1.444 | 483.8 | LOS F | 102.4 | 771.5 | 1.00 | 1.95 | 6.8 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 795 | 7.9 | 610 | 9.0 | 0.378 | 10.7 | LOS A | 12.1 | 91.2 | 0.54 | 0.71 | 51.4 |
| 8 T1 | 833 | 19.3 | 651 | 21.6 | 0.383 | 21.5 | LOS B | 12.8 | 108.3 | 0.66 | 0.58 | 13.1 |
| Approach | 1628 | 13.7 | $1261{ }^{\text {N1 }}$ | 15.5 | 0.383 | 16.3 | LOS B | 12.8 | 108.3 | 0.60 | 0.64 | 40.9 |
| All Vehicles | 4581 | 9.6 | 4032 N1 | 10.9 | 1.444 | 210.3 | LOS F | 102.4 | 771.5 | 0.87 | 1.50 | 8.4 |

## PHASING SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 2 AM
\$ゆ Network: 2030 MIMT \& SIMTA OPT 2 AM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)

| Phase Timing Results | B | A | D |
| :--- | :---: | :---: | :---: |
| Phase | Yes | No | No |
| Reference Phase | 0 | 15 | 88 |
| Phase Change Time (sec) | 9 | 67 | 39 |
| Green Time (sec) | 4 | 4 | 4 |
| Yellow Time (sec) | 2 | 2 | 2 |
| All-Red Time (sec) | 15 | 73 | 45 |
| Phase Time (sec) | $11 \%$ | $55 \%$ | $34 \%$ |
| Phase Split |  |  |  |

Phase B

## MOVEMENT SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 2 PM

㿾 Network: 2030 MIMT \& SIMTA OPT 2 PM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV veh/h \% |  | Arrival Flows Deg. SatnTotal HV |  |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% |  | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1221 | 9.0 |  |  |  |  | 1221 | 9.0 |  | 0.970 | 72.2 | LOS F | 56.8 | 432.9 | 0.99 | 1.28 | 11.6 |
| $3 \quad \mathrm{R} 2$ | 48 | 8.7 | 48 | 8.7 |  | 0.401 | 64.7 | LOS E | 2.8 | 20.9 | 1.00 | 0.74 | 32.2 |
| Approach | 1269 | 9.0 | 1269 | 9.0 |  | 0.970 | 71.9 | LOS F | 56.8 | 432.9 | 0.99 | 1.26 | 12.9 |
| East: Heathcote Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 76 | 19.4 | 76 | 19.4 |  | 1.442 | 454.6 | LOS F | 95.1 | 707.4 | 1.00 | 2.03 | 7.1 |
| 6 R2 | 812 | 5.2 | 812 | 5.2 |  | 1.442 | 453.8 | LOS F | 95.1 | 707.4 | 1.00 | 2.04 | 7.1 |
| Approach | 887 | 6.4 | 887 | 6.4 |  | 1.442 | 453.9 | LOS F | 95.1 | 707.4 | 1.00 | 2.04 | 7.1 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 884 | 3.7 | 764 | 3.8 |  | 0.361 | 7.5 | LOS A | 5.1 | 36.6 | 0.24 | 0.61 | 53.8 |
| 8 T1 | 1491 | 6.5 | 1290 | 6.7 |  | 0.673 | 6.3 | LOS A | 11.8 | 88.8 | 0.35 | 0.32 | 29.2 |
| Approach | 2375 | 5.5 | 2054 N1 | 5.6 |  | 0.673 | 6.7 | LOS A | 11.8 | 88.8 | 0.31 | 0.43 | 48.4 |
| All Vehicles | 4532 | 6.6 | 4211 N1 | 7.1 |  | 1.442 | 120.6 | LOS F | 95.1 | 707.4 | 0.66 | 1.02 | 12.8 |

## PHASING SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 2 PM
\$ Network: 2030 MIMT \& SIMTA OPT 2 PM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | B | A | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 14 | 80 |
| Green Time (sec) | 8 | 60 | 30 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 14 | 66 | 36 |
| Phase Split | $12 \%$ | $57 \%$ | $31 \%$ |

## I-08 Intersection of Moorebank Avenue and Industry Park Access

## MOVEMENT SUMMARY

Site: I-08 2030 MIMT \& SIMTA Opt 2 AM

## \$ Network: 2030 MIMT \& SIMTA OPT 2 AM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=133$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV | Arrival Total | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Deg. Satn | Average Delay | Level of Service | 95\% Back <br> Vehicles | Queue Distance | Prop. Queued | Effective Stop Rate | Average Speed |
|  | veh/h \% | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 913.5 | 91 | 3.5 | 0.056 | 6.1 | LOS A | 0.4 | 2.6 | 0.12 | 0.58 | 43.1 |
| 2 T1 | 19296.4 | 1929 | 6.4 | 1.258 | 294.8 | LOS F | 169.6 | 1272.1 | 1.00 | 2.23 | 5.5 |
| Approach | 20206.3 | 2020 | 6.3 | 1.258 | 281.8 | LOS F | 169.6 | 1272.1 | 0.96 | 2.15 | 5.8 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 75418.0 | 587 | 20.1 | 0.208 | 2.5 | LOS A | 3.9 | 32.4 | 0.22 | 0.20 | 56.9 |
| 9 R2 | $65 \quad 38.7$ | 52 | 41.7 | 0.990 | 105.3 | LOS F | 4.3 | 40.9 | 1.00 | 1.02 | 12.6 |
| Approach | 81919.7 | 639 N1 | 21.8 | 0.990 | 10.9 | LOS A | 4.3 | 40.9 | 0.29 | 0.26 | 47.5 |
| West: Industry Park Access (W) |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3462.5 | 34 | 62.5 | 0.415 | 64.9 | LOS E | 2.3 | 24.3 | 0.95 | 0.73 | 9.6 |
| 12 R2 | $58 \quad 72.7$ | 58 | 72.7 | 0.413 | 68.0 | LOS E | 2.7 | 31.4 | 0.98 | 0.73 | 19.8 |
| Approach | 9269.0 | 92 | 69.0 | 0.415 | 66.9 | LOS E | 2.7 | 31.4 | 0.97 | 0.73 | 16.8 |
| All Vehicles | 293112.0 | 2751 N1 | 12.8 | 1.258 | 211.7 | LOS F | 169.6 | 1272.1 | 0.80 | 1.67 | 8.2 |

## PHASING SUMMARY

Site: I-08 2030 MIMT \& SIMTA Opt 2 AM

中审 Network: 2030 MIMT \& SIMTA OPT 2 AM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=133$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | C |
| :--- | :---: | :---: |
| Reference Phase | Yes | No |
| Phase Change Time (sec) | 0 | 116 |
| Green Time (sec) | 110 | 11 |
| Yellow Time (sec) | 4 | 4 |
| All-Red Time (sec) | 2 | 2 |
| Phase Time (sec) | 116 | 17 |
| Phase Split | $87 \%$ | $13 \%$ |



## MOVEMENT SUMMARY

Site: I-08 2030 MIMT \& SIMTA Opt 2 PM

Network: 2030 MIMT \& SIMTA OPT 2 PM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (Network Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV veh/h \% |  | Arrival Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 30.0 |  |  |  | 11 | 30.0 | 0.009 | 6.6 | LOS A | 0.1 | 0.5 | 0.14 | 0.56 | 42.9 |
| 2 T1 | 1191 | 8.3 | 1191 | 8.3 | 0.474 | 4.9 | LOS A | 12.7 | 96.5 | 0.38 | 0.35 | 51.6 |
| Approach | 1201 | 8.5 | 1201 | 8.5 | 0.474 | 4.9 | LOS A | 12.7 | 96.5 | 0.38 | 0.35 | 51.4 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1556 | 5.6 | 1338 | 5.6 | 0.462 | 4.8 | LOS A | 12.9 | 96.1 | 0.38 | 0.35 | 54.3 |
| 9 R2 | 25 | 62.5 | 22 | 62.4 | 0.162 | 15.6 | LOS B | 0.5 | 5.6 | 0.42 | 0.66 | 32.2 |
| Approach | 1581 | 6.5 | 1360 N1 | 6.5 | 0.462 | 5.0 | LOS A | 12.9 | 96.1 | 0.38 | 0.35 | 53.9 |
| West: Industry Park Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 34 | 15.6 | 34 | 15.6 | 0.090 | 4.0 | LOS A | 0.4 | 3.2 | 0.27 | 0.39 | 26.5 |
| 12 R2 | 189 | 10.0 | 189 | 10.0 | 0.455 | 54.9 | LOS D | 5.2 | 39.6 | 0.97 | 0.77 | 22.7 |
| Approach | 223 | 10.8 | 223 | 10.8 | 0.455 | 47.2 | LOS D | 5.2 | 39.6 | 0.87 | 0.71 | 22.9 |
| All Vehicles | 3005 | 7.6 | 2784 N1 | 8.2 | 0.474 | 8.3 | LOS A | 12.9 | 96.5 | 0.42 | 0.38 | 47.8 |

## PHASING SUMMARY

Site: I-08 2030 MIMT \& SIMTA Opt 2 PM

Network: 2030 MIMT \& SIMTA OPT 2 PM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (Network Cycle Time)
Phase Timing Results

| Phase | A | C |
| :--- | :---: | :---: |
| Reference Phase | Yes | No |
| Phase Change Time (sec) | 0 | 96 |
| Green Time (sec) | 90 | 14 |
| Yellow Time (sec) | 4 | 4 |
| All-Red Time (sec) | 2 | 2 |
| Phase Time (sec) | 96 | 20 |
| Phase Split | $83 \%$ | $17 \%$ |



## I-09 Intersection of Moorebank Avenue and Church Road

## MOVEMENT SUMMARY

## $\nabla$ Site: I-09 2030 MIMT \& SIMTA OPT 2 AM

Moorebank Avenue / Church Road
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 2132 | 7.8 | 0.793 | 6.7 | LOS A | 11.8 | 89.6 | 0.14 | 0.10 | 53.5 |
| 3 R2 | 284 | 8.5 | 0.793 | 31.3 | LOS C | 11.8 | 89.6 | 1.00 | 0.72 | 37.8 |
| Approach | 2416 | 7.9 | 0.992 | 9.6 | NA | 11.8 | 89.6 | 0.24 | 0.18 | 51.0 |
| East: Church Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 204 | 15.8 | 0.269 | 7.7 | LOS A | 1.1 | 8.8 | 0.52 | 0.75 | 47.1 |
| 6 R2 | 7 | 0.0 | 0.945 | 693.1 | LOS F | 2.3 | 16.1 | 1.00 | 1.05 | 4.7 |
| Approach | 211 | 15.2 | 0.945 | 31.6 | LOS C | 2.3 | 16.1 | 0.54 | 0.76 | 35.9 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 37 | 0.0 | 0.244 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.05 | 57.7 |
| 8 T1 | 783 | 23.2 | 0.244 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.03 | 59.6 |
| Approach | 820 | 22.2 | 0.244 | 0.3 | NA | 0.0 | 0.0 | 0.00 | 0.03 | 59.5 |
| All Vehicles | 3447 | 11.7 | 0.992 | 8.7 | NA | 11.8 | 89.6 | 0.20 | 0.18 | 51.4 |

## MOVEMENT SUMMARY

Site: I-09 2030 MIMT \& SIMTA OPT 2 PM
Moorebank Avenue / Church Road
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1227 | 11.8 | 0.670 | 0.9 | LOS A | 4.5 | 35.5 | 0.02 | 0.02 | 59.0 |
| 3 R2 | 111 | 13.4 | 0.670 | 48.2 | LOS D | 4.5 | 35.5 | 1.00 | 1.05 | 31.5 |
| Approach | 1337 | 11.9 | 0.670 | 4.8 | NA | 4.5 | 35.5 | 0.10 | 0.10 | 54.9 |
| East: Church Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 427 | 5.0 | 1.373 | 224.3 | LOS F | 52.2 | 383.4 | 1.00 | 3.40 | 12.4 |
| 6 R2 | 1 | 0.0 | 0.194 | 647.2 | LOS F | 0.5 | 3.2 | 1.00 | 1.00 | 5.0 |
| Approach | 428 | 5.0 | 1.373 | 225.3 | LOS F | 52.2 | 383.4 | 1.00 | 3.39 | 12.3 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 14 | 7.7 | 0.932 | 7.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 54.7 |
| 8 T1 | 1719 | 6.3 | 0.932 | 2.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 56.2 |
| Approach | 1732 | 6.3 | 0.932 | 2.0 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 56.1 |
| All Vehicles | 3497 | 8.3 | 1.373 | 30.4 | NA | 52.2 | 383.4 | 0.16 | 0.46 | 38.6 |

## I-10 Intersection of Heathcote Road and Nuwarra Road

## MOVEMENT SUMMARY

Site: I-10 2030 MIMT \& SIMTA OPT 2 AM
Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA OPT 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=131$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| SouthEast: Heathcote Road (SE) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 271 | 1.2 | 0.188 | 8.5 | LOS A | 3.8 | 26.9 | 0.28 | 0.63 | 48.0 |
| 5 T1 | 2073 | 5.2 | 1.260 | 171.7 | LOS F | 118.0 | 863.5 | 1.00 | 1.59 | 15.4 |
| 6 R2 | 647 | 3.3 | 1.268 | 159.7 | LOS F | 28.4 | 204.2 | 1.00 | 1.23 | 16.7 |
| Approach | 2991 | 4.4 | 1.268 | 154.3 | LOS F | 118.0 | 863.5 | 0.94 | 1.43 | 16.4 |
| NorthEast: Nuwarra Road (NE) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 416 | 4.8 | 0.484 | 24.5 | LOS B | 16.5 | 120.1 | 0.71 | 0.78 | 42.4 |
| 8 T1 | 275 | 7.7 | 0.440 | 53.4 | LOS D | 8.0 | 59.7 | 0.95 | 0.76 | 26.1 |
| 9 R2 | 508 | 5.8 | 1.436 | 280.3 | LOS F | 34.0 | 249.7 | 1.00 | 1.43 | 10.4 |
| Approach | 1199 | 5.9 | 1.436 | 139.6 | LOS F | 34.0 | 249.7 | 0.89 | 1.05 | 17.1 |
| NorthWest: Heathcote Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 254 | 11.6 | 0.334 | 21.5 | LOS B | 7.8 | 60.1 | 0.70 | 0.76 | 42.7 |
| 11 T1 | 1044 | 11.2 | 0.957 | 51.8 | LOS D | 40.8 | 312.9 | 0.90 | 0.94 | 32.1 |
| 12 R2 | 235 | 6.3 | 0.786 | 75.4 | LOS F | 8.0 | 59.1 | 1.00 | 0.88 | 19.9 |
| Approach | 1532 | 10.5 | 0.957 | 50.4 | LOS D | 40.8 | 312.9 | 0.88 | 0.90 | 31.4 |
| SouthWest: Wattle Grove Drive (SW) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 639 | 2.1 | 0.849 | 51.7 | LOS D | 31.8 | 226.4 | 0.99 | 1.15 | 24.8 |
| 2 T1 | 543 | 4.5 | 0.817 | 61.7 | LOS E | 19.6 | 142.5 | 1.00 | 0.94 | 23.8 |
| 3 R2 | 263 | 4.0 | 1.277 | 207.3 | LOS F | 30.6 | 221.5 | 1.00 | 1.37 | 9.9 |
| Approach | 1445 | 3.4 | 1.277 | 83.8 | LOS F | 31.8 | 226.4 | 0.99 | 1.11 | 19.1 |
| All Vehicles | 7167 | 5.8 | 1.436 | 115.4 | LOS F | 118.0 | 863.5 | 0.93 | 1.19 | 19.0 |

## PHASING SUMMARY

Site: I-10 2030 MIMT \& SIMTA OPT 2 AM
Heathcote Road / Nuwarra Road / Wattle Grove Drive 2030 MIMT \& SIMTA OPT 2 AM PEAK 7:45 am - 8:45 am Signals - Fixed Time Cycle Time = 131 seconds (User-Given Phase Times)

Phase Timing Results

| Phase | A | B | D | E | G |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No | No |
| Phase Change Time (sec) | 0 | 54 | 67 | 86 | 114 |
| Green Time (sec) | 48 | 7 | 13 | 22 | 11 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 54 | 13 | 19 | 28 | 17 |
| Phase Split | $41 \%$ | $10 \%$ | $15 \%$ | $21 \%$ | $13 \%$ |

Phase $A$

## MOVEMENT SUMMARY

## Site: I-10 2030 MIMT \& SIMTA OPT 2 PM

Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA OPT 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=139$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| SouthEast: Heathcote Road (SE) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 337 | 2.5 | 0.282 | 15.4 | LOS B | 8.9 | 63.6 | 0.45 | 0.70 | 42.4 |
| 5 T1 | 1331 | 5.4 | 0.992 | 66.0 | LOS E | 54.7 | 400.4 | 0.93 | 1.05 | 28.4 |
| 6 R2 | 469 | 3.1 | 1.197 | 179.1 | LOS F | 26.2 | 188.2 | 1.00 | 1.22 | 15.3 |
| Approach | 2137 | 4.5 | 1.197 | 82.9 | LOS F | 54.7 | 400.4 | 0.87 | 1.03 | 24.4 |
| NorthEast: Nuwarra Road (NE) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 646 | 2.8 | 0.950 | 74.6 | LOS F | 44.7 | 320.2 | 1.00 | 1.19 | 27.0 |
| 8 T1 | 621 | 1.4 | 0.996 | 88.2 | LOS F | 27.4 | 193.9 | 1.00 | 1.09 | 19.1 |
| $9 \quad \mathrm{R} 2$ | 556 | 7.0 | 1.120 | 135.5 | LOS F | 29.2 | 216.3 | 1.00 | 1.13 | 18.1 |
| Approach | 1823 | 3.6 | 1.120 | 97.8 | LOS F | 44.7 | 320.2 | 1.00 | 1.14 | 21.2 |
| NorthWest: Heathcote Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 258 | 6.1 | 0.232 | 21.3 | LOS B | 8.5 | 62.5 | 0.53 | 0.73 | 43.0 |
| 11 T1 | 1701 | 2.7 | 1.170 | 143.6 | LOS F | 91.8 | 658.0 | 1.00 | 1.40 | 17.6 |
| 12 R2 | 467 | 2.0 | 1.098 | 128.9 | LOS F | 23.4 | 166.5 | 1.00 | 1.09 | 13.6 |
| Approach | 2427 | 3.0 | 1.170 | 127.8 | LOS F | 91.8 | 658.0 | 0.95 | 1.27 | 18.1 |
| SouthWest: Wattle Grove Drive (SW) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 305 | 1.7 | 0.387 | 33.9 | LOS C | 14.1 | 100.1 | 0.76 | 0.85 | 30.6 |
| 2 T1 | 361 | 1.2 | 0.512 | 58.0 | LOS E | 11.3 | 79.5 | 0.96 | 0.79 | 24.6 |
| $3 \quad \mathrm{R} 2$ | 383 | 1.1 | 1.422 | 280.1 | LOS F | 52.2 | 369.0 | 1.00 | 1.48 | 7.7 |
| Approach | 1049 | 1.3 | 1.422 | 132.1 | LOS F | 52.2 | 369.0 | 0.92 | 1.06 | 13.9 |
| All Vehicles | 7437 | 3.3 | 1.422 | 108.1 | LOS F | 91.8 | 658.0 | 0.93 | 1.14 | 19.7 |

## PHASING SUMMARY

Site: I-10 2030 MIMT \& SIMTA OPT 2 PM
Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA OPT 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 139 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E | G |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 63 | 89 | 118 |
| Green Time (sec) | 57 | 20 | 23 | 15 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 63 | 26 | 29 | 21 |
| Phase Split | $45 \%$ | $19 \%$ | $21 \%$ | $15 \%$ |



## I-11 Intersection of Newbridge Road and Nuwarra Road

## MOVEMENT SUMMARY

Site: I-11 2030 MIMT \& SIMTA OPT 2 AM
Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Nuwarra Road (S) per veh er |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 37 | 8.6 | 0.752 | 49.6 | LOS D | 21.6 | 154.3 | 0.90 | 0.83 | 37.4 |
| 2 T1 | 334 | 1.5 | 0.752 | 46.6 | LOS D | 21.6 | 154.3 | 0.90 | 0.83 | 31.1 |
| 3 R2 | 809 | 6.2 | 1.171 | 168.1 | LOS F | 48.7 | 358.7 | 1.00 | 1.21 | 17.5 |
| Approach | 1180 | 4.9 | 1.171 | 130.0 | LOS F | 48.7 | 358.7 | 0.97 | 1.09 | 20.4 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 340 | 16.5 | 0.644 | 28.4 | LOS B | 22.6 | 178.3 | 0.73 | 0.78 | 44.8 |
| 5 T1 | 1300 | 11.8 | 0.644 | 23.7 | LOS B | 23.0 | 178.7 | 0.68 | 0.63 | 51.0 |
| Approach | 1640 | 12.8 | 0.644 | 24.7 | LOS B | 23.0 | 178.7 | 0.69 | 0.66 | 49.7 |
| North: Nuwarra Road (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 8 | 0.0 | 0.978 | 99.7 | LOS F | 10.7 | 75.1 | 1.00 | 1.10 | 23.5 |
| 8 T1 | 151 | 0.7 | 1.223 | 118.2 | LOS F | 20.1 | 145.7 | 1.00 | 1.16 | 20.5 |
| 9 R2 | 142 | 5.2 | 1.223 | 189.4 | LOS F | 20.1 | 145.7 | 1.00 | 1.35 | 16.5 |
| Approach | 301 | 2.8 | 1.223 | 151.3 | LOS F | 20.1 | 145.7 | 1.00 | 1.25 | 18.3 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 305 | 2.1 | 1.161 | 139.8 | LOS F | 93.5 | 699.2 | 1.00 | 1.33 | 20.6 |
| $11 \quad$ T1 | 2307 | 9.8 | 1.235 | 148.3 | LOS F | 107.6 | 826.4 | 1.00 | 1.46 | 21.3 |
| Approach | 2612 | 8.9 | 1.235 | 147.3 | LOS F | 107.6 | 826.4 | 1.00 | 1.44 | 21.3 |
| All Vehicles | 5733 | 8.9 | 1.235 | 108.9 | LOS F | 107.6 | 826.4 | 0.91 | 1.14 | 25.0 |

## PHASING SUMMARY

## Site: I-11 2030 MIMT \& SIMTA OPT 2 AM

Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 140 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 72 | 89 |
| Green Time (sec) | 66 | 11 | 45 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 72 | 17 | 51 |
| Phase Split | $51 \%$ | $12 \%$ | $36 \%$ |



## MOVEMENT SUMMARY

## Site: I-11 2030 MIMT \& SIMTA OPT 2 PM

Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Nuwarra Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 58 | 7.3 | 0.768 | 71.0 | LOS F | 14.7 | 105.1 | 1.00 | 0.89 | 31.8 |
| 2 T1 | 155 | 0.6 | 0.768 | 66.6 | LOS E | 14.7 | 105.1 | 1.00 | 0.89 | 28.9 |
| 3 R 2 | 554 | 6.1 | 0.991 | 100.5 | LOS F | 23.9 | 176.2 | 1.00 | 1.02 | 24.6 |
| Approach | 767 | 5.1 | 0.991 | 91.4 | LOS F | 23.9 | 176.2 | 1.00 | 0.98 | 25.8 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 728 | 3.8 | 0.780 | 18.5 | LOS B | 32.6 | 237.3 | 0.58 | 0.78 | 50.1 |
| 5 T1 | 2231 | 6.1 | 0.780 | 16.4 | LOS B | 39.8 | 295.3 | 0.65 | 0.64 | 55.5 |
| Approach | 2959 | 5.5 | 0.780 | 17.0 | LOS B | 39.8 | 295.3 | 0.64 | 0.67 | 54.2 |
| North: Nuwarra Road (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 17 | 0.0 | 0.844 | 73.2 | LOS F | 17.1 | 120.7 | 1.00 | 0.96 | 29.7 |
| 8 T1 | 281 | 1.1 | 1.055 | 81.3 | LOS F | 25.7 | 182.0 | 1.00 | 1.00 | 26.4 |
| 9 R2 | 213 | 1.5 | 1.055 | 129.0 | LOS F | 25.7 | 182.0 | 1.00 | 1.14 | 22.1 |
| Approach | 511 | 1.2 | 1.055 | 100.9 | LOS F | 25.7 | 182.0 | 1.00 | 1.06 | 24.4 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 103 | 0.0 | 0.550 | 21.6 | LOS B | 17.8 | 132.3 | 0.51 | 0.52 | 48.4 |
| 11 T1 | 1697 | 8.2 | 0.625 | 14.8 | LOS B | 20.7 | 156.0 | 0.51 | 0.47 | 56.8 |
| Approach | 1800 | 7.8 | 0.625 | 15.2 | LOS B | 20.7 | 156.0 | 0.51 | 0.48 | 56.3 |
| All Vehicles | 6036 | 5.8 | 1.055 | 33.0 | LOS C | 39.8 | 295.3 | 0.67 | 0.69 | 44.4 |

## PHASING SUMMARY

## Site: I-11 2030 MIMT \& SIMTA OPT 2 PM

Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 84 | 112 |
| Green Time (sec) | 78 | 22 | 22 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 84 | 28 | 28 |
| Phase Split | $60 \%$ | $20 \%$ | $20 \%$ |



## I-12 Intersection of Newbridge Road and Governor Macquarie Drive

## MOVEMENT SUMMARY

Site: I-12 2030 MIMT \& SIMTA OPT 2 AM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Brickmakers Drive (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 0.0 | 0.867 | 78.5 | LOS F | 15.6 | 110.4 | 1.00 | 0.98 | 25.2 |
| 2 T1 | 197 | 1.0 | 0.867 | 74.1 | LOS F | 15.6 | 110.4 | 1.00 | 0.98 | 24.9 |
| 3 R2 | 684 | 1.2 | 1.177 | 166.5 | LOS F | 36.9 | 260.6 | 1.00 | 1.25 | 19.6 |
| Approach | 895 | 1.1 | 1.177 | 144.8 | LOS F | 36.9 | 260.6 | 1.00 | 1.19 | 20.4 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 230 | 3.0 | 0.168 | 7.7 | LOS A | 1.9 | 13.9 | 0.18 | 0.63 | 58.2 |
| 5 T1 | 1491 | 11.3 | 0.437 | 14.0 | LOS A | 17.0 | 131.5 | 0.55 | 0.50 | 59.8 |
| 6 R2 | 649 | 9.9 | 0.964 | 91.3 | LOS F | 26.2 | 198.7 | 1.00 | 0.98 | 32.2 |
| Approach | 2370 | 10.1 | 0.964 | 34.6 | LOS C | 26.2 | 198.7 | 0.64 | 0.64 | 48.1 |
| North: Governor Macquarie Drive (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 727 | 7.8 | 0.689 | 52.1 | LOS D | 21.9 | 163.5 | 0.94 | 0.85 | 40.3 |
| 8 T1 | 128 | 2.3 | 0.518 | 63.9 | LOS E | 8.3 | 59.5 | 0.98 | 0.79 | 27.0 |
| 9 R2 | 179 | 31.8 | 1.034 | 117.9 | LOS F | 16.5 | 146.8 | 1.00 | 1.07 | 22.7 |
| Approach | 1034 | 11.3 | 1.034 | 65.0 | LOS E | 21.9 | 163.5 | 0.96 | 0.88 | 35.1 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 132 | 29.9 | 1.225 | 165.5 | LOS F | 120.8 | 928.0 | 1.00 | 1.46 | 18.7 |
| 11 T1 | 3009 | 7.4 | 1.225 | 158.2 | LOS F | 124.0 | 931.9 | 1.00 | 1.49 | 24.0 |
| 12 R2 | 5 | 20.0 | 0.046 | 33.1 | LOS C | 0.2 | 1.8 | 0.60 | 0.68 | 37.8 |
| Approach | 3147 | 8.4 | 1.225 | 158.2 | LOS F | 124.0 | 931.9 | 1.00 | 1.48 | 23.8 |
| All Vehicles | 7445 | 8.5 | 1.225 | 104.3 | LOS F | 124.0 | 931.9 | 0.88 | 1.10 | 29.5 |

## PHASING SUMMARY

Site: I-12 2030 MIMT \& SIMTA OPT 2 AM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 140 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E | G1 |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 66 | 88 | 112 |
| Green Time (sec) | 60 | 16 | 18 | 22 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 66 | 22 | 24 | 28 |
| Phase Split | $47 \%$ | $16 \%$ | $17 \%$ | $20 \%$ |



## MOVEMENT SUMMARY

## Site: I-12 2030 MIMT \& SIMTA OPT 2 PM

Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Brickmakers Drive (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 0.0 | 0.530 | 70.2 | LOS E | 6.8 | 49.8 | 0.99 | 0.78 | 26.9 |
| 2 T1 | 92 | 5.4 | 0.530 | 66.1 | LOS E | 6.8 | 49.8 | 0.99 | 0.78 | 26.5 |
| 3 R2 | 257 | 0.8 | 0.609 | 69.8 | LOS E | 8.6 | 60.6 | 1.00 | 0.80 | 32.6 |
| Approach | 360 | 1.9 | 0.609 | 68.9 | LOS E | 8.6 | 60.6 | 1.00 | 0.80 | 31.1 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 654 | 1.4 | 0.461 | 9.4 | LOS A | 7.6 | 53.7 | 0.28 | 0.69 | 57.1 |
| 5 T1 | 2764 | 4.9 | 0.831 | 28.5 | LOS C | 51.9 | 380.6 | 0.76 | 0.77 | 52.0 |
| 6 R2 | 707 | 10.3 | 1.052 | 126.4 | LOS F | 33.5 | 255.2 | 1.00 | 1.06 | 26.9 |
| Approach | 4125 | 5.3 | 1.052 | 42.3 | LOS C | 51.9 | 380.6 | 0.72 | 0.80 | 45.1 |
| North: Governor Macquarie Drive (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 583 | 7.9 | 0.440 | 46.3 | LOS D | 15.7 | 117.1 | 0.85 | 0.81 | 42.1 |
| 8 T1 | 298 | 1.7 | 1.003 | 99.9 | LOS F | 25.1 | 177.9 | 1.00 | 1.09 | 20.9 |
| 9 R2 | 305 | 35.9 | 1.602 | 360.0 | LOS F | 46.6 | 428.5 | 1.00 | 1.47 | 9.9 |
| Approach | 1186 | 13.5 | 1.602 | 140.5 | LOS F | 46.6 | 428.5 | 0.93 | 1.05 | 21.9 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 175 | 15.1 | 0.865 | 46.4 | LOS D | 45.9 | 344.9 | 0.94 | 0.89 | 39.0 |
| 11 T1 | 2086 | 5.6 | 0.865 | 38.4 | LOS C | 46.6 | 343.9 | 0.92 | 0.87 | 47.6 |
| 12 R 2 | 4 | 0.0 | 0.070 | 54.5 | LOS D | 0.2 | 1.7 | 0.80 | 0.69 | 30.3 |
| Approach | 2265 | 6.4 | 0.865 | 39.0 | LOS C | 46.6 | 344.9 | 0.92 | 0.87 | 47.0 |
| All Vehicles | 7935 | 6.7 | 1.602 | 57.2 | LOS E | 51.9 | 428.5 | 0.82 | 0.86 | 39.4 |

## PHASING SUMMARY

Site: I-12 2030 MIMT \& SIMTA OPT 2 PM

## Newbridge Road / Governor Macquarie Drive

2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 140 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E | G1 |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 64 | 86 | 107 |
| Green Time (sec) | 58 | 16 | 15 | 27 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 64 | 22 | 21 | 33 |
| Phase Split | $46 \%$ | $16 \%$ | $15 \%$ | $24 \%$ |



## I-13 Intersection of Moorebank Avenue and M5 Motorway

## MOVEMENT SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 2 AM
Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 74 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Deman <br> Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn <br> v/c | Average Delay sec | Level of Service | 95\% Bac <br> Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 398 | 36.3 | 0.439 | 10.4 | LOS A | 5.1 | 54.4 | 0.49 | 0.70 | 48.6 |
| 2 T1 | 716 | 10.5 | 0.878 | 39.8 | LOS C | 15.2 | 121.1 | 1.00 | 1.05 | 34.9 |
| 3 R2 | 319 | 6.3 | 0.463 | 33.5 | LOS C | 5.7 | 43.2 | 0.91 | 0.79 | 36.6 |
| Approach | 1434 | 16.7 | 0.878 | 30.2 | LOS C | 15.2 | 121.1 | 0.84 | 0.90 | 38.3 |
| East: M5 Motorway on\&off ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 323 | 14.5 | 0.428 | 11.8 | LOS A | 4.7 | 39.0 | 0.62 | 0.74 | 48.4 |
| 6 R2 | 237 | 6.2 | 0.246 | 28.8 | LOS C | 3.4 | 25.1 | 0.82 | 0.76 | 40.4 |
| Approach | 559 | 11.0 | 0.428 | 19.0 | LOS B | 4.7 | 39.0 | 0.71 | 0.75 | 44.4 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 51 | 47.9 | 0.050 | 7.9 | LOS A | 0.4 | 3.5 | 0.29 | 0.60 | 51.1 |
| 8 T1 | 253 | 19.7 | 0.331 | 26.4 | LOS B | 3.9 | 34.2 | 0.88 | 0.70 | 40.6 |
| 9 R2 | 454 | 25.5 | 0.772 | 37.8 | LOS C | 10.0 | 85.1 | 0.97 | 0.87 | 36.3 |
| Approach | 757 | 25.1 | 0.772 | 32.0 | LOS C | 10.0 | 85.1 | 0.90 | 0.80 | 38.3 |
| West: M5 Motorway on\&off ramp (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1722 | 7.5 | 0.977 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.50 | 51.6 |
| 12 R2 | 680 | 19.4 | 0.824 | 40.1 | LOS C | 13.5 | 121.9 | 1.00 | 0.97 | 34.2 |
| Approach | 2403 | 10.8 | 0.977 | 17.0 | LOS B | 13.5 | 121.9 | 0.28 | 0.63 | 45.6 |
| All Vehicles | 5153 | 14.6 | 0.977 | 23.1 | LOS B | 15.2 | 121.9 | 0.57 | 0.74 | 42.2 |

## PHASING SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 2 AM
Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=74$ seconds (User-Given Phase Times)

| Phase Timing Results | A | E | F |
| :--- | :---: | :---: | :---: |
| Phase | Yes | No | No |
| Reference Phase | 0 | 24 | 51 |
| Phase Change Time (sec) | 17 | 20 | 16 |
| Green Time (sec) | 4 | 4 | 4 |
| Yellow Time (sec) | 3 | 3 | 3 |
| All-Red Time (sec) | 24 | 27 | 23 |
| Phase Time (sec) | $32 \%$ | $36 \%$ | $31 \%$ |
| Phase Split |  |  |  |



## MOVEMENT SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 2 PM
Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=94$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 639 | 17.8 | 0.959 | 61.4 | LOS E | 38.9 | 347.0 | 1.00 | 1.12 | 28.1 |
| 2 T1 | 248 | 14.6 | 0.968 | 72.9 | LOS F | 7.6 | 63.5 | 1.00 | 1.15 | 25.9 |
| 3 R2 | 411 | 9.9 | 0.372 | 29.3 | LOS C | 7.7 | 61.5 | 0.77 | 0.78 | 38.3 |
| Approach | 1298 | 14.7 | 0.968 | 53.4 | LOS D | 38.9 | 347.0 | 0.93 | 1.01 | 30.1 |
| East: M5 Motorway on\&off ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 460 | 7.3 | 0.572 | 17.0 | LOS B | 9.3 | 71.0 | 0.70 | 0.81 | 45.2 |
| 6 R2 | 97 | 21.7 | 0.177 | 42.7 | LOS D | 2.0 | 16.2 | 0.89 | 0.73 | 34.9 |
| Approach | 557 | 9.8 | 0.572 | 21.5 | LOS B | 9.3 | 71.0 | 0.74 | 0.80 | 42.8 |
| North: Moorebank Avenue ( N ) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 139 | 6.1 | 0.116 | 7.7 | LOS A | 1.3 | 9.3 | 0.29 | 0.63 | 52.4 |
| 8 T1 | 757 | 7.5 | 0.846 | 44.1 | LOS D | 18.9 | 144.8 | 1.00 | 1.01 | 33.3 |
| 9 R2 | 1488 | 7.0 | 0.920 | 43.0 | LOS D | 34.3 | 254.6 | 1.00 | 1.06 | 34.8 |
| Approach | 2384 | 7.1 | 0.920 | 41.3 | LOS C | 34.3 | 254.6 | 0.96 | 1.02 | 35.0 |
| West: M5 Motorway on\&off ramp (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 620 | 13.8 | 0.367 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 54.4 |
| 12 R2 | 365 | 32.7 | 0.792 | 53.0 | LOS D | 9.1 | 95.7 | 1.00 | 0.94 | 30.0 |
| Approach | 985 | 20.8 | 0.792 | 23.3 | LOS B | 9.1 | 95.7 | 0.37 | 0.68 | 42.5 |
| All Vehicles | 5223 | 11.9 | 0.968 | 38.8 | LOS C | 38.9 | 347.0 | 0.82 | 0.93 | 35.5 |

## PHASING SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 2 PM

## Moorebank Avenue / the M5 Motorway

2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 94 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | C | E | F |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 14 | 30 | 53 |
| Green Time (sec) | 7 | 9 | 16 | 34 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 | 3 |
| Phase Time (sec) | 14 | 16 | 23 | 41 |
| Phase Split | $15 \%$ | $17 \%$ | $24 \%$ | $44 \%$ |



## I-14 Intersection of M5 Motorway and Hume Highway

## MOVEMENT SUMMARY

Site: I-14 2030 MIMT \& SIMTA OPT 2 AM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=159$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 4256 | 4.6 | 1.027 | 59.4 | LOS E | 152.3 | 1108.5 | 1.00 | 1.21 | 33.2 |
| 3 R2 | 680 | 4.0 | 0.936 | 50.9 | LOS D | 20.3 | 146.7 | 1.00 | 0.95 | 35.4 |
| Approach | 4936 | 4.5 | 1.027 | 58.3 | LOS E | 152.3 | 1108.5 | 1.00 | 1.17 | 33.5 |
| East: M5 Motorway on\&off-ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 338 | 5.9 | 0.134 | 30.5 | LOS C | 4.8 | 35.4 | 0.60 | 0.71 | 41.9 |
| 6 R2 | 1211 | 6.4 | 1.287 | 357.4 | LOS F | 74.2 | 558.7 | 1.00 | 1.54 | 7.2 |
| Approach | 1549 | 6.3 | 1.287 | 286.1 | LOS F | 74.2 | 558.7 | 0.91 | 1.36 | 9.6 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 780 | 9.5 | 0.653 | 14.0 | LOS A | 25.0 | 194.9 | 0.53 | 0.74 | 45.7 |
| 8 T1 | 1208 | 6.7 | 0.490 | 28.5 | LOS B | 17.8 | 131.7 | 0.62 | 0.55 | 43.3 |
| Approach | 1988 | 7.8 | 0.653 | 22.8 | LOS B | 25.0 | 194.9 | 0.59 | 0.62 | 44.0 |
| All Vehicles | 8472 | 5.6 | 1.287 | 91.6 | LOS F | 152.3 | 1108.5 | 0.89 | 1.08 | 25.5 |

## PHASING SUMMARY

Site: I-14 2030 MIMT \& SIMTA OPT 2 AM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)

## Phase Timing Results

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | No | No | No | Yes |
| Phase Change Time (sec) | 20 | 97 | 123 | 0 |
| Green Time (sec) | 70 | 19 | 29 | 13 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 | 3 |
| Phase Time (sec) | 77 | 26 | 36 | 20 |
| Phase Split | $48 \%$ | $16 \%$ | $23 \%$ | $13 \%$ |

Phase A

## MOVEMENT SUMMARY

## Site: I-14 2030 MIMT \& SIMTA OPT 2 PM

M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=159$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 2555 | 3.9 | 0.624 | 2.2 | LOS A | 7.1 | 51.1 | 0.12 | 0.11 | 58.3 |
| 3 R 2 | 401 | 1.8 | 1.023 | 122.1 | LOS F | 20.4 | 145.1 | 1.00 | 1.07 | 22.6 |
| Approach | 2956 | 3.6 | 1.023 | 18.4 | LOS B | 20.4 | 145.1 | 0.24 | 0.24 | 48.0 |
| East: M5 Motorway on\&off-ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1513 | 3.3 | 1.138 | 245.4 | LOS F | 98.0 | 705.7 | 1.00 | 1.33 | 13.8 |
| 6 R2 | 1265 | 5.7 | 1.276 | 348.8 | LOS F | 78.1 | 583.7 | 1.00 | 1.52 | 7.4 |
| Approach | 2777 | 4.4 | 1.276 | 292.5 | LOS F | 98.0 | 705.7 | 1.00 | 1.42 | 10.5 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 884 | 5.7 | 0.697 | 14.5 | LOS B | 27.6 | 208.5 | 0.61 | 0.82 | 45.6 |
| 8 T1 | 2837 | 2.4 | 0.870 | 20.5 | LOS B | 51.6 | 368.7 | 0.78 | 0.73 | 47.0 |
| Approach | 3721 | 3.2 | 0.870 | 19.1 | LOS B | 51.6 | 368.7 | 0.74 | 0.75 | 46.7 |
| All Vehicles | 9454 | 3.7 | 1.276 | 99.2 | LOS F | 98.0 | 705.7 | 0.66 | 0.79 | 24.4 |

## PHASING SUMMARY

## Site: I-14 2030 MIMT \& SIMTA OPT 2 PM

M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 97 | 121 |
| Green Time (sec) | 90 | 17 | 31 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 |
| Phase Time (sec) | 97 | 24 | 38 |
| Phase Split | $61 \%$ | $15 \%$ | $24 \%$ |

Phase A

## I-15 Intersection of Cambridge Avenue and Canterbury Road MOVEMENT SUMMARY

Site: I-15 2030 MIMT \& SIMTA OPT 2 AM
Canterbury Road / Cambridge Avenue / Glenfield Road 2030 MIMT \& SIMTA Opt 2 AM PEAK 7:45 am - 8:45 am
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Canterbury Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 449 | 3.5 | 0.503 | 6.1 | LOS A | 3.2 | 22.9 | 0.60 | 0.69 | 52.9 |
| 2 T1 | 8 | 0.0 | 0.888 | 10.5 | LOS A | 16.4 | 117.0 | 0.95 | 0.95 | 49.1 |
| 3 R 2 | 1095 | 1.9 | 0.888 | 15.9 | LOS B | 16.4 | 117.0 | 0.95 | 0.95 | 49.2 |
| Approach | 1553 | 2.4 | 0.888 | 13.0 | LOS A | 16.4 | 117.0 | 0.85 | 0.87 | 50.1 |
| East: Cambridge Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 307 | 3.1 | 0.163 | 3.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.43 | 56.5 |
| 5 T1 | 81 | 7.8 | 0.082 | 5.1 | LOS A | 0.5 | 3.4 | 0.50 | 0.56 | 53.5 |
| 6 R2 | 54 | 9.8 | 0.082 | 10.4 | LOS A | 0.5 | 3.4 | 0.49 | 0.59 | 53.7 |
| Approach | 442 | 4.8 | 0.163 | 4.6 | LOS A | 0.5 | 3.4 | 0.15 | 0.47 | 55.6 |
| North: Railway Parade (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 338 | 0.6 | 0.871 | 55.5 | LOS D | 13.3 | 93.7 | 1.00 | 1.54 | 31.3 |
| 8 T1 | 3 | 0.0 | 0.611 | 29.4 | LOS C | 4.8 | 33.9 | 0.99 | 1.15 | 39.5 |
| 9 R2 | 168 | 1.9 | 0.611 | 34.8 | LOS C | 4.8 | 33.9 | 0.99 | 1.15 | 37.7 |
| Approach | 509 | 1.0 | 0.871 | 48.5 | LOS D | 13.3 | 93.7 | 1.00 | 1.41 | 33.1 |
| West: Glenfield Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 399 | 6.3 | 1.480 | 470.5 | LOS F | 129.3 | 956.8 | 1.00 | 4.85 | 6.1 |
| 11 T1 | 222 | 7.6 | 1.480 | 471.2 | LOS F | 129.3 | 956.8 | 1.00 | 4.68 | 6.1 |
| 12 R2 | 367 | 6.9 | 1.480 | 478.2 | LOS F | 104.4 | 774.9 | 1.00 | 4.34 | 6.3 |
| Approach | 988 | 6.8 | 1.480 | 473.5 | LOS F | 129.3 | 956.8 | 1.00 | 4.62 | 6.2 |
| All Vehicles | 3493 | 3.7 | 1.480 | 147.5 | LOS F | 129.3 | 956.8 | 0.83 | 1.96 | 17.1 |

## MOVEMENT SUMMARY

$\theta$ Site: I-15 2030 MIMT \& SIMTA OPT 2 PM
Canterbury Road / Cambridge Avenue / Glenfield Road 2030 MIMT \& SIMTA Opt 2 PM PEAK 4:30 pm - 5:30 pm
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Deman <br> Total veh/h | lows <br> HV \% | Deg. Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Canterbury Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 338 | 2.2 | 0.493 | 9.4 | LOS A | 3.3 | 23.3 | 0.81 | 0.95 | 50.5 |
| 2 T1 | 6 | 0.0 | 0.417 | 7.6 | LOS A | 2.7 | 18.8 | 0.78 | 0.94 | 51.0 |
| 3 R2 | 334 | 1.3 | 0.417 | 13.0 | LOS A | 2.7 | 18.8 | 0.78 | 0.94 | 51.2 |
| Approach | 678 | 1.7 | 0.493 | 11.1 | LOS A | 3.3 | 23.3 | 0.79 | 0.94 | 50.9 |
| East: Cambridge Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1232 | 2.1 | 0.649 | 3.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.43 | 56.3 |
| 5 T1 | 315 | 7.4 | 0.486 | 7.4 | LOS A | 4.1 | 29.4 | 0.77 | 0.78 | 51.9 |
| 6 R2 | 356 | 0.9 | 0.486 | 12.7 | LOS A | 4.1 | 29.4 | 0.83 | 0.82 | 52.0 |
| Approach | 1902 | 2.7 | 0.649 | 5.9 | LOS A | 4.1 | 29.4 | 0.28 | 0.56 | 54.7 |
| North: Railway Parade (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 125 | 1.7 | 0.192 | 7.9 | LOS A | 1.0 | 6.9 | 0.69 | 0.80 | 52.8 |
| 8 T1 | 0 | 0.0 | 0.000 | 0.0 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.0 |
| 9 R2 | 240 | 8.3 | 0.295 | 12.7 | LOS A | 1.7 | 12.7 | 0.73 | 0.86 | 50.0 |
| Approach | 365 | 6.1 | 0.295 | 11.0 | LOS A | 1.7 | 12.7 | 0.71 | 0.84 | 51.0 |
| West: Glenfield Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 271 | 4.7 | 0.442 | 9.0 | LOS A | 3.0 | 21.7 | 0.78 | 0.87 | 50.8 |
| 11 T1 | 54 | 0.0 | 0.442 | 8.8 | LOS A | 3.0 | 21.7 | 0.78 | 0.87 | 52.7 |
| 12 R2 | 451 | 3.7 | 0.513 | 14.2 | LOS A | 4.1 | 29.9 | 0.81 | 0.93 | 49.0 |
| Approach | 775 | 3.8 | 0.513 | 12.0 | LOS A | 4.1 | 29.9 | 0.80 | 0.90 | 49.9 |
| All Vehicles | 3720 | 3.1 | 0.649 | 8.6 | LOS A | 4.1 | 29.9 | 0.53 | 0.73 | 52.6 |

## 6. On the wider road network - 2030 cumulative scenario 3

## I-01 Intersection of the Hume Highway and Orange Grove Road

## MOVEMENT SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand <br> Total | Flows HV | Deg. Satn | Average Delay | Level of Service | 95\% Bac <br> Vehicles | of Queue <br> Distance | Prop. Queued | Effective Stop Rate | Average Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| NorthEast: Hume Highway (NE) |  |  |  |  |  |  |  |  |  |  |
| 25 T1 | 991 | 10.8 | 0.709 | 24.9 | LOS B | 20.7 | 158.2 | 0.85 | 0.78 | 35.4 |
| 26 R2 | 389 | 10.0 | 0.907 | 85.9 | LOS F | 16.8 | 127.3 | 1.00 | 0.92 | 23.9 |
| Approach | 1381 | 10.6 | 0.907 | 42.1 | LOS C | 20.7 | 158.2 | 0.90 | 0.82 | 30.0 |
| NorthWest: Orange Grove Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 602 | 6.5 | 0.712 | 18.8 | LOS B | 19.5 | 144.4 | 0.54 | 0.81 | 44.8 |
| 29 R2 | 1371 | 8.4 | 1.019 | 107.8 | LOS F | 45.1 | 343.5 | 1.00 | 1.03 | 18.2 |
| Approach | 1973 | 7.8 | 1.073 | 80.7 | LOS F | 45.1 | 343.5 | 0.86 | 0.96 | 22.8 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 1281 | 8.6 | 0.462 | 11.7 | LOS A | 14.5 | 110.4 | 0.34 | 0.70 | 50.1 |
| 31 T1 | 2186 | 4.9 | 0.805 | 22.9 | LOS B | 39.5 | 287.9 | 0.71 | 0.65 | 40.2 |
| Approach | 3468 | 6.3 | 0.805 | 18.7 | LOS B | 39.5 | 287.9 | 0.57 | 0.67 | 44.0 |
| All Vehicles | 6821 | 7.6 | 1.073 | 41.4 | LOS C | 45.1 | 343.5 | 0.72 | 0.78 | 31.4 |

## PHASING SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 84 | 108 |
| Green Time (sec) | 77 | 17 | 36 |
| Yellow Time (sec) | 5 | 4 | 5 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 84 | 23 | 43 |
| Phase Split | $56 \%$ | $15 \%$ | $29 \%$ |



## MOVEMENT SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 3 PM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| NorthEast: Hume Highway (NE) |  |  |  |  |  |  |  |  |  |  |
| 25 T1 | 1766 | 3.5 | 0.921 | 42.1 | LOS C | 48.3 | 348.2 | 0.91 | 0.96 | 27.6 |
| 26 R2 | 816 | 2.8 | 0.958 | 61.5 | LOS E | 22.8 | 163.7 | 1.00 | 1.00 | 29.2 |
| Approach | 2581 | 3.3 | 0.958 | 48.3 | LOS D | 48.3 | 348.2 | 0.94 | 0.97 | 28.2 |
| NorthWest: Orange Grove Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 391 | 4.3 | 0.393 | 14.2 | LOS A | 8.3 | 60.0 | 0.33 | 0.66 | 48.0 |
| 29 R2 | 1383 | 4.9 | 1.085 | 118.6 | LOS F | 50.0 | 369.5 | 1.00 | 1.07 | 17.1 |
| Approach | 1774 | 4.8 | 1.085 | 95.6 | LOS F | 50.0 | 369.5 | 0.85 | 0.98 | 20.3 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 1330 | 4.7 | 0.791 | 19.8 | LOS B | 21.2 | 156.6 | 0.80 | 0.84 | 44.7 |
| 31 T1 | 1123 | 5.3 | 1.009 | 90.7 | LOS F | 38.2 | 280.2 | 1.00 | 1.11 | 17.7 |
| Approach | 2453 | 5.0 | 1.009 | 52.2 | LOS D | 38.2 | 280.2 | 0.89 | 0.97 | 28.1 |
| All Vehicles | 6809 | 4.3 | 1.085 | 62.0 | LOS E | 50.0 | 369.5 | 0.90 | 0.97 | 25.3 |

## PHASING SUMMARY

Site: I-01 2030 MIMT \& SIMTA OPT 3 PM
Hume Highway / Orange Grove Road
2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)
Phase times specified by the user
Sequence: TCS 866 PM - Modified
Movement Class: All Movement Classes
Input Sequence: A, B, C, D
Output Sequence: A, B, C, D
Phase Timing Results

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 53 | 80 | 124 |
| Green Time (sec) | 47 | 20 | 38 | 19 |
| Yellow Time (sec) | 5 | 4 | 5 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 54 | 26 | 45 | 25 |
| Phase Split | $36 \%$ | $17 \%$ | $30 \%$ | $17 \%$ |



## I-02 Intersection of the Hume Highway and Elizabeth Drive

## MOVEMENT SUMMARY

Site: I-02 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) per pren |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 137 | 5.4 | 0.155 | 22.6 | LOS B | 3.7 | 27.3 | 0.40 | 0.68 | 36.5 |
| 2 T1 | 2385 | 7.6 | 0.969 | 61.6 | LOS E | 68.1 | 512.0 | 0.99 | 1.03 | 19.6 |
| Approach | 2522 | 7.5 | 0.989 | 59.5 | LOS E | 68.1 | 512.0 | 0.95 | 1.01 | 20.2 |
| East: Elizabeth Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 39 | 5.4 | 0.426 | 59.6 | LOS E | 10.5 | 77.4 | 0.91 | 0.82 | 18.6 |
| 5 T1 | 502 | 5.7 | 0.426 | 55.8 | LOS D | 11.9 | 87.2 | 0.90 | 0.82 | 23.7 |
| 6 R2 | 156 | 2.7 | 0.754 | 78.1 | LOS F | 11.7 | 83.5 | 1.00 | 0.87 | 14.8 |
| Approach | 697 | 5.0 | 0.754 | 61.0 | LOS E | 11.9 | 87.2 | 0.92 | 0.83 | 21.1 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 82 | 2.6 | 0.666 | 26.1 | LOS B | 25.3 | 192.5 | 0.62 | 0.59 | 31.4 |
| 8 T1 | 1813 | 9.9 | 0.666 | 20.0 | LOS B | 25.7 | 196.8 | 0.61 | 0.56 | 35.8 |
| 9 R2 | 353 | 9.6 | 1.170 | 171.2 | LOS F | 19.8 | 149.6 | 1.00 | 1.15 | 10.5 |
| Approach | 2247 | 9.5 | 1.170 | 44.0 | LOS D | 25.7 | 196.8 | 0.67 | 0.66 | 24.7 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 627 | 5.2 | 1.011 | 93.3 | LOS F | 57.3 | 419.3 | 1.00 | 1.01 | 16.3 |
| 11 T1 | 1089 | 3.0 | 1.050 | 107.6 | LOS F | 52.2 | 375.0 | 1.00 | 1.18 | 14.2 |
| 12 R2 | 522 | 7.0 | 1.305 | 231.6 | LOS F | 33.9 | 252.9 | 1.00 | 1.27 | 8.2 |
| Approach | 2239 | 4.5 | 1.305 | 132.5 | LOS F | 57.3 | 419.3 | 1.00 | 1.15 | 12.4 |
| All Vehicles | 7705 | 7.0 | 1.305 | 76.3 | LOS F | 68.1 | 512.0 | 0.88 | 0.93 | 17.7 |

## PHASING SUMMARY

Site: I-02 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)


## MOVEMENT SUMMARY

Site: I-02 2030 MIMT \& SIMTA OPT 3 PM
Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Deman | Flows | Deg. Satn | Average | Level of | 95\% Bac | of Queue | Prop. | Effective | Average |
| v | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 326 | 5.2 | 0.481 | 39.9 | LOS C | 15.4 | 113.2 | 0.70 | 0.78 | 28.3 |
| 2 T1 | 1587 | 6.3 | 0.956 | 71.7 | LOS F | 46.4 | 345.9 | 0.98 | 1.03 | 17.7 |
| Approach | 1913 | 6.1 | 0.956 | 66.3 | LOS E | 46.4 | 345.9 | 0.93 | 0.99 | 19.1 |
| East: Elizabeth Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 128 | 0.8 | 0.984 | 98.9 | LOS F | 31.7 | 225.4 | 1.00 | 1.08 | 12.9 |
| 5 T1 | 1082 | 2.3 | 0.984 | 94.6 | LOS F | 40.3 | 287.5 | 1.00 | 1.10 | 16.3 |
| 6 R2 | 172 | 0.0 | 1.066 | 131.4 | LOS F | 17.1 | 119.5 | 1.00 | 1.12 | 9.9 |
| Approach | 1382 | 1.9 | 1.066 | 99.6 | LOS F | 40.3 | 287.5 | 1.00 | 1.10 | 15.0 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 66 | 4.8 | 0.874 | 25.4 | LOS B | 43.2 | 315.6 | 0.74 | 0.72 | 32.1 |
| 8 T1 | 2473 | 4.0 | 0.874 | 19.5 | LOS B | 44.0 | 320.9 | 0.74 | 0.71 | 36.2 |
| 9 R2 | 961 | 3.0 | 0.917 | 75.8 | LOS F | 37.4 | 268.2 | 1.00 | 0.94 | 19.6 |
| Approach | 3501 | 3.7 | 0.917 | 35.1 | LOS C | 44.0 | 320.9 | 0.81 | 0.78 | 28.6 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 325 | 5.8 | 0.434 | 34.2 | LOS C | 13.6 | 100.2 | 0.62 | 0.76 | 29.6 |
| 11 T1 | 529 | 4.4 | 0.698 | 61.8 | LOS E | 17.6 | 127.6 | 0.96 | 0.82 | 20.9 |
| 12 R2 | 309 | 2.4 | 0.978 | 105.6 | LOS F | 13.7 | 98.2 | 1.00 | 1.00 | 15.4 |
| Approach | 1164 | 4.2 | 0.978 | 65.7 | LOS E | 17.6 | 127.6 | 0.88 | 0.85 | 20.6 |
| All Vehicles | 7960 | 4.1 | 1.066 | 58.2 | LOS E | 46.4 | 345.9 | 0.88 | 0.90 | 21.4 |

## PHASING SUMMARY

## Site: I-02 2030 MIMT \& SIMTA OPT 3 PM

Hume Highway / Elizabeth Drive
2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | D | F | A | E |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 53 | 72 | 108 |
| Green Time (sec) | 47 | 13 | 30 | 36 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 53 | 19 | 36 | 42 |
| Phase Split | $35 \%$ | $13 \%$ | $24 \%$ | $28 \%$ |



## I-03 Intersection of the Hume Highway and Memorial Avenue

## MOVEMENT SUMMARY

Site: I-03 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 157 | 1.3 | 0.976 | 67.6 | LOS E | 68.6 | 512.6 | 1.00 | 1.06 | 27.0 |
| 2 T1 | 2130 | 8.4 | 0.976 | 59.3 | LOS E | 69.9 | 529.1 | 0.94 | 1.01 | 25.3 |
| 3 R2 | 267 | 0.0 | 1.137 | 158.3 | LOS F | 29.3 | 204.9 | 1.00 | 1.12 | 12.4 |
| Approach | 2554 | 7.1 | 1.137 | 70.1 | LOS E | 69.9 | 529.1 | 0.95 | 1.03 | 23.1 |
| East: Memorial Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 29 | 28.6 | 1.264 | 214.3 | LOS F | 21.6 | 165.9 | 1.00 | 1.33 | 9.8 |
| 5 T1 | 164 | 7.7 | 1.264 | 209.5 | LOS F | 21.6 | 165.9 | 1.00 | 1.33 | 9.6 |
| 6 R2 | 134 | 18.1 | 1.264 | 214.6 | LOS F | 19.4 | 155.3 | 1.00 | 1.32 | 6.9 |
| Approach | 327 | 13.8 | 1.264 | 212.0 | LOS F | 21.6 | 165.9 | 1.00 | 1.33 | 8.6 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 121 | 6.1 | 0.103 | 12.4 | LOS A | 2.6 | 19.4 | 0.36 | 0.64 | 39.4 |
| 8 T1 | 1826 | 12.3 | 0.784 | 29.0 | LOS C | 34.8 | 272.3 | 0.77 | 0.69 | 36.0 |
| 9 R2 | 101 | 3.1 | 0.439 | 72.0 | LOS F | 7.0 | 50.1 | 0.97 | 0.79 | 21.4 |
| Approach | 2048 | 11.5 | 0.784 | 30.1 | LOS C | 34.8 | 272.3 | 0.75 | 0.69 | 34.9 |
| West: Memorial Avenue (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 128 | 3.3 | 1.187 | 160.9 | LOS F | 36.6 | 261.2 | 1.00 | 1.28 | 12.5 |
| 11 T1 | 460 | 1.6 | 1.187 | 163.7 | LOS F | 46.9 | 334.6 | 1.00 | 1.31 | 11.6 |
| 12 R2 | 169 | 3.1 | 1.187 | 175.5 | LOS F | 46.9 | 334.6 | 1.00 | 1.35 | 14.5 |
| Approach | 757 | 2.2 | 1.187 | 165.9 | LOS F | 46.9 | 334.6 | 1.00 | 1.31 | 12.4 |
| All Vehicles | 5687 | 8.4 | 1.264 | 76.7 | LOS F | 69.9 | 529.1 | 0.89 | 0.96 | 21.3 |

## PHASING SUMMARY

## Site: I-03 2030 MIMT \& SIMTA OPT 3 AM

Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Phase Timing Results | A | D | E | F |
| :--- | :---: | :---: | :---: | :---: |
| Phase | Yes | No | No | No |
| Reference Phase | 0 | 75 | 108 | 125 |
| Phase Change Time (sec) | 69 | 27 | 11 | 19 |
| Green Time (sec) | 4 | 4 | 4 | 4 |
| Yellow Time (sec) | 2 | 2 | 2 | 2 |
| All-Red Time (sec) | 75 | 33 | 17 | 25 |
| Phase Time (sec) | $50 \%$ | $22 \%$ | $11 \%$ | $17 \%$ |
| Phase Split |  |  |  |  |

Phase A Phase D

## MOVEMENT SUMMARY

## Site: I-03 2030 MIMT \& SIMTA OPT 3 PM

Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 124 | 0.8 | 0.848 | 49.7 | LOS D | 40.0 | 295.8 | 0.93 | 0.90 | 31.4 |
| 2 T1 | 1699 | 6.7 | 0.848 | 41.5 | LOS C | 40.8 | 306.0 | 0.89 | 0.84 | 30.6 |
| 3 R2 | 116 | 0.0 | 0.779 | 84.4 | LOS F | 8.9 | 62.5 | 1.00 | 0.86 | 19.4 |
| Approach | 1939 | 6.0 | 0.848 | 44.6 | LOS D | 40.8 | 306.0 | 0.90 | 0.85 | 29.7 |
| East: Memorial Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 55 | 0.0 | 1.228 | 195.7 | LOS F | 34.9 | 247.9 | 1.00 | 1.40 | 10.7 |
| 5 T1 | 289 | 2.2 | 1.228 | 191.2 | LOS F | 34.9 | 247.9 | 1.00 | 1.39 | 10.3 |
| 6 R2 | 211 | 6.0 | 1.228 | 196.2 | LOS F | 32.3 | 235.9 | 1.00 | 1.32 | 7.5 |
| Approach | 555 | 3.4 | 1.228 | 193.5 | LOS F | 34.9 | 247.9 | 1.00 | 1.37 | 9.3 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 152 | 2.8 | 0.090 | 8.4 | LOS A | 2.0 | 14.7 | 0.24 | 0.61 | 43.5 |
| 8 T1 | 2954 | 3.7 | 0.937 | 19.5 | LOS B | 63.5 | 461.8 | 0.68 | 0.68 | 41.5 |
| $9 \quad \mathrm{R} 2$ | 214 | 2.0 | 0.729 | 42.6 | LOS D | 9.2 | 65.2 | 1.00 | 0.83 | 28.2 |
| Approach | 3320 | 3.6 | 0.937 | 20.5 | LOS B | 63.5 | 461.8 | 0.68 | 0.69 | 40.3 |
| West: Memorial Avenue (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 82 | 1.3 | 0.947 | 89.9 | LOS F | 17.2 | 121.7 | 1.00 | 1.08 | 18.9 |
| 11 T1 | 209 | 1.0 | 0.947 | 86.8 | LOS F | 21.4 | 150.2 | 1.00 | 1.06 | 18.0 |
| 12 R2 | 171 | 0.0 | 0.947 | 93.9 | LOS F | 21.4 | 150.2 | 1.00 | 1.03 | 21.9 |
| Approach | 462 | 0.7 | 0.947 | 90.0 | LOS F | 21.4 | 150.2 | 1.00 | 1.05 | 19.7 |
| All Vehicles | 6276 | 4.1 | 1.228 | 48.4 | LOS D | 63.5 | 461.8 | 0.80 | 0.82 | 27.8 |

## PHASING SUMMARY

## Site: I-03 2030 MIMT \& SIMTA OPT 3 PM

Hume Highway / Memorial Avenue
2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)

## Phase Timing Results

| Phase | A | C | D | E | F |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No | No |
| Phase Change Time (sec) | 0 | 67 | 81 | 108 | 132 |
| Green Time (sec) | 61 | 8 | 21 | 18 | 12 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 67 | 14 | 27 | 24 | 18 |
| Phase Split | $45 \%$ | $9 \%$ | $18 \%$ | $16 \%$ | $12 \%$ |

## I-04 Intersection of the Hume Highway and Hoxton Park Drive

## MOVEMENT SUMMARY

Site: I-04 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Hoxton Park Road / Macquarie Street 2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) per |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 109 | 12.9 | 0.096 | 8.8 | LOS A | 0.9 | 7.2 | 0.13 | 0.57 | 50.6 |
| 2 T1 | 2154 | 6.3 | 0.848 | 31.1 | LOS C | 43.9 | 326.7 | 0.83 | 0.77 | 38.1 |
| 3 R2 | 1213 | 1.9 | 1.038 | 98.4 | LOS F | 46.4 | 330.1 | 1.00 | 1.09 | 17.7 |
| Approach | 3475 | 5.0 | 1.038 | 53.9 | LOS D | 46.4 | 330.1 | 0.87 | 0.88 | 28.7 |
| East: Macquarie Street (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 361 | 5.8 | 0.230 | 21.3 | LOS B | 5.5 | 40.4 | 0.66 | 0.73 | 39.0 |
| 5 T1 | 545 | 4.6 | 1.080 | 130.0 | LOS F | 27.8 | 202.5 | 1.00 | 1.19 | 16.2 |
| Approach | 906 | 5.1 | 1.080 | 86.7 | LOS F | 27.8 | 202.5 | 0.86 | 1.01 | 20.6 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 236 | 15.6 | 1.045 | 61.2 | LOS E | 47.8 | 371.9 | 1.00 | 1.02 | 25.9 |
| 8 T1 | 1543 | 9.6 | 1.045 | 94.3 | LOS F | 60.0 | 460.7 | 1.00 | 1.13 | 21.8 |
| 9 R2 | 246 | 19.2 | 1.257 | 211.1 | LOS F | 30.8 | 251.3 | 1.00 | 1.27 | 13.2 |
| Approach | 2025 | 11.5 | 1.257 | 104.7 | LOS F | 60.0 | 460.7 | 1.00 | 1.14 | 20.3 |
| West: Hoxton Park Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 345 | 18.0 | 0.583 | 47.3 | LOS D | 20.3 | 164.2 | 0.87 | 0.83 | 32.5 |
| 11 T1 | 1372 | 4.8 | 1.132 | 165.1 | LOS F | 55.7 | 406.4 | 1.00 | 1.34 | 13.5 |
| 12 R2 | 395 | 4.6 | 1.158 | 143.8 | LOS F | 24.1 | 176.3 | 1.00 | 1.11 | 16.6 |
| Approach | 2112 | 6.9 | 1.158 | 141.9 | LOS F | 55.7 | 406.4 | 0.98 | 1.21 | 15.8 |
| All Vehicles | 8519 | 7.0 | 1.257 | 91.2 | LOS F | 60.0 | 460.7 | 0.93 | 1.04 | 21.3 |

## PHASING SUMMARY

## Site: I-04 2030 MIMT \& SIMTA OPT 3 AM

Hume Highway / Hoxton Park Road / Macquarie Street 2030 MIMT \& SIMTA Option 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)
Phase times specified by the user
Sequence: TCS 405 AM - Modified
Movement Class: All Movement Classes
Input Sequence: A, C, E, D, F
Output Sequence: A, C, E, D, F
Phase Timing Results

| Phase | A | C | E | D | F |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No | No |
| Phase Change Time (sec) | 0 | 49 | 77 | 100 | 126 |
| Green Time (sec) | 43 | 22 | 17 | 20 | 18 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 49 | 28 | 23 | 26 | 24 |
| Phase Split | $33 \%$ | $19 \%$ | $15 \%$ | $17 \%$ | $16 \%$ |

## MOVEMENT SUMMARY

## Site: I-04 2030 MIMT \& SIMTA OPT 3 PM

Hume Highway / Hoxton Park Road / Macquarie Street
2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 203 | 6.4 | 0.173 | 9.6 | LOS A | 2.1 | 15.6 | 0.16 | 0.59 | 50.2 |
| 2 T1 | 1657 | 6.7 | 0.664 | 24.5 | LOS B | 26.6 | 199.7 | 0.65 | 0.59 | 41.3 |
| 3 R2 | 448 | 1.2 | 0.934 | 93.1 | LOS F | 18.7 | 132.4 | 1.00 | 0.96 | 18.4 |
| Approach | 2309 | 5.6 | 0.934 | 36.5 | LOS C | 26.6 | 199.7 | 0.68 | 0.66 | 35.0 |
| East: Macquarie Street (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 785 | 1.5 | 1.024 | 141.2 | LOS F | 35.3 | 250.1 | 0.98 | 1.03 | 13.6 |
| 5 T1 | 706 | 3.3 | 1.087 | 125.9 | LOS F | 35.4 | 254.8 | 1.00 | 1.19 | 16.5 |
| Approach | 1492 | 2.3 | 1.087 | 133.9 | LOS F | 35.4 | 254.8 | 0.99 | 1.10 | 14.9 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 101 | 5.2 | 0.965 | 33.4 | LOS C | 74.2 | 538.7 | 0.94 | 0.98 | 36.4 |
| 8 T1 | 2837 | 3.5 | 0.965 | 28.2 | LOS B | 75.5 | 548.5 | 0.83 | 0.86 | 39.3 |
| 9 R2 | 283 | 6.3 | 1.406 | 276.3 | LOS F | 39.8 | 293.6 | 1.00 | 1.37 | 10.6 |
| Approach | 3222 | 3.8 | 1.406 | 50.1 | LOS D | 75.5 | 548.5 | 0.85 | 0.91 | 31.1 |
| West: Hoxton Park Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 252 | 4.2 | 0.395 | 44.4 | LOS D | 13.7 | 99.2 | 0.80 | 0.80 | 33.6 |
| 11 T1 | 717 | 4.3 | 0.439 | 46.6 | LOS D | 14.2 | 102.8 | 0.87 | 0.73 | 30.4 |
| 12 R2 | 387 | 3.4 | 1.256 | 176.1 | LOS F | 26.0 | 189.3 | 1.00 | 1.18 | 14.3 |
| Approach | 1355 | 4.0 | 1.256 | 83.2 | LOS F | 26.0 | 189.3 | 0.89 | 0.87 | 23.0 |
| All Vehicles | 8378 | 4.1 | 1.406 | 66.6 | LOS E | 75.5 | 548.5 | 0.83 | 0.87 | 26.1 |

## PHASING SUMMARY

## Site: I-04 2030 MIMT \& SIMTA OPT 3 PM

Hume Highway / Hoxton Park Road / Macquarie Street 2030 MIMT \& SIMTA Option 3 PM PEAK 4:30 pm - 5:30 pm Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

## Phase Timing Results

| Phase | A | E | D | F |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 78 | 98 | 127 |
| Green Time (sec) | 72 | 14 | 23 | 17 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 78 | 20 | 29 | 23 |
| Phase Split | $52 \%$ | $13 \%$ | $19 \%$ | $15 \%$ |

Phase $A$

## I-05 Intersection of the Hume Highway and Reilly Street

## MOVEMENT SUMMARY

Site: I-05 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Hignway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 80 | 2.6 | 0.944 | 32.6 | LOS C | 72.7 | 531.8 | 0.86 | 0.88 | 35.9 |
| 2 T1 | 3175 | 4.6 | 0.944 | 26.3 | LOS B | 72.7 | 531.8 | 0.79 | 0.82 | 35.6 |
| 3 R2 | 14 | 7.7 | 0.117 | 24.4 | LOS B | 0.5 | 3.8 | 0.51 | 0.68 | 36.1 |
| Approach | 3269 | 4.5 | 0.944 | 26.5 | LOS B | 72.7 | 531.8 | 0.79 | 0.82 | 35.6 |
| East: Congressional Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 49 | 2.1 | 0.263 | 59.1 | LOS E | 5.9 | 42.6 | 0.89 | 0.74 | 24.5 |
| 5 T1 | 46 | 4.5 | 0.263 | 54.5 | LOS D | 5.9 | 42.6 | 0.89 | 0.74 | 24.0 |
| 6 R2 | 91 | 4.7 | 0.428 | 67.2 | LOS E | 6.1 | 44.6 | 0.95 | 0.79 | 18.7 |
| Approach | 186 | 4.0 | 0.428 | 61.9 | LOS E | 6.1 | 44.6 | 0.92 | 0.76 | 21.6 |
| North: Hume Hignway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 32 | 3.3 | 0.579 | 18.3 | LOS B | 23.4 | 177.9 | 0.54 | 0.58 | 39.1 |
| 8 T1 | 1936 | 8.8 | 0.579 | 11.4 | LOS A | 26.6 | 202.5 | 0.51 | 0.50 | 46.3 |
| 9 R2 | 99 | 1.1 | 0.772 | 60.4 | LOS E | 6.1 | 42.9 | 1.00 | 0.93 | 22.5 |
| Approach | 2067 | 8.3 | 0.772 | 13.8 | LOS A | 26.6 | 202.5 | 0.54 | 0.52 | 43.9 |
| West: Reilly Street (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 120 | 3.5 | 0.274 | 50.3 | LOS D | 7.6 | 55.2 | 0.83 | 0.76 | 24.5 |
| 11 T1 | 14 | 7.7 | 0.274 | 45.7 | LOS D | 7.6 | 55.2 | 0.83 | 0.76 | 25.6 |
| 12 R2 | 239 | 1.3 | 1.049 | 131.2 | LOS F | 24.1 | 171.0 | 1.00 | 1.11 | 15.9 |
| Approach | 373 | 2.3 | 1.049 | 102.1 | LOS F | 24.1 | 171.0 | 0.94 | 0.98 | 17.9 |
| All Vehicles | 5895 | 5.7 | 1.049 | 27.9 | LOS B | 72.7 | 531.8 | 0.72 | 0.72 | 34.6 |

## PHASING SUMMARY

Site: I-05 2030 MIMT \& SIMTA OPT 3 AM
Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 150 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E2 |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 100 | 138 |
| Green Time (sec) | 94 | 32 | 6 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 100 | 38 | 12 |
| Phase Split | $67 \%$ | $25 \%$ | $8 \%$ |



## MOVEMENT SUMMARY

## Site: I-05 2030 MIMT \& SIMTA OPT 3 PM

Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Demand | Flows | Deg. Satn | Average | Level of | 95\% Bac | of Queue | Prop. | Effective | Average |
| v | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Hume Hignway (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 228 | 0.5 | 0.689 | 20.0 | LOS B | 27.9 | 204.1 | 0.55 | 0.58 | 41.6 |
| 2 T1 | 2123 | 5.9 | 0.689 | 12.0 | LOS A | 27.9 | 204.1 | 0.48 | 0.46 | 45.4 |
| 3 R2 | 21 | 5.0 | 0.391 | 30.3 | LOS C | 1.0 | 7.5 | 0.62 | 0.73 | 33.4 |
| Approach | 2372 | 5.3 | 0.689 | 12.9 | LOS A | 27.9 | 204.1 | 0.49 | 0.48 | 44.8 |
| East: Congressional Drive (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 42 | 2.5 | 0.205 | 61.9 | LOS E | 4.2 | 29.6 | 0.90 | 0.73 | 23.8 |
| 5 T1 | 24 | 0.0 | 0.205 | 57.3 | LOS E | 4.2 | 29.6 | 0.90 | 0.73 | 23.3 |
| 6 R2 | 52 | 0.0 | 0.236 | 65.6 | LOS E | 3.4 | 23.6 | 0.92 | 0.75 | 19.1 |
| Approach | 118 | 0.9 | 0.236 | 62.6 | LOS E | 4.2 | 29.6 | 0.91 | 0.74 | 21.7 |
| North: Hume Hignway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 67 | 0.0 | 0.986 | 31.4 | LOS C | 87.9 | 634.4 | 0.77 | 0.85 | 31.0 |
| 8 T1 | 3695 | 3.0 | 0.986 | 26.7 | LOS B | 87.9 | 634.4 | 0.59 | 0.67 | 35.4 |
| $9 \quad \mathrm{R} 2$ | 178 | 1.2 | 0.819 | 61.6 | LOS E | 11.8 | 83.2 | 1.00 | 1.02 | 22.3 |
| Approach | 3940 | 2.9 | 0.986 | 28.4 | LOS B | 87.9 | 634.4 | 0.61 | 0.69 | 34.4 |
| West: Reilly Street (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 65 | 0.0 | 0.235 | 56.1 | LOS D | 5.8 | 40.6 | 0.86 | 0.74 | 23.5 |
| 11 T1 | 32 | 0.0 | 0.235 | 51.6 | LOS D | 5.8 | 40.6 | 0.86 | 0.74 | 24.5 |
| 12 R2 | 261 | 1.6 | 1.120 | 156.3 | LOS F | 28.6 | 203.3 | 1.00 | 1.17 | 14.1 |
| Approach | 358 | 1.2 | 1.120 | 128.8 | LOS F | 28.6 | 203.3 | 0.96 | 1.06 | 15.5 |
| All Vehicles | 6788 | 3.6 | 1.120 | 28.9 | LOS C | 87.9 | 634.4 | 0.59 | 0.64 | 34.2 |

## PHASING SUMMARY

Site: I-05 2030 MIMT \& SIMTA OPT 3 PM
Hume Highway / Reilly Street
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=150$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E2 |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 98 | 133 |
| Green Time (sec) | 92 | 29 | 11 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 98 | 35 | 17 |
| Phase Split | $65 \%$ | $23 \%$ | $11 \%$ |

Phase A

## I-06 Intersection of Newbridge Road and Moorebank Avenue

## MOVEMENT SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 3 AM

Network: 2030 MIMT \& SIMTA OPT 3 AM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV veh/h |  | Arrival Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1535 | 3.2 |  |  |  | 1232 | 3.2 | 0.636 | 19.0 | LOS B | 13.6 | 98.2 | 0.57 | 0.82 | 42.3 |
| 3 R2 | 1403 | 11.5 | 1128 | 11.7 | 0.683 | 15.2 | LOS B | 14.4 | 113.0 | 0.43 | 0.69 | 52.4 |
| Approach | 2938 | 7.1 | 2360 N1 | 7.3 | 0.683 | 17.2 | LOS B | 14.4 | 113.0 | 0.50 | 0.76 | 47.8 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 737 | 20.7 | 737 | 20.7 | 0.521 | 18.6 | LOS B | 8.4 | 70.4 | 0.72 | 0.80 | 51.8 |
| 5 T1 | 965 | 5.1 | 965 | 5.1 | 1.260 | 311.5 | LOS F | 77.3 | 564.9 | 1.00 | 1.91 | 14.7 |
| Approach | 1702 | 11.9 | 1702 | 11.9 | 1.260 | 184.7 | LOS F | 77.3 | 564.9 | 0.88 | 1.43 | 19.1 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1582 | 6.6 | 1582 | 6.6 | 0.853 | 12.5 | LOS A | 31.0 | 229.6 | 0.64 | 0.60 | 60.8 |
| 12 R2 | 907 | 7.3 | 907 | 7.3 | 1.696 | 683.2 | LOS F | 114.9 | 854.8 | 1.00 | 2.01 | 3.0 |
| Approach | 2489 | 6.8 | 2489 | 6.8 | 1.696 | 256.9 | LOS F | 114.9 | 854.8 | 0.77 | 1.11 | 13.9 |
| All Vehicles | 7129 | 8.2 | 6551 N1 | 8.9 | 1.696 | 151.8 | LOS F | 114.9 | 854.8 | 0.70 | 1.07 | 19.4 |

## PHASING SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 3 AM

Network: 2030 MIMT \& SIMTA OPT 3 AM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=133$ seconds (User-Given Phase Times)
Phase Timing Results


## MOVEMENT SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 3 PM
$\phi$
Network: 2030 MIMT \& SIMTA OPT 3 PM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV veh/h \% |  | Arrival Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1034 | 2.9 |  |  |  | 912 | 3.0 | 0.519 | 22.6 | LOS B | 13.7 | 98.2 | 0.58 | 0.75 | 39.8 |
| 3 R2 | 989 | 11.0 | 876 | 11.4 | 1.147 | 190.3 | LOS F | 16.8 | 130.6 | 1.00 | 1.43 | 15.8 |
| Approach | 2023 | 6.8 | 1788 N1 | 7.1 | 1.147 | 104.8 | LOS F | 16.8 | 130.6 | 0.78 | 1.08 | 20.7 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1271 | 7.1 | 1271 | 7.1 | 1.106 | 189.6 | LOS F | 78.5 | 590.7 | 1.00 | 1.30 | 15.1 |
| 5 T1 | 1373 | 4.8 | 1373 | 4.8 | 0.923 | 51.1 | LOS D | 42.7 | 311.4 | 1.00 | 1.04 | 43.3 |
| Approach | 2643 | 5.9 | 2643 | 5.9 | 1.106 | 117.7 | LOS F | 78.5 | 590.7 | 1.00 | 1.17 | 25.6 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1129 | 4.0 | 1129 | 4.0 | 0.442 | 9.3 | LOS A | 14.6 | 105.8 | 0.50 | 0.45 | 62.9 |
| 12 R2 | 1120 | 2.8 | 1120 | 2.8 | 1.200 | 233.1 | LOS F | 74.8 | 536.3 | 1.00 | 1.47 | 8.2 |
| Approach | 2249 | 3.4 | 2249 | 3.4 | 1.200 | 120.8 | LOS F | 74.8 | 536.3 | 0.75 | 0.96 | 22.4 |
| All Vehicles | 6916 | 5.4 | $6681{ }^{\text {N1 }}$ | 5.6 | 1.200 | 115.3 | LOS F | 78.5 | 590.7 | 0.86 | 1.07 | 23.4 |

## PHASING SUMMARY

Site: I-06 2030 MIMT \& SIMTA Opt 3 PM

Network: 2030 MIMT \& SIMTA OPT 3 PM

Newbridge Road / Moorebank Avenue
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=116$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | C | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 44 | 76 |
| Green Time (sec) | 38 | 26 | 34 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 44 | 32 | 40 |
| Phase Split | $38 \%$ | $28 \%$ | $34 \%$ |



I-07 Intersection of Moorebank Avenue and Heathcote Road

## MOVEMENT SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 3 AM

Network: 2030 MIMT \& SIMTA OPT 3 AM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Demand | Flows | Arrival | fows | Deg. Satn | Average | Level of | 95\% Back | of Queue | Prop. | Effective | Average |
| v | Total | HV | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1952 | 7.2 | 1766 | 7.3 | 1.165 | 196.3 | LOS F | 58.4 | 440.6 | 1.00 | 1.85 | 4.9 |
| 3 R2 | 23 | 18.2 | 21 | 18.4 | 0.189 | 71.8 | LOS F | 1.3 | 10.9 | 0.98 | 0.71 | 30.6 |
| Approach | 1975 | 7.3 | 1787 N1 | 7.4 | 1.165 | 194.8 | LOS F | 58.4 | 440.6 | 1.00 | 1.84 | 5.1 |
| East: Heathcote Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 29 | 57.1 | 29 | 57.1 | 1.442 | 482.1 | LOS F | 102.2 | 769.9 | 1.00 | 1.95 | 6.8 |
| 6 R2 | 952 | 5.9 | 952 | 5.9 | 1.442 | 481.9 | LOS F | 102.2 | 769.9 | 1.00 | 1.95 | 6.8 |
| Approach | 981 | 7.4 | 981 | 7.4 | 1.442 | 482.0 | LOS F | 102.2 | 769.9 | 1.00 | 1.95 | 6.8 |
| North: Moorebank Avenue ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 888 | 17.7 | 698 | 19.8 | 0.483 | 11.0 | LOS A | 14.9 | 124.4 | 0.56 | 0.72 | 50.8 |
| 8 T1 | 784 | 8.1 | 607 | 9.1 | 0.327 | 20.7 | LOS B | 11.5 | 86.7 | 0.64 | 0.55 | 13.4 |
| Approach | 1673 | 13.2 | $1305{ }^{\text {N1 }}$ | 14.8 | 0.483 | 15.5 | LOS B | 14.9 | 124.4 | 0.59 | 0.64 | 42.3 |
| All Vehicles | 4628 | 9.4 | 4073 N1 | 10.7 | 1.442 | 206.5 | LOS F | 102.2 | 769.9 | 0.87 | 1.48 | 8.7 |

## PHASING SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 3 AM

Network: 2030 MIMT \& SIMTA OPT 3 AM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=133$ seconds (User-Given Phase Times)

| Phase Timing Results | B | A | D |
| :--- | :---: | :---: | :---: |
| Phase | Yes | No | No |
| Reference Phase | 0 | 15 | 88 |
| Phase Change Time (sec) | 9 | 67 | 39 |
| Green Time (sec) | 4 | 4 | 4 |
| Yellow Time (sec) | 2 | 2 | 2 |
| All-Red Time (sec) | 15 | 73 | 45 |
| Phase Time (sec) | $11 \%$ | $55 \%$ | $34 \%$ |
| Phase Split |  |  |  |

Phase B

## MOVEMENT SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 3 PM
\$
Network: 2030 MIMT \& SIMTA OPT 3 PM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Demand | Flows | Arrival | Flows | Deg. Satn | Average | Level of | 95\% Back | of Queue | Prop. | Effective | Average |
| v | Total | HV | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1241 | 8.7 | 1241 | 8.7 | 0.987 | 82.2 | LOS F | 58.0 | 440.6 | 1.00 | 1.35 | 10.5 |
| $3 \quad \mathrm{R} 2$ | 48 | 8.7 | 48 | 8.7 | 0.401 | 64.7 | LOS E | 2.8 | 20.9 | 1.00 | 0.74 | 32.2 |
| Approach | 1289 | 8.7 | 1289 | 8.7 | 0.987 | 81.6 | LOS F | 58.0 | 440.6 | 1.00 | 1.33 | 11.6 |
| East: Heathcote Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 76 | 19.4 | 76 | 19.4 | 1.458 | 468.8 | LOS F | 96.2 | 715.9 | 1.00 | 2.06 | 6.9 |
| 6 R2 | 812 | 5.2 | 812 | 5.2 | 1.458 | 468.0 | LOS F | 96.2 | 715.9 | 1.00 | 2.07 | 7.0 |
| Approach | 887 | 6.4 | 887 | 6.4 | 1.458 | 468.0 | LOS F | 96.2 | 715.9 | 1.00 | 2.07 | 7.0 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 884 | 3.7 | 770 | 3.7 | 0.366 | 7.5 | LOS A | 5.1 | 37.2 | 0.24 | 0.61 | 53.8 |
| 8 T1 | 1481 | 5.9 | 1290 | 6.0 | 0.669 | 6.3 | LOS A | 11.8 | 87.7 | 0.35 | 0.32 | 29.3 |
| Approach | 2365 | 5.1 | 2060 N1 | 5.2 | 0.669 | 6.7 | LOS A | 11.8 | 87.7 | 0.31 | 0.43 | 48.5 |
| All Vehicles | 4542 | 6.4 | 4237 N1 | 6.8 | 1.458 | 126.1 | LOS F | 96.2 | 715.9 | 0.66 | 1.04 | 12.4 |

## PHASING SUMMARY

Site: I-07 2030 MIMT \& SIMTA Opt 3 PM
${ }_{\phi}^{\boldsymbol{\phi}}$ Network: 2030 MIMT \& SIMTA OPT 3 PM

Moorebank Avenue / Heathcote Road
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=116$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | B | A | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 14 | 80 |
| Green Time (sec) | 8 | 60 | 30 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 14 | 66 | 36 |
| Phase Split | $12 \%$ | $57 \%$ | $31 \%$ |

Phase B

I-08 Intersection of Moorebank Avenue and Industry Park Access

## MOVEMENT SUMMARY

Site: I-08 2030 MIMT \& SIMTA Opt 3 AM

Network: 2030 MIMT \& SIMTA OPT 3 AM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV veh/h \% |  | Arrival Flows Deg. SatnTotal HV |  |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  | Vehicles | Distance |  |  |  |  |  |
|  |  |  | veh/h | \% |  | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 91 | 3.5 |  |  |  |  | 91 | 3.5 |  | 0.056 | 6.1 | LOS A | 0.4 | 3.0 | 0.12 | 0.58 | 43.1 |
| 2 T1 | 1933 | 6.6 | 1933 | 6.6 |  | 1.261 | 297.7 | LOS F | 170.6 | 1281.3 | 1.00 | 2.24 | 5.5 |
| Approach | 2023 | 6.5 | 2023 | 6.5 |  | 1.261 | 284.6 | LOS F | 170.6 | 1281.3 | 0.96 | 2.16 | 5.8 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 789 | 17.3 | 627 | 20.2 |  | 0.223 | 2.6 | LOS A | 4.2 | 35.1 | 0.23 | 0.20 | 56.8 |
| 9 R2 | 65 | 38.7 | 54 | 43.1 |  | 1.027 | 125.9 | LOS F | 4.9 | 47.1 | 1.00 | 1.07 | 11.1 |
| Approach | 855 | 19.0 | 681 N1 | 22.0 |  | 1.027 | 12.3 | LOS A | 4.9 | 47.1 | 0.29 | 0.27 | 46.3 |
| West: Industry Park Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 34 | 62.5 | 34 | 62.5 |  | 0.415 | 64.9 | LOS E | 2.3 | 24.3 | 0.95 | 0.73 | 9.6 |
| 12 R2 | 58 | 72.7 | 58 | 72.7 |  | 0.413 | 68.0 | LOS E | 2.7 | 31.4 | 0.98 | 0.73 | 19.8 |
| Approach | 92 | 69.0 | 92 | 69.0 |  | 0.415 | 66.9 | LOS E | 2.7 | 31.4 | 0.97 | 0.73 | 16.8 |
| All Vehicles | 2969 | 12.0 | 2795 N1 | 12.7 |  | 1.261 | 211.2 | LOS F | 170.6 | 1281.3 | 0.80 | 1.66 | 8.3 |

## PHASING SUMMARY

Site: I-08 2030 MIMT \& SIMTA Opt 3 AM

Network: 2030 MIMT \& SIMTA OPT 3 AM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 133 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | C |
| :--- | :---: | :---: |
| Reference Phase | Yes | No |
| Phase Change Time (sec) | 0 | 116 |
| Green Time (sec) | 110 | 11 |
| Yellow Time (sec) | 4 | 4 |
| All-Red Time (sec) | 2 | 2 |
| Phase Time (sec) | 116 | 17 |
| Phase Split | $87 \%$ | $13 \%$ |



MOVEMENT SUMMARY
Site: I-08 2030 MIMT \& SIMTA Opt 3 PM

Network: 2030 MIMT \& SIMTA OPT 3 PM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 116 seconds (Network Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Total HV veh/h \% |  | Arrival Flows Deg. Satn |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  | Total | HV |  |  |  | Vehicles | Distance |  |  |  |
|  |  |  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 30.0 | 11 | 30.0 | 0.009 | 6.6 | LOS A | 0.1 | 0.5 | 0.14 | 0.56 | 42.9 |
| 2 T1 | 1211 | 8.1 | 1211 | 8.1 | 0.514 | 4.8 | LOS A | 13.3 | 100.4 | 0.39 | 0.36 | 51.7 |
| Approach | 1221 | 8.3 | 1221 | 8.3 | 0.514 | 4.8 | LOS A | 13.3 | 100.4 | 0.39 | 0.36 | 51.6 |
| North: Moorebank Avenue ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1555 | 5.6 | 1345 | 5.5 | 0.459 | 4.4 | LOS A | 12.5 | 93.0 | 0.36 | 0.33 | 54.7 |
| 9 R2 | 25 | 62.5 | 22 | 62.2 | 0.168 | 15.7 | LOS B | 0.5 | 5.6 | 0.42 | 0.66 | 32.1 |
| Approach | 1580 | 6.5 | 1367 N1 | 6.4 | 0.459 | 4.6 | LOS A | 12.5 | 93.0 | 0.37 | 0.34 | 54.3 |
| West: Industry Park Access (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 34 | 15.6 | 34 | 15.6 | 0.103 | 4.3 | LOS A | 0.4 | 3.4 | 0.28 | 0.39 | 26.2 |
| 12 R2 | 189 | 10.0 | 189 | 10.0 | 0.490 | 56.1 | LOS D | 5.2 | 40.1 | 0.98 | 0.78 | 22.4 |
| Approach | 223 | 10.8 | 223 | 10.8 | 0.490 | 48.3 | LOS D | 5.2 | 40.1 | 0.88 | 0.72 | 22.6 |
| All Vehicles | 3024 | 7.5 | 2811 N1 | 8.1 | 0.514 | 8.2 | LOS A | 13.3 | 100.4 | 0.42 | 0.38 | 48.0 |

## PHASING SUMMARY

Site: I-08 2030 MIMT \& SIMTA Opt 3 PM

Network: 2030 MIMT \& SIMTA OPT 3 PM

Moorebank Avenue / Industry Park Access
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=116$ seconds (Network Cycle Time)
Phase Timing Results

| Phase | A | C |
| :--- | :---: | :---: |
| Reference Phase | Yes | No |
| Phase Change Time (sec) | 0 | 97 |
| Green Time (sec) | 91 | 13 |
| Yellow Time (sec) | 4 | 4 |
| All-Red Time (sec) | 2 | 2 |
| Phase Time (sec) | 97 | 19 |
| Phase Split | $84 \%$ | $16 \%$ |

Phase A

## I-09 Intersection of Moorebank Avenue and Church Road

## MOVEMENT SUMMARY

## $\nabla$ Site: I-09 2030 MIMT \& SIMTA OPT 3 AM

Moorebank Avenue / Church Road
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 2134 | 7.8 | 0.813 | 9.0 | LOS A | 11.7 | 88.8 | 0.12 | 0.10 | 51.7 |
| 3 R2 | 284 | 8.6 | 0.813 | 32.9 | LOS C | 11.7 | 88.8 | 1.00 | 0.79 | 37.1 |
| Approach | 2418 | 7.9 | 1.016 | 11.8 | NA | 11.7 | 88.8 | 0.23 | 0.18 | 49.4 |
| East: Church Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 204 | 15.8 | 0.276 | 8.0 | LOS A | 1.1 | 9.2 | 0.53 | 0.77 | 47.0 |
| 6 R2 | 7 | 0.0 | 0.945 | 589.5 | LOS F | 2.0 | 13.8 | 1.00 | 1.05 | 5.5 |
| Approach | 211 | 15.3 | 0.945 | 28.2 | LOS B | 2.0 | 13.8 | 0.55 | 0.78 | 37.2 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 37 | 0.0 | 0.253 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.05 | 57.7 |
| 8 T1 | 819 | 22.4 | 0.253 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 59.6 |
| Approach | 856 | 21.4 | 0.253 | 0.3 | NA | 0.0 | 0.0 | 0.00 | 0.03 | 59.6 |
| All Vehicles | 3485 | 11.7 | 1.016 | 10.0 | NA | 11.7 | 88.8 | 0.19 | 0.18 | 50.4 |

## MOVEMENT SUMMARY

Site: I-09 2030 MIMT \& SIMTA OPT 3 PM
Moorebank Avenue / Church Road
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1185 | 11.6 | 0.598 | 3.8 | LOS A | 6.1 | 48.1 | 0.09 | 0.06 | 56.2 |
| 3 R2 | 105 | 13.4 | 0.598 | 45.9 | LOS D | 6.1 | 48.1 | 1.00 | 0.62 | 32.7 |
| Approach | 1290 | 11.7 | 0.598 | 7.2 | NA | 6.1 | 48.1 | 0.16 | 0.10 | 53.0 |
| East: Church Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 405 | 5.0 | 1.222 | 164.1 | LOS F | 41.0 | 301.2 | 1.00 | 3.03 | 15.6 |
| 6 R2 | 1 | 0.0 | 0.117 | 372.6 | LOS F | 0.3 | 2.0 | 0.99 | 1.00 | 8.2 |
| Approach | 406 | 5.0 | 1.222 | 164.6 | LOS F | 41.0 | 301.2 | 1.00 | 3.02 | 15.5 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 13 | 7.7 | 0.884 | 6.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 55.9 |
| 8 T1 | 1632 | 6.2 | 0.884 | 1.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 57.6 |
| Approach | 1645 | 6.3 | 0.884 | 1.3 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 57.6 |
| All Vehicles | 3341 | 8.2 | 1.222 | 23.4 | NA | 41.0 | 301.2 | 0.19 | 0.41 | 42.0 |

## I-10 Intersection of Heathcote Road and Nuwarra Road

## MOVEMENT SUMMARY

Site: I-10 2030 MIMT \& SIMTA OPT 3 AM
Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA OPT 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=131$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| SouthEast: Heathcote Road (SE) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 291 | 1.1 | 0.204 | 8.8 | LOS A | 4.3 | 30.7 | 0.30 | 0.64 | 47.7 |
| 5 T1 | 2073 | 5.2 | 1.265 | 174.0 | LOS F | 119.2 | 871.7 | 1.00 | 1.60 | 15.3 |
| 6 R2 | 647 | 3.3 | 1.268 | 159.7 | LOS F | 28.4 | 204.2 | 1.00 | 1.23 | 16.7 |
| Approach | 3011 | 4.4 | 1.268 | 155.0 | LOS F | 119.2 | 871.7 | 0.93 | 1.43 | 16.4 |
| NorthEast: Nuwarra Road (NE) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 416 | 4.8 | 0.484 | 24.5 | LOS B | 16.5 | 120.1 | 0.71 | 0.78 | 42.4 |
| 8 T1 | 301 | 7.0 | 0.481 | 53.9 | LOS D | 8.8 | 65.6 | 0.95 | 0.78 | 26.0 |
| 9 R2 | 508 | 5.8 | 1.436 | 280.3 | LOS F | 34.0 | 249.7 | 1.00 | 1.43 | 10.4 |
| Approach | 1226 | 5.8 | 1.436 | 137.9 | LOS F | 34.0 | 249.7 | 0.89 | 1.05 | 17.2 |
| NorthWest: Heathcote Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 254 | 11.6 | 0.334 | 21.5 | LOS B | 7.8 | 60.1 | 0.70 | 0.76 | 42.7 |
| 11 T1 | 1044 | 11.2 | 0.957 | 51.9 | LOS D | 40.8 | 313.1 | 0.90 | 0.94 | 32.1 |
| 12 R2 | 235 | 6.3 | 0.786 | 75.4 | LOS F | 8.0 | 59.1 | 1.00 | 0.88 | 19.9 |
| Approach | 1532 | 10.5 | 0.957 | 50.4 | LOS D | 40.8 | 313.1 | 0.88 | 0.90 | 31.4 |
| SouthWest: Wattle Grove Drive (SW) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 639 | 2.1 | 0.849 | 51.7 | LOS D | 31.8 | 226.4 | 0.99 | 1.15 | 24.8 |
| 2 T1 | 543 | 4.5 | 0.817 | 61.7 | LOS E | 19.6 | 142.5 | 1.00 | 0.94 | 23.8 |
| 3 R2 | 263 | 4.0 | 1.277 | 207.3 | LOS F | 30.6 | 221.5 | 1.00 | 1.37 | 9.9 |
| Approach | 1445 | 3.4 | 1.277 | 83.8 | LOS F | 31.8 | 226.4 | 0.99 | 1.11 | 19.1 |
| All Vehicles | 7214 | 5.7 | 1.436 | 115.6 | LOS F | 119.2 | 871.7 | 0.93 | 1.19 | 18.9 |

## PHASING SUMMARY

Site: I-10 2030 MIMT \& SIMTA OPT 3 AM
Heathcote Road / Nuwarra Road / Wattle Grove Drive 2030 MIMT \& SIMTA OPT 3 AM PEAK 7:45 am - 8:45 am Signals - Fixed Time Cycle Time = 131 seconds (User-Given Phase Times)


## MOVEMENT SUMMARY

## Site: I-10 2030 MIMT \& SIMTA OPT 3 PM

Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA OPT 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=139$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective <br> Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| SouthEast: Heathcote Road (SE) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 337 | 2.5 | 0.282 | 15.4 | LOS B | 8.9 | 63.6 | 0.45 | 0.70 | 42.4 |
| 5 T1 | 1331 | 5.4 | 0.992 | 66.0 | LOS E | 54.6 | 400.4 | 0.93 | 1.05 | 28.4 |
| 6 R2 | 469 | 3.1 | 1.197 | 179.1 | LOS F | 26.2 | 188.2 | 1.00 | 1.22 | 15.3 |
| Approach | 2137 | 4.5 | 1.197 | 82.9 | LOS F | 54.6 | 400.4 | 0.87 | 1.03 | 24.4 |
| NorthEast: Nuwarra Road (NE) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 646 | 2.8 | 0.950 | 74.6 | LOS F | 44.7 | 320.2 | 1.00 | 1.19 | 27.0 |
| 8 T1 | 621 | 1.4 | 0.996 | 88.2 | LOS F | 27.4 | 193.9 | 1.00 | 1.09 | 19.1 |
| 9 R2 | 556 | 7.0 | 1.120 | 135.5 | LOS F | 29.2 | 216.3 | 1.00 | 1.13 | 18.1 |
| Approach | 1823 | 3.6 | 1.120 | 97.8 | LOS F | 44.7 | 320.2 | 1.00 | 1.14 | 21.2 |
| NorthWest: Heathcote Road (NW) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 258 | 6.1 | 0.232 | 21.3 | LOS B | 8.5 | 62.5 | 0.53 | 0.73 | 43.0 |
| 11 T1 | 1701 | 2.7 | 1.170 | 143.6 | LOS F | 91.8 | 658.0 | 1.00 | 1.40 | 17.6 |
| 12 R 2 | 467 | 2.0 | 1.098 | 128.9 | LOS F | 23.4 | 166.5 | 1.00 | 1.09 | 13.6 |
| Approach | 2427 | 3.0 | 1.170 | 127.8 | LOS F | 91.8 | 658.0 | 0.95 | 1.27 | 18.1 |
| SouthWest: Wattle Grove Drive (SW) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 305 | 1.7 | 0.387 | 33.9 | LOS C | 14.1 | 100.1 | 0.76 | 0.85 | 30.6 |
| 2 T1 | 376 | 1.1 | 0.534 | 58.3 | LOS E | 11.8 | 83.3 | 0.97 | 0.80 | 24.5 |
| 3 R2 | 395 | 1.1 | 1.468 | 300.7 | LOS F | 55.6 | 392.6 | 1.00 | 1.51 | 7.2 |
| Approach | 1077 | 1.3 | 1.468 | 140.4 | LOS F | 55.6 | 392.6 | 0.92 | 1.08 | 13.3 |
| All Vehicles | 7464 | 3.3 | 1.468 | 109.4 | LOS F | 91.8 | 658.0 | 0.93 | 1.14 | 19.6 |

## PHASING SUMMARY

Site: I-10 2030 MIMT \& SIMTA OPT 3 PM
Heathcote Road / Nuwarra Road / Wattle Grove Drive
2030 MIMT \& SIMTA OPT 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 139 seconds (User-Given Phase Times)
Phase Timing Results


## I-11 Intersection of Newbridge Road and Nuwarra Road

## MOVEMENT SUMMARY

Site: I-11 2030 MIMT \& SIMTA OPT 3 AM
Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Nuwarra Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 37 | 8.6 | 0.751 | 49.6 | LOS D | 21.6 | 154.2 | 0.90 | 0.83 | 37.4 |
| 2 T1 | 334 | 1.5 | 0.751 | 46.6 | LOS D | 21.6 | 154.2 | 0.90 | 0.83 | 31.1 |
| 3 R2 | 809 | 6.2 | 1.171 | 168.1 | LOS F | 48.7 | 358.7 | 1.00 | 1.21 | 17.5 |
| Approach | 1180 | 4.9 | 1.171 | 130.0 | LOS F | 48.7 | 358.7 | 0.97 | 1.09 | 20.4 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 353 | 15.9 | 0.652 | 28.4 | LOS B | 23.1 | 181.8 | 0.74 | 0.79 | 44.8 |
| 5 T1 | 1311 | 11.8 | 0.652 | 23.9 | LOS B | 23.5 | 182.6 | 0.69 | 0.64 | 50.9 |
| Approach | 1664 | 12.7 | 0.652 | 24.8 | LOS B | 23.5 | 182.6 | 0.70 | 0.67 | 49.6 |
| North: Nuwarra Road (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 8 | 0.0 | 0.998 | 104.8 | LOS F | 11.2 | 78.6 | 1.00 | 1.13 | 22.9 |
| 8 T1 | 156 | 0.6 | 1.247 | 125.2 | LOS F | 21.0 | 152.5 | 1.00 | 1.18 | 19.8 |
| 9 R2 | 143 | 5.1 | 1.247 | 199.9 | LOS F | 21.0 | 152.5 | 1.00 | 1.38 | 15.9 |
| Approach | 307 | 2.7 | 1.247 | 159.5 | LOS F | 21.0 | 152.5 | 1.00 | 1.27 | 17.7 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 305 | 2.1 | 1.161 | 140.1 | LOS F | 93.7 | 700.2 | 1.00 | 1.33 | 20.6 |
| 11 T1 | 2308 | 9.9 | 1.236 | 148.6 | LOS F | 107.8 | 827.5 | 1.00 | 1.46 | 21.3 |
| Approach | 2614 | 9.0 | 1.236 | 147.6 | LOS F | 107.8 | 827.5 | 1.00 | 1.44 | 21.2 |
| All Vehicles | 5765 | 8.9 | 1.247 | 109.2 | LOS F | 107.8 | 827.5 | 0.91 | 1.14 | 24.9 |

## PHASING SUMMARY

## Site: I-11 2030 MIMT \& SIMTA OPT 3 AM

Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 140 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 72 | 89 |
| Green Time (sec) | 66 | 11 | 45 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 72 | 17 | 51 |
| Phase Split | $51 \%$ | $12 \%$ | $36 \%$ |



## MOVEMENT SUMMARY

## Site: I-11 2030 MIMT \& SIMTA OPT 3 PM

Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Nuwarra Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 58 | 7.3 | 0.778 | 71.4 | LOS F | 15.0 | 107.3 | 1.00 | 0.90 | 31.7 |
| 2 T1 | 158 | 0.6 | 0.778 | 67.0 | LOS E | 15.0 | 107.3 | 1.00 | 0.90 | 28.8 |
| 3 R2 | 561 | 6.1 | 1.003 | 104.0 | LOS F | 24.6 | 181.5 | 1.00 | 1.03 | 24.1 |
| Approach | 777 | 5.0 | 1.003 | 94.1 | LOS F | 24.6 | 181.5 | 1.00 | 0.99 | 25.4 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 728 | 3.8 | 0.779 | 18.5 | LOS B | 32.5 | 236.8 | 0.58 | 0.78 | 50.1 |
| 5 T1 | 2230 | 6.0 | 0.779 | 16.4 | LOS B | 39.7 | 294.8 | 0.65 | 0.64 | 55.5 |
| Approach | 2958 | 5.5 | 0.779 | 17.0 | LOS B | 39.7 | 294.8 | 0.64 | 0.67 | 54.2 |
| North: Nuwarra Road (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 17 | 0.0 | 0.844 | 73.2 | LOS F | 17.1 | 120.7 | 1.00 | 0.96 | 29.7 |
| 8 T1 | 281 | 1.1 | 1.055 | 81.3 | LOS F | 25.7 | 182.0 | 1.00 | 1.00 | 26.4 |
| $9 \quad \mathrm{R} 2$ | 213 | 1.5 | 1.055 | 129.0 | LOS F | 25.7 | 182.0 | 1.00 | 1.14 | 22.1 |
| Approach | 511 | 1.2 | 1.055 | 100.9 | LOS F | 25.7 | 182.0 | 1.00 | 1.06 | 24.4 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 104 | 0.0 | 0.552 | 21.6 | LOS B | 17.9 | 133.0 | 0.51 | 0.52 | 48.4 |
| 11 T1 | 1702 | 8.2 | 0.627 | 14.8 | LOS B | 20.8 | 156.9 | 0.51 | 0.48 | 56.8 |
| Approach | 1806 | 7.7 | 0.627 | 15.2 | LOS B | 20.8 | 156.9 | 0.51 | 0.48 | 56.2 |
| All Vehicles | 6052 | 5.7 | 1.055 | 33.4 | LOS C | 39.7 | 294.8 | 0.68 | 0.69 | 44.2 |

## PHASING SUMMARY

## Site: I-11 2030 MIMT \& SIMTA OPT 3 PM

Newbridge Road / Nuwarra Road
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 84 | 112 |
| Green Time (sec) | 78 | 22 | 22 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 84 | 28 | 28 |
| Phase Split | $60 \%$ | $20 \%$ | $20 \%$ |



## I-12 Intersection of Newbridge Road and Governor Macquarie Drive

## MOVEMENT SUMMARY

Site: I-12 2030 MIMT \& SIMTA OPT 3 AM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Brickmakers Drive (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 0.0 | 0.867 | 78.5 | LOS F | 15.6 | 110.4 | 1.00 | 0.98 | 25.2 |
| 2 T1 | 197 | 1.0 | 0.867 | 74.1 | LOS F | 15.6 | 110.4 | 1.00 | 0.98 | 24.9 |
| 3 R2 | 684 | 1.2 | 1.177 | 166.5 | LOS F | 36.9 | 260.6 | 1.00 | 1.25 | 19.6 |
| Approach | 895 | 1.1 | 1.177 | 144.8 | LOS F | 36.9 | 260.6 | 1.00 | 1.19 | 20.4 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 230 | 3.0 | 0.169 | 7.7 | LOS A | 1.9 | 13.9 | 0.18 | 0.63 | 58.2 |
| 5 T1 | 1514 | 11.2 | 0.444 | 14.1 | LOS A | 17.4 | 134.2 | 0.56 | 0.50 | 59.8 |
| 6 R2 | 649 | 9.9 | 0.964 | 91.3 | LOS F | 26.2 | 198.7 | 1.00 | 0.98 | 32.2 |
| Approach | 2393 | 10.1 | 0.964 | 34.4 | LOS C | 26.2 | 198.7 | 0.64 | 0.64 | 48.2 |
| North: Governor Macquarie Drive (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 727 | 7.8 | 0.689 | 52.1 | LOS D | 21.9 | 163.5 | 0.94 | 0.85 | 40.3 |
| 8 T1 | 128 | 2.3 | 0.518 | 63.9 | LOS E | 8.3 | 59.5 | 0.98 | 0.79 | 27.0 |
| 9 R2 | 180 | 31.5 | 1.040 | 120.0 | LOS F | 16.7 | 148.9 | 1.00 | 1.08 | 22.4 |
| Approach | 1035 | 11.3 | 1.040 | 65.4 | LOS E | 21.9 | 163.5 | 0.96 | 0.88 | 35.0 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 132 | 29.9 | 1.226 | 165.8 | LOS F | 121.0 | 929.5 | 1.00 | 1.47 | 18.7 |
| 11 T1 | 3011 | 7.5 | 1.226 | 158.5 | LOS F | 124.2 | 933.4 | 1.00 | 1.49 | 23.9 |
| 12 R2 | 5 | 20.0 | 0.047 | 33.1 | LOS C | 0.2 | 1.8 | 0.60 | 0.68 | 37.7 |
| Approach | 3148 | 8.5 | 1.226 | 158.6 | LOS F | 124.2 | 933.4 | 1.00 | 1.48 | 23.7 |
| All Vehicles | 7471 | 8.5 | 1.226 | 104.3 | LOS F | 124.2 | 933.4 | 0.88 | 1.10 | 29.5 |

## PHASING SUMMARY

Site: I-12 2030 MIMT \& SIMTA OPT 3 AM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 140 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E | G1 |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 66 | 88 | 112 |
| Green Time (sec) | 60 | 16 | 18 | 22 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 66 | 22 | 24 | 28 |
| Phase Split | $47 \%$ | $16 \%$ | $17 \%$ | $20 \%$ |



## MOVEMENT SUMMARY

## Site: I-12 2030 MIMT \& SIMTA OPT 3 PM

Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=140$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Brickmakers Drive (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 0.0 | 0.530 | 70.2 | LOS E | 6.8 | 49.8 | 0.99 | 0.78 | 26.9 |
| 2 T1 | 92 | 5.4 | 0.530 | 66.1 | LOS E | 6.8 | 49.8 | 0.99 | 0.78 | 26.5 |
| 3 R2 | 257 | 0.8 | 0.609 | 69.8 | LOS E | 8.6 | 60.6 | 1.00 | 0.80 | 32.6 |
| Approach | 360 | 1.9 | 0.609 | 68.9 | LOS E | 8.6 | 60.6 | 1.00 | 0.80 | 31.1 |
| East: Newbridge Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 654 | 1.4 | 0.461 | 9.4 | LOS A | 7.6 | 53.7 | 0.28 | 0.69 | 57.1 |
| 5 T1 | 2763 | 4.9 | 0.831 | 28.4 | LOS B | 51.8 | 380.1 | 0.76 | 0.76 | 52.1 |
| 6 R2 | 707 | 10.3 | 1.052 | 126.4 | LOS F | 33.5 | 255.2 | 1.00 | 1.06 | 26.9 |
| Approach | 4124 | 5.3 | 1.052 | 42.2 | LOS C | 51.8 | 380.1 | 0.72 | 0.80 | 45.1 |
| North: Governor Macquarie Drive (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 583 | 7.9 | 0.440 | 46.3 | LOS D | 15.7 | 117.1 | 0.85 | 0.81 | 42.1 |
| 8 T1 | 298 | 1.7 | 1.003 | 99.9 | LOS F | 25.1 | 177.9 | 1.00 | 1.09 | 20.9 |
| 9 R2 | 305 | 35.9 | 1.602 | 359.7 | LOS F | 46.6 | 428.1 | 1.00 | 1.47 | 9.9 |
| Approach | 1186 | 13.5 | 1.602 | 140.4 | LOS F | 46.6 | 428.1 | 0.93 | 1.05 | 21.9 |
| West: Newbridge Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 176 | 14.9 | 0.869 | 46.9 | LOS D | 46.6 | 350.2 | 0.94 | 0.90 | 38.8 |
| 11 T1 | 2099 | 5.6 | 0.869 | 38.9 | LOS C | 47.4 | 349.2 | 0.92 | 0.88 | 47.4 |
| 12 R 2 | 4 | 0.0 | 0.070 | 54.5 | LOS D | 0.2 | 1.7 | 0.80 | 0.69 | 30.3 |
| Approach | 2279 | 6.3 | 0.869 | 39.5 | LOS C | 47.4 | 350.2 | 0.93 | 0.88 | 46.8 |
| All Vehicles | 7948 | 6.6 | 1.602 | 57.3 | LOS E | 51.8 | 428.1 | 0.82 | 0.86 | 39.4 |

## PHASING SUMMARY

Site: I-12 2030 MIMT \& SIMTA OPT 3 PM
Newbridge Road / Governor Macquarie Drive
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 140 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | D | E |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |  |  |  |
| Phase Change Time (sec) | 0 | 64 | 86 |  |  |  |
| Green Time (sec) | 58 | 16 | 15 |  |  |  |
| Yellow Time (sec) | 4 | 4 | 4 |  |  |  |
| All-Red Time (sec) | 2 | 2 | 2 |  |  |  |
| Phase Time (sec) | 64 | 22 | 21 |  |  |  |
| Phase Split | 46 \% | 16 \% | 15 \% |  |  |  |
| Phase A | Phase D$\underbrace{\text { dIL }}$ |  |  |  | Phase E | Phase G1 |

## I-13 Intersection of Moorebank Avenue and M5 Motorway

## MOVEMENT SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 3 AM
Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 74 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Total veh/h | lows HV \% | Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 402 | 36.9 | 0.443 | 10.4 | LOS A | 5.1 | 54.8 | 0.49 | 0.70 | 48.5 |
| 2 T1 | 718 | 10.7 | 0.881 | 40.7 | LOS C | 15.5 | 123.5 | 1.00 | 1.08 | 34.5 |
| 3 R2 | 320 | 6.5 | 0.464 | 33.5 | LOS C | 5.7 | 43.3 | 0.91 | 0.79 | 36.6 |
| Approach | 1440 | 17.1 | 0.881 | 30.7 | LOS C | 15.5 | 123.5 | 0.84 | 0.91 | 38.1 |
| East: M5 Motorway on\&off ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 384 | 12.6 | 0.826 | 29.9 | LOS C | 13.0 | 106.2 | 0.99 | 1.02 | 38.3 |
| 6 R2 | 237 | 6.2 | 0.246 | 28.8 | LOS C | 3.4 | 25.1 | 0.82 | 0.76 | 40.4 |
| Approach | 621 | 10.2 | 0.826 | 29.5 | LOS C | 13.0 | 106.2 | 0.92 | 0.92 | 39.1 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 51 | 47.9 | 0.050 | 7.9 | LOS A | 0.4 | 3.5 | 0.29 | 0.60 | 51.1 |
| 8 T1 | 290 | 17.7 | 0.373 | 26.7 | LOS B | 4.5 | 38.8 | 0.89 | 0.72 | 40.5 |
| 9 R2 | 454 | 25.5 | 0.772 | 37.8 | LOS C | 10.0 | 85.2 | 0.97 | 0.88 | 36.3 |
| Approach | 794 | 24.1 | 0.772 | 31.8 | LOS C | 10.0 | 85.2 | 0.90 | 0.80 | 38.4 |
| West: M5 Motorway on\&off ramp (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1722 | 7.5 | 0.977 | 8.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.50 | 51.2 |
| 12 R2 | 861 | 16.1 | 1.009 | 87.7 | LOS F | 27.8 | 240.6 | 1.00 | 1.34 | 23.0 |
| Approach | 2583 | 10.4 | 1.009 | 34.7 | LOS C | 27.8 | 240.6 | 0.33 | 0.78 | 37.1 |
| All Vehicles | 5438 | 14.1 | 1.009 | 32.6 | LOS C | 27.8 | 240.6 | 0.62 | 0.83 | 37.8 |

## PHASING SUMMARY

## Site: I-13 2030 MIMT \& SIMTA OPT 3 AM

Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=74$ seconds (User-Given Phase Times)

| Phase Timing Results | A | E | F |
| :--- | :---: | :---: | :---: |
| Phase | Yes | No | No |
| Reference Phase | 0 | 24 | 51 |
| Phase Change Time (sec) | 17 | 20 | 16 |
| Green Time (sec) | 4 | 4 | 4 |
| Yellow Time (sec) | 3 | 3 | 3 |
| All-Red Time (sec) | 24 | 27 | 23 |
| Phase Time (sec) | $32 \%$ | $36 \%$ | $31 \%$ |
| Phase Split |  |  |  |



## MOVEMENT SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 3 PM
Moorebank Avenue / the M5 Motorway
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time $=94$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Demand | Flows | Deg. Satn | Average | Level of | 95\% Bac | of Queue | Prop. | Effective | Average |
| v | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 739 | 15.3 | 1.081 | 137.1 | LOS F | 67.9 | 585.0 | 1.00 | 1.43 | 17.1 |
| 2 T1 | 268 | 13.4 | 1.036 | 107.6 | LOS F | 10.2 | 83.8 | 1.00 | 1.28 | 20.3 |
| 3 R 2 | 446 | 9.1 | 0.399 | 29.6 | LOS C | 8.4 | 66.6 | 0.78 | 0.78 | 38.2 |
| Approach | 1453 | 13.0 | 1.081 | 98.7 | LOS F | 67.9 | 585.0 | 0.93 | 1.20 | 21.3 |
| East: M5 Motorway on\&off ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 459 | 7.1 | 0.567 | 16.5 | LOS B | 8.9 | 68.3 | 0.69 | 0.81 | 45.5 |
| 6 R2 | 97 | 21.7 | 0.177 | 42.7 | LOS D | 2.0 | 16.2 | 0.89 | 0.73 | 34.9 |
| Approach | 556 | 9.7 | 0.567 | 21.1 | LOS B | 8.9 | 68.3 | 0.72 | 0.79 | 43.0 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 139 | 6.1 | 0.118 | 7.9 | LOS A | 1.3 | 9.9 | 0.30 | 0.63 | 52.3 |
| 8 T1 | 756 | 7.4 | 0.844 | 43.9 | LOS D | 18.8 | 143.7 | 1.00 | 1.00 | 33.4 |
| 9 R2 | 1488 | 7.0 | 0.920 | 43.0 | LOS D | 34.3 | 254.6 | 1.00 | 1.06 | 34.8 |
| Approach | 2383 | 7.1 | 0.920 | 41.3 | LOS C | 34.3 | 254.6 | 0.96 | 1.02 | 35.1 |
| West: M5 Motorway on\&off ramp (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 620 | 13.8 | 0.367 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 54.4 |
| 12 R2 | 362 | 32.2 | 0.779 | 52.2 | LOS D | 8.9 | 92.6 | 1.00 | 0.93 | 30.3 |
| Approach | 982 | 20.6 | 0.779 | 22.9 | LOS B | 8.9 | 92.6 | 0.37 | 0.67 | 42.7 |
| All Vehicles | 5374 | 11.4 | 1.081 | 51.3 | LOS D | 67.9 | 585.0 | 0.82 | 0.98 | 31.5 |

## PHASING SUMMARY

Site: I-13 2030 MIMT \& SIMTA OPT 3 PM

## Moorebank Avenue / the M5 Motorway

2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 94 seconds (User-Given Phase Times)

Phase Timing Results

| Phase | A | C | E | F |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 14 | 30 | 53 |
| Green Time (sec) | 7 | 9 | 16 | 34 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 | 3 |
| Phase Time (sec) | 14 | 16 | 23 | 41 |
| Phase Split | $15 \%$ | $17 \%$ | $24 \%$ | $44 \%$ |

Phase A

## I-14 Intersection of M5 Motorway and Hume Highway

## MOVEMENT SUMMARY

Site: I-14 2030 MIMT \& SIMTA OPT 3 AM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time $=159$ seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 4256 | 4.6 | 1.027 | 59.4 | LOS E | 152.3 | 1108.5 | 1.00 | 1.21 | 33.2 |
| 3 R2 | 718 | 3.8 | 0.987 | 68.7 | LOS E | 24.5 | 177.1 | 1.00 | 1.03 | 31.0 |
| Approach | 4974 | 4.5 | 1.027 | 60.8 | LOS E | 152.3 | 1108.5 | 1.00 | 1.18 | 32.9 |
| East: M5 Motorway on\&off-ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 338 | 5.9 | 0.134 | 30.5 | LOS C | 4.8 | 35.4 | 0.60 | 0.71 | 41.9 |
| 6 R2 | 1212 | 6.5 | 1.289 | 358.8 | LOS F | 74.4 | 560.4 | 1.00 | 1.54 | 7.2 |
| Approach | 1550 | 6.3 | 1.289 | 287.2 | LOS F | 74.4 | 560.4 | 0.91 | 1.36 | 9.5 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 827 | 9.2 | 0.695 | 15.2 | LOS B | 28.8 | 224.1 | 0.58 | 0.75 | 44.9 |
| 8 T1 | 1208 | 6.7 | 0.490 | 28.5 | LOS B | 17.8 | 131.7 | 0.62 | 0.55 | 43.3 |
| Approach | 2036 | 7.7 | 0.695 | 23.1 | LOS B | 28.8 | 224.1 | 0.60 | 0.63 | 43.8 |
| All Vehicles | 8560 | 5.6 | 1.289 | 92.8 | LOS F | 152.3 | 1108.5 | 0.89 | 1.08 | 25.3 |

## PHASING SUMMARY

Site: I-14 2030 MIMT \& SIMTA OPT 3 AM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | No | No | No | Yes |
| Phase Change Time (sec) | 20 | 97 | 123 | 0 |
| Green Time (sec) | 70 | 19 | 29 | 13 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 | 3 |
| Phase Time (sec) | 77 | 26 | 36 | 20 |
| Phase Split | $48 \%$ | $16 \%$ | $23 \%$ | $13 \%$ |

Phase A

## MOVEMENT SUMMARY

## Site: I-14 2030 MIMT \& SIMTA OPT 3 PM

M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. SatnTotal HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Hume Highway (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 2555 | 3.9 | 0.624 | 2.2 | LOS A | 7.1 | 51.1 | 0.12 | 0.11 | 58.3 |
| 3 R2 | 401 | 1.8 | 1.023 | 122.1 | LOS F | 20.4 | 145.1 | 1.00 | 1.07 | 22.6 |
| Approach | 2956 | 3.6 | 1.023 | 18.4 | LOS B | 20.4 | 145.1 | 0.24 | 0.24 | 48.0 |
| East: M5 Motorway on\&off-ramp (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1535 | 3.3 | 1.154 | 259.1 | LOS F | 102.5 | 737.7 | 1.00 | 1.36 | 13.2 |
| 6 R2 | 1291 | 5.6 | 1.300 | 369.9 | LOS F | 82.2 | 612.7 | 1.00 | 1.56 | 7.0 |
| Approach | 2826 | 4.3 | 1.300 | 309.7 | LOS F | 102.5 | 737.7 | 1.00 | 1.45 | 10.0 |
| North: Hume Highway (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 883 | 5.6 | 0.695 | 14.5 | LOS A | 27.6 | 207.7 | 0.60 | 0.81 | 45.6 |
| 8 T1 | 2837 | 2.4 | 0.870 | 20.5 | LOS B | 51.6 | 368.7 | 0.78 | 0.73 | 47.0 |
| Approach | 3720 | 3.2 | 0.870 | 19.1 | LOS B | 51.6 | 368.7 | 0.74 | 0.75 | 46.7 |
| All Vehicles | 9502 | 3.7 | 1.300 | 105.3 | LOS F | 102.5 | 737.7 | 0.66 | 0.80 | 23.5 |

## PHASING SUMMARY

Site: I-14 2030 MIMT \& SIMTA OPT 3 PM
M5 Motorway / Hume Highway
2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Signals - Fixed Time Cycle Time = 159 seconds (User-Given Phase Times)
Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 97 | 121 |
| Green Time (sec) | 90 | 17 | 31 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 3 | 3 | 3 |
| Phase Time (sec) | 97 | 24 | 38 |
| Phase Split | $61 \%$ | $15 \%$ | $24 \%$ |



## I-15 Intersection of Cambridge Avenue and Canterbury Road MOVEMENT SUMMARY

Site: I-15 2030 MIMT \& SIMTA OPT 3 AM
Canterbury Road / Cambridge Avenue / Glenfield Road 2030 MIMT \& SIMTA Opt 3 AM PEAK 7:45 am - 8:45 am
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Canterbury Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 449 | 3.5 | 0.517 | 6.3 | LOS A | 3.4 | 24.2 | 0.61 | 0.71 | 52.9 |
| 2 T1 | 8 | 0.0 | 0.959 | 15.7 | LOS B | 25.6 | 181.8 | 1.00 | 1.10 | 46.0 |
| $3 \quad \mathrm{R} 2$ | 1187 | 1.8 | 0.959 | 21.1 | LOS B | 25.6 | 181.8 | 1.00 | 1.10 | 46.1 |
| Approach | 1645 | 2.2 | 0.959 | 17.0 | LOS B | 25.6 | 181.8 | 0.89 | 0.99 | 47.6 |
| East: Cambridge Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 307 | 3.1 | 0.163 | 3.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.43 | 56.5 |
| 5 T1 | 81 | 7.8 | 0.079 | 4.9 | LOS A | 0.4 | 3.1 | 0.45 | 0.54 | 53.7 |
| 6 R2 | 54 | 9.8 | 0.079 | 10.2 | LOS A | 0.4 | 3.1 | 0.45 | 0.57 | 53.9 |
| Approach | 442 | 4.8 | 0.163 | 4.6 | LOS A | 0.4 | 3.1 | 0.14 | 0.47 | 55.6 |
| North: Railway Parade (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 362 | 0.6 | 1.057 | 97.8 | LOS F | 24.0 | 169.1 | 1.00 | 1.87 | 23.0 |
| 8 T1 | 3 | 0.0 | 0.696 | 38.1 | LOS C | 5.9 | 41.8 | 1.00 | 1.20 | 36.3 |
| 9 R2 | 168 | 1.9 | 0.696 | 43.5 | LOS D | 5.9 | 41.8 | 1.00 | 1.20 | 34.3 |
| Approach | 534 | 1.0 | 1.057 | 80.3 | LOS F | 24.0 | 169.1 | 1.00 | 1.65 | 25.5 |
| West: Glenfield Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 399 | 6.3 | 1.873 | 433.0 | LOS F | 102.2 | 755.5 | 1.00 | 3.27 | 6.5 |
| 11 T1 | 240 | 7.0 | 1.873 | 433.7 | LOS F | 102.2 | 755.5 | 1.00 | 3.16 | 6.6 |
| 12 R2 | 367 | 6.9 | 1.873 | 440.7 | LOS F | 82.0 | 607.6 | 1.00 | 2.94 | 6.7 |
| Approach | 1007 | 6.7 | 1.873 | 436.0 | LOS F | 102.2 | 755.5 | 1.00 | 3.12 | 6.6 |
| All Vehicles | 3628 | 3.6 | 1.873 | 141.1 | LOS F | 102.2 | 755.5 | 0.85 | 1.62 | 17.7 |

## MOVEMENT SUMMARY

$\theta$ Site: I-15 2030 MIMT \& SIMTA OPT 3 PM
Canterbury Road / Cambridge Avenue / Glenfield Road 2030 MIMT \& SIMTA Opt 3 PM PEAK 4:30 pm - 5:30 pm
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Deman Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Canterbury Road (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 338 | 2.2 | 0.505 | 9.7 | LOS A | 3.4 | 24.2 | 0.82 | 0.96 | 50.3 |
| 2 T1 | 6 | 0.0 | 0.426 | 7.8 | LOS A | 2.8 | 19.5 | 0.79 | 0.95 | 50.9 |
| 3 R2 | 334 | 1.3 | 0.426 | 13.2 | LOS A | 2.8 | 19.5 | 0.79 | 0.95 | 51.0 |
| Approach | 678 | 1.7 | 0.505 | 11.4 | LOS A | 3.4 | 24.2 | 0.81 | 0.96 | 50.7 |
| East: Cambridge Avenue (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1285 | 2.0 | 0.677 | 3.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.43 | 56.3 |
| 5 T1 | 325 | 7.1 | 0.505 | 7.5 | LOS A | 4.4 | 31.7 | 0.78 | 0.79 | 51.8 |
| 6 R2 | 370 | 0.9 | 0.505 | 13.0 | LOS A | 4.4 | 31.7 | 0.84 | 0.84 | 51.9 |
| Approach | 1981 | 2.6 | 0.677 | 6.0 | LOS A | 4.4 | 31.7 | 0.28 | 0.57 | 54.7 |
| North: Railway Parade (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 125 | 1.7 | 0.192 | 7.9 | LOS A | 1.0 | 6.9 | 0.69 | 0.80 | 52.8 |
| 8 T1 | 0 | 0.0 | 0.000 | 0.0 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.0 |
| 9 R2 | 240 | 8.3 | 0.296 | 12.7 | LOS A | 1.7 | 12.8 | 0.73 | 0.86 | 50.0 |
| Approach | 365 | 6.1 | 0.296 | 11.0 | LOS A | 1.7 | 12.8 | 0.72 | 0.84 | 51.0 |
| West: Glenfield Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 271 | 4.7 | 0.450 | 9.2 | LOS A | 3.1 | 22.5 | 0.79 | 0.89 | 50.6 |
| 11 T1 | 54 | 0.0 | 0.450 | 9.1 | LOS A | 3.1 | 22.5 | 0.79 | 0.89 | 52.5 |
| 12 R2 | 451 | 3.7 | 0.522 | 14.5 | LOS B | 4.3 | 31.1 | 0.83 | 0.94 | 48.8 |
| Approach | 775 | 3.8 | 0.522 | 12.3 | LOS A | 4.3 | 31.1 | 0.81 | 0.92 | 49.7 |
| All Vehicles | 3799 | 3.0 | 0.677 | 8.7 | LOS A | 4.4 | 31.7 | 0.53 | 0.73 | 52.6 |

## 7. Mitigation measures for cumulative scenario 3

## I-01 Intersection of Moorebank Avenue, Anzac Road and Bapaume Road

## MOVEMENT SUMMARY

Site: I-01 Cumulative Scenario 3 AM UP
Intersection of Moorebank Avenue, Anzac Road and Bapaume Road 2030 Cumulative Scenario 3 AM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time $=120$ seconds (Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 20 | 0.0 | 0.734 | 22.8 | LOS B | 23.2 | 201.1 | 0.67 | 0.62 | 38.2 |
| 2 T1 | 1264 | 17.3 | 0.734 | 17.2 | LOS B | 23.2 | 201.1 | 0.67 | 0.61 | 43.5 |
| 3 R2 | 473 | 3.1 | 0.918 | 77.4 | LOS F | 16.4 | 118.2 | 1.00 | 1.00 | 23.2 |
| Approach | 1757 | 13.3 | 0.918 | 33.5 | LOS C | 23.2 | 201.1 | 0.76 | 0.72 | 34.7 |
| East: Anzac Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 271 | 3.1 | 0.454 | 38.6 | LOS C | 12.5 | 89.9 | 0.83 | 0.81 | 33.2 |
| 5 T1 | 4 | 0.0 | 0.454 | 34.3 | LOS C | 12.5 | 89.9 | 0.83 | 0.81 | 32.2 |
| 6 R2 | 224 | 13.6 | 0.851 | 68.0 | LOS E | 14.4 | 112.8 | 1.00 | 0.95 | 26.9 |
| Approach | 499 | 7.8 | 0.851 | 51.8 | LOS D | 14.4 | 112.8 | 0.91 | 0.87 | 29.8 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 383 | 9.9 | 0.294 | 8.6 | LOS A | 5.3 | 40.2 | 0.32 | 0.65 | 51.1 |
| 8 T1 | 1452 | 13.4 | 0.904 | 30.7 | LOS C | 37.7 | 316.5 | 0.75 | 0.79 | 35.8 |
| 9 R2 | 101 | 3.1 | 0.393 | 57.2 | LOS E | 5.5 | 39.6 | 0.95 | 0.78 | 25.1 |
| Approach | 1936 | 12.2 | 0.904 | 27.7 | LOS B | 37.7 | 316.5 | 0.67 | 0.76 | 37.6 |
| West: Bapaume Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 5 | 60.0 | 0.013 | 12.5 | LOS A | 0.1 | 1.0 | 0.48 | 0.58 | 41.6 |
| 11 T1 | 1 | 0.0 | 0.015 | 56.1 | LOS D | 0.1 | 0.8 | 0.94 | 0.61 | 26.7 |
| 12 R2 | 1 | 0.0 | 0.015 | 59.8 | LOS E | 0.1 | 0.8 | 0.94 | 0.61 | 22.9 |
| Approach | 7 | 42.9 | 0.015 | 25.5 | LOS B | 0.1 | 1.0 | 0.61 | 0.59 | 35.0 |
| All Vehicles | 4199 | 12.2 | 0.918 | 33.0 | LOS C | 37.7 | 316.5 | 0.74 | 0.76 | 35.2 |

## PHASING SUMMARY

## Site: I-01 Cumulative Scenario 3 AM UP

Intersection of Moorebank Avenue, Anzac Road and Bapaume Road 2030 Cumulative Scenario 3 AM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time $=120$ seconds (Optimum Cycle Time - Minimum Delay)
Phase Timing Results

| Phase | A | B | D |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 69 | 97 |
| Green Time (sec) | 63 | 22 | 17 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 69 | 28 | 23 |
| Phase Split | $58 \%$ | $23 \%$ | $19 \%$ |



## MOVEMENT SUMMARY

## Site: I-01 Cumulative Scenario 3 PM UP

Intersection of Moorebank Avenue, Anzac Road and Bapaume Road 2030 Cumulative Scenario 3 PM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time $=115$ seconds (Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Demand | Flows | Deg. Satn | Average | Level of | 95\% Bac | of Queue | Prop. | Effective | Average |
| v | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0.0 | 0.706 | 24.2 | LOS B | 21.0 | 179.1 | 0.69 | 0.62 | 37.5 |
| 2 T1 | 1186 | 14.3 | 0.706 | 18.6 | LOS B | 21.0 | 179.1 | 0.69 | 0.62 | 42.5 |
| 3 R2 | 261 | 0.8 | 1.016 | 112.2 | LOS F | 10.7 | 75.4 | 1.00 | 1.17 | 18.3 |
| Approach | 1448 | 11.8 | 1.016 | 35.5 | LOS C | 21.0 | 179.1 | 0.74 | 0.72 | 33.8 |
| East: Anzac Road (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 568 | 2.2 | 0.835 | 45.4 | LOS D | 31.5 | 224.5 | 0.98 | 0.92 | 30.9 |
| 5 T1 | 1 | 0.0 | 0.835 | 41.1 | LOS C | 31.5 | 224.5 | 0.98 | 0.92 | 30.0 |
| 6 R2 | 391 | 5.4 | 1.053 | 138.8 | LOS F | 38.7 | 283.2 | 1.00 | 1.29 | 17.2 |
| Approach | 960 | 3.5 | 1.053 | 83.4 | LOS F | 38.7 | 283.2 | 0.99 | 1.07 | 23.0 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 353 | 3.9 | 0.257 | 7.1 | LOS A | 3.2 | 23.3 | 0.24 | 0.62 | 52.4 |
| 8 T1 | 1419 | 13.2 | 0.904 | 33.0 | LOS C | 41.0 | 341.5 | 0.82 | 0.87 | 34.7 |
| $9 \quad \mathrm{R} 2$ | 23 | 18.2 | 0.202 | 63.1 | LOS E | 1.3 | 10.5 | 0.98 | 0.71 | 23.7 |
| Approach | 1795 | 11.4 | 0.904 | 28.3 | LOS B | 41.0 | 341.5 | 0.71 | 0.82 | 37.5 |
| West: Bapaume Road (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 111 | 4.8 | 0.286 | 16.8 | LOS B | 2.2 | 15.8 | 0.69 | 0.72 | 40.3 |
| 11 T1 | 7 | 0.0 | 0.058 | 35.4 | LOS C | 0.8 | 5.3 | 0.78 | 0.66 | 32.7 |
| 12 R2 | 11 | 0.0 | 0.058 | 39.1 | LOS C | 0.8 | 5.3 | 0.78 | 0.66 | 28.6 |
| Approach | 128 | 4.1 | 0.286 | 19.7 | LOS B | 2.2 | 15.8 | 0.71 | 0.71 | 38.6 |
| All Vehicles | 4332 | 9.6 | 1.053 | 42.7 | LOS D | 41.0 | 341.5 | 0.78 | 0.84 | 31.6 |

## PHASING SUMMARY

## Site: I-01 Cumulative Scenario 3 PM UP

Intersection of Moorebank Avenue, Anzac Road and Bapaume Road
2030 Cumulative Scenario 3 PM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time = 115 seconds (Optimum Cycle Time - Minimum Delay)

## Phase Timing Results

| Phase | A | C | B |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 63 | 101 |
| Green Time (sec) | 57 | 32 | 8 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 63 | 38 | 14 |
| Phase Split | $55 \%$ | $33 \%$ | $12 \%$ |



## I-02 Intersection of Moorebank Avenue and DNSDC Access

## MOVEMENT SUMMARY

Site: I-02 Cumulative Scenario 3 AM UP
Intersection of Moorebank Avenue and DNSDC Access 2030 Cumulative Scenario 3 AM PEAK - Proposed Upgrade Signals - Fixed Time Cycle Time = 100 seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1718 | 11.7 | 0.627 | 0.5 | LOS A | 2.1 | 17.3 | 0.06 | 0.05 | 59.4 |
| $3 \quad \mathrm{R} 2$ | 44 | 2.4 | 0.201 | 17.9 | LOS B | 1.0 | 7.3 | 0.69 | 0.72 | 43.8 |
| Approach | 1762 | 11.5 | 0.627 | 1.0 | LOS A | 2.1 | 17.3 | 0.07 | 0.07 | 58.8 |
| East: DNSDC Access (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 6 | 33.3 | 0.466 | 60.3 | LOS E | 1.5 | 22.3 | 1.00 | 0.74 | 29.3 |
| 6 R2 | 39 | 83.8 | 0.466 | 62.7 | LOS E | 1.5 | 22.3 | 1.00 | 0.74 | 21.8 |
| Approach | 45 | 76.7 | 0.466 | 62.4 | LOS E | 1.5 | 22.3 | 1.00 | 0.74 | 22.8 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 516 | 11.4 | 0.773 | 16.6 | LOS B | 24.4 | 200.7 | 0.66 | 0.73 | 42.0 |
| 8 T1 | 1205 | 11.9 | 0.773 | 6.6 | LOS A | 24.4 | 200.7 | 0.47 | 0.47 | 52.9 |
| Approach | 1721 | 11.7 | 0.773 | 9.6 | LOS A | 24.4 | 200.7 | 0.53 | 0.55 | 49.3 |
| All Vehicles | 3528 | 12.4 | 0.773 | 6.0 | LOS A | 24.4 | 200.7 | 0.31 | 0.31 | 52.9 |

## PHASING SUMMARY

Site: I-02 Cumulative Scenario 3 AM UP
Intersection of Moorebank Avenue and DNSDC Access 2030 Cumulative Scenario 3 AM PEAK - Proposed Upgrade Signals - Fixed Time Cycle Time = 100 seconds (User-Given Cycle Time)

Phase Timing Results

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Reference Phase | Yes | No | No |
| Phase Change Time (sec) | 0 | 72 | 88 |
| Green Time (sec) | 66 | 10 | 6 |
| Yellow Time (sec) | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 |
| Phase Time (sec) | 72 | 16 | 12 |
| Phase Split | $72 \%$ | $16 \%$ | $12 \%$ |



## MOVEMENT SUMMARY

## Site: I-02 Cumulative Scenario 3 PM UP

Intersection of Moorebank Avenue and DNSDC Access 2030 Cumulative Scenario 3 PM PEAK - Proposed upgrade Signals - Fixed Time Cycle Time $=100$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop.Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1083 | 13.4 | 0.457 | 2.2 | LOS A | 3.6 | 30.2 | 0.15 | 0.13 | 57.7 |
| 3 R2 | 1 | 100.0 | 0.016 | 21.0 | LOS B | 0.0 | 0.4 | 0.52 | 0.63 | 42.1 |
| Approach | 1084 | 13.5 | 0.457 | 2.2 | LOS A | 3.6 | 30.2 | 0.15 | 0.13 | 57.7 |
| East: DNSDC Access (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 21 | 0.0 | 0.855 | 59.5 | LOS E | 10.7 | 83.5 | 1.00 | 0.98 | 29.9 |
| 6 R2 | 363 | 7.2 | 0.855 | 59.7 | LOS E | 10.7 | 83.5 | 1.00 | 0.97 | 25.1 |
| Approach | 384 | 6.8 | 0.855 | 59.7 | LOS E | 10.7 | 83.5 | 1.00 | 0.97 | 25.4 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 46 | 88.6 | 0.819 | 11.4 | LOS A | 16.8 | 138.5 | 0.37 | 0.37 | 46.6 |
| 8 T1 | 1952 | 8.1 | 0.819 | 4.2 | LOS A | 16.8 | 138.5 | 0.36 | 0.35 | 55.8 |
| Approach | 1998 | 10.0 | 0.819 | 4.3 | LOS A | 16.8 | 138.5 | 0.36 | 0.35 | 55.6 |
| All Vehicles | 3466 | 10.8 | 0.855 | 9.8 | LOS A | 16.8 | 138.5 | 0.37 | 0.35 | 50.1 |

## PHASING SUMMARY

## Site: I-02 Cumulative Scenario 3 PM UP

Intersection of Moorebank Avenue and DNSDC Access
2030 Cumulative Scenario 3 PM PEAK - Proposed upgrade
Signals - Fixed Time Cycle Time = 100 seconds (User-Given Cycle Time)
Phase Timing Results

| Phase | A | B |
| :--- | :---: | :---: |
| Reference Phase | Yes | No |
| Phase Change Time (sec) | 0 | 75 |
| Green Time (sec) | 69 | 19 |
| Yellow Time (sec) | 4 | 4 |
| All-Red Time (sec) | 2 | 2 |
| Phase Time (sec) | 75 | 25 |
| Phase Split | $75 \%$ | $25 \%$ |



## I-03 Intersection of Moorebank Avenue, MIMT Main Access and SIMTA Central Access

## MOVEMENT SUMMARY

Site: I-03 Cumulative Scenario 3 AM UP
Intersection of Moorebank Avenue, MIMT Main Access and SIMTA Central Access 2030 Cumulative Scenario 3 AM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time $=120$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo v | Demand Flows Deg. Satn Total HV |  |  | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Stop Rate | Average Speed |
|  |  |  |  | Vehicles |  | Distance |  |  |  |
|  | veh/h | \% | v/c |  | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) per |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 7 | 0.0 | 0.693 | 9.5 | LOS A | 12.1 | 93.4 | 0.27 | 0.25 | 50.2 |
| 2 T1 | 1709 | 8.7 | 0.693 | 3.9 | LOS A | 12.1 | 93.4 | 0.26 | 0.25 | 56.3 |
| 3 R 2 | 19 | 5.6 | 0.212 | 68.4 | LOS E | 1.1 | 8.3 | 0.99 | 0.70 | 20.4 |
| Approach | 1736 | 8.7 | 0.693 | 4.7 | LOS A | 12.1 | 93.4 | 0.27 | 0.25 | 55.7 |
| East: SIMTA Central Access (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 100.0 | 0.239 | 65.6 | LOS E | 1.0 | 18.3 | 0.97 | 0.72 | 20.2 |
| 6 R2 | 32 | 100.0 | 0.239 | 66.6 | LOS E | 1.0 | 18.3 | 0.97 | 0.71 | 23.9 |
| Approach | 33 | 100.0 | 0.239 | 66.6 | LOS E | 1.0 | 18.3 | 0.97 | 0.71 | 23.8 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 398 | 13.0 | 0.501 | 14.5 | LOS B | 13.3 | 110.2 | 0.45 | 0.64 | 45.0 |
| 8 T1 | 775 | 9.4 | 0.501 | 4.2 | LOS A | 13.3 | 110.2 | 0.23 | 0.26 | 55.4 |
| 9 R2 | 39 | 54.1 | 0.701 | 75.9 | LOS F | 2.6 | 34.7 | 1.00 | 0.85 | 22.7 |
| Approach | 1212 | 12.0 | 0.701 | 9.9 | LOS A | 13.3 | 110.2 | 0.33 | 0.40 | 50.1 |
| West: Main Access (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 21 | 100.0 | 0.133 | 50.2 | LOS D | 1.1 | 20.2 | 0.86 | 0.72 | 27.6 |
| 12 R2 | 1 | 0.0 | 0.006 | 58.1 | LOS E | 0.1 | 0.4 | 0.93 | 0.59 | 22.3 |
| Approach | 22 | 95.2 | 0.133 | 50.6 | LOS D | 1.1 | 20.2 | 0.87 | 0.71 | 27.3 |
| All Vehicles | 3002 | 11.6 | 0.701 | 7.8 | LOS A | 13.3 | 110.2 | 0.31 | 0.32 | 52.4 |

## PHASING SUMMARY

## Site: I-03 Cumulative Scenario 3 AM UP

Intersection of Moorebank Avenue, MIMT Main Access and SIMTA Central Access
2030 Cumulative Scenario 3 AM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time = 120 seconds (User-Given Cycle Time)

| Phase Timing Results | A | B | D |
| :--- | :---: | :---: | :---: |
| Phase | Yes | No | No |
| Reference Phase | 0 | 88 | 108 |
| Phase Change Time (sec) | 82 | 14 | 6 |
| Green Time (sec) | 4 | 4 | 4 |
| Yellow Time (sec) | 2 | 2 | 2 |
| All-Red Time (sec) | 88 | 20 | 12 |
| Phase Time (sec) | $73 \%$ | $17 \%$ | $10 \%$ |
| Phase Split |  |  |  |

Phase A

## MOVEMENT SUMMARY

## Site: I-03 Cumulative Scenario 3 PM UP

Intersection of Moorebank Avenue, MIMT Main Access and SIMTA Central Access 2030 Cumulative Scenario 3 PM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time $=120$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID ODMo | Demand | Flows | Deg. Satn | Average | Level of | 95\% Bac | of Queue | Prop. | Effective | Average |
| v | Total | HV |  | Delay | Service | Vehicles | Distance | Queued | Stop Rate | Speed |
|  | veh/h | \% | v/c | sec |  | veh | m |  | per veh | km/h |
| South: Moorebank Avenue (S) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0.0 | 0.398 | 18.8 | LOS B | 8.5 | 71.0 | 0.45 | 0.39 | 41.5 |
| 2 T1 | 706 | 14.3 | 0.398 | 13.6 | LOS A | 8.8 | 73.1 | 0.45 | 0.40 | 49.1 |
| 3 R 2 | 1 | 100.0 | 0.020 | 42.7 | LOS D | 0.0 | 0.6 | 0.74 | 0.64 | 26.6 |
| Approach | 708 | 14.4 | 0.398 | 13.6 | LOS A | 8.8 | 73.1 | 0.45 | 0.40 | 49.0 |
| East: SIMTA Central Access (E) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 17 | 0.0 | 0.905 | 76.3 | LOS F | 12.1 | 94.6 | 1.00 | 1.03 | 18.9 |
| 6 R2 | 339 | 7.1 | 0.905 | 76.3 | LOS F | 12.3 | 97.2 | 1.00 | 1.02 | 22.6 |
| Approach | 356 | 6.8 | 0.905 | 76.3 | LOS F | 12.3 | 97.2 | 1.00 | 1.02 | 22.5 |
| North: Moorebank Avenue (N) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 40 | 100.0 | 0.879 | 21.9 | LOS B | 39.5 | 311.3 | 0.69 | 0.70 | 42.2 |
| 8 T1 | 1912 | 5.1 | 0.879 | 15.4 | LOS B | 39.5 | 311.3 | 0.67 | 0.67 | 47.8 |
| 9 R2 | 21 | 100.0 | 0.508 | 75.2 | LOS F | 1.4 | 26.3 | 1.00 | 0.76 | 22.9 |
| Approach | 1973 | 8.1 | 0.879 | 16.3 | LOS B | 39.5 | 311.3 | 0.67 | 0.67 | 47.3 |
| West: Main Access (W) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 39 | 54.1 | 0.247 | 38.3 | LOS C | 1.6 | 22.0 | 0.92 | 0.73 | 31.0 |
| 12 R2 | 7 | 0.0 | 0.034 | 55.6 | LOS D | 0.4 | 2.7 | 0.91 | 0.66 | 22.9 |
| Approach | 46 | 45.5 | 0.247 | 41.0 | LOS C | 1.6 | 22.0 | 0.92 | 0.72 | 29.7 |
| All Vehicles | 3083 | 9.9 | 0.905 | 22.9 | LOS B | 39.5 | 311.3 | 0.66 | 0.65 | 42.8 |

## PHASING SUMMARY

## Site: I-03 Cumulative Scenario 3 PM UP

Intersection of Moorebank Avenue, MIMT Main Access and SIMTA Central Access 2030 Cumulative Scenario 3 PM PEAK - Proposed Upgrade
Signals - Fixed Time Cycle Time $=120$ seconds (User-Given Cycle Time)

## Phase Timing Results

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Reference Phase | Yes | No | No | No |
| Phase Change Time (sec) | 0 | 68 | 88 | 108 |
| Green Time (sec) | 62 | 14 | 14 | 6 |
| Yellow Time (sec) | 4 | 4 | 4 | 4 |
| All-Red Time (sec) | 2 | 2 | 2 | 2 |
| Phase Time (sec) | 68 | 20 | 20 | 12 |
| Phase Split | $57 \%$ | $17 \%$ | $17 \%$ | $10 \%$ |



## Appendix J

Strategic traffic modelling report (August 2014)

Moorebank Intermodal Company

## Strategic Traffic Modelling for Moorebank Intermodal Terminal

26 September 2014


## Document information

## Client: Moorebank Intermodal Company

Title: Strategic Traffic Modelling for Moorebank Intermodal Terminal
Document No: 2189293E-ITP-REP-001 RevA
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| Author, Reviewer and Approver details |  |  |  |
| :--- | :--- | :--- | :--- |
| Prepared by: | Mihiri Elangasinghe | Date: 25/09/2014 | Signature: |
| Reviewed by: | Brian Betts | Date: 25/09/2014 | Signature: |
| Approved by: | John Webster | Date: 26/09/2014 | Signature: |

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Parsons Brinckerhoff Australia Pty Limited
ABN 80078004798
Level 27 Ernst \& Young Centre
680 George Street
Sydney NSW 2000
GPO Box 5394
Sydney NSW 2001
Australia
Tel: +61 292725100
Fax: +61 292725101
www.pbworld.com
Certified to ISO 9001, ISO 14001, OHSAS 18001

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## 1. Introduction

The Moorebank Intermodal Terminal (IMT) Project (the Project) involves the construction and operation of an IMT and associated commercial facilities and warehousing on a site of approximately 220 hectares. The development includes a rail connecting spur to the planned Southern Sydney Freight Line (SSFL) and road entry and exit points from Moorebank Avenue.

The primary function of the IMT is to be a transfer point in the logistics chain for shipping containers in the handling of both international IMEX cargo, and domestic interstate and intrastate (regional) cargo. The key aims of the Project are to increase Sydney's rail freight mode share including: promoting the movement of container freight by rail between Port Botany and western and south-western Sydney; and reducing road freight on Sydney's congested road network.

The Project proponent is Moorebank Intermodal Company (MIC), a Government Business Enterprise set up to facilitate the development of the Project.

The Project site is currently largely occupied by the Department of Defence's (Defence) School of Military Engineering (SME). Under the approved Moorebank Units Relocation (MUR) Project, the SME is planned to be relocated to Holsworthy Barracks by mid-2015, which would enable the construction of the Project to commence.

The key features/components of the Project comprise:

- an IMEX freight terminal - designed to handle up to 1.05 million TEU per annum (525,000 TEU inbound and 525,000 TEU outbound) of IMEX containerised freight to service 'port shuttle' train services between Port Botany and the Project;
- an Interstate freight terminal - designed to handle up to 500,000 TEU per annum (250,000 TEU inbound and 250,000 TEU outbound) of interstate containerised freight to service freight trains travelling to and from regional and interstate destinations; and
- warehousing facilities - with capacity for up to 300,000 square metres $\left(\mathrm{m}^{2}\right)$ of warehousing to provide an interface between the IMT and commercial users of the facilities such as freight forwarders, logistics facilities and retail distribution centres.

The proposal concept described in the main EIS (refer Chapters 7 and 8) provides an indicative layout and operational concept for the Project, while retaining flexibility for future developers and operators of the Project. The proposal concept is indicative only and subject to further refinement during detailed design. The EIS considers three rail access options for the site.

### 1.1 Project location and study area

The Project is situated in the Sydney suburb of Moorebank; NSW located approximately 35 km south west from the centre of Sydney and approximately 2 km south of Liverpool CBD. It is located in the Liverpool City Council (LCC) Local Government Area (LGA). The site is bounded by Moorebank Avenue to the east, the East Hills Railway Line to the south, the Georges River to the west and the ABB (a power and automation technology manufacturer) and the M5 South Western Motorway to the north. The M5 provides access to other Sydney motorways, with the M7 interchange approximately 5 km by road west of the proposed site.

The Southern Sydney Freight Line has been constructed on the western side of the Georges River along the South Line/Bankstown Line and would be used to service the terminal by rail.


[^0]Figure 1.1 Project site and context

Figure 1.1 Project site and context

### 1.2 Strategic modelling scope

This report describes the strategic modelling which has been undertaken to provide forecasts input for the transport and accessibility impact assessment. The key output from the strategic model is the changes in the level of articulated truck movements on the local and the wider strategic road network as a consequence of the Project. The strategic level changes are to be based on the differences between the 'Project Case' compared to 'Base Case' scenarios which represents the operation of the road network with and without the Project.

Since the reduction of trucks vehicle kilometres on the roads is one of the projects main goals, the extent to which this goal could be achieved is investigated and reported. This is based around the premise that the Moorebank IMT is an effective means for managing future growth in congestion.

The wider operation of the network can be assessed by considering the metrics of vehicle kilometres travelled (VKT) and vehicle hours travelled (VHT) that together represent the change in usage of the road network. The strategic modelling considers the operation of the Moorebank IMT for the following:

- Planning years (2018 and 2030)
- Time periods (Two hours AM peak, and total daily)
- Class of vehicles (Articulated trucks, and background traffic)
- Traffic on impacted corridors including the M5,M7, and F3 motorways as well as Hume Highway/Cumberland Highway, Foreshore Road, General Holmes Drive and Pennant Hills Road


## 2. Existing strategic models

### 2.1 Introduction

Strategic modelling has been undertaken to investigate the traffic related changes associated with the Moorebank IMT Project. This analysis has been based on utilising the Transport for New South Wales (TfNSW) strategic models to examine the projected changes on truck volumes resulting from the operations of the 'Project Case' as compared to the 'Base Case' without the Project.

The travel demand sources available to the study include:

- Sydney Strategic Travel Model (STM)
- Light Commercial Vehicle Model (LCVM)
- Freight Movement Model (FMM) for rigid and articulated commercial vehicles

These three components provide the travel demand across the highway network. The supply of highway network has been based on:

- Roads and Maritime Services (RMS) highway network as used in the STM.

These four data sources are outlined in Table 2.1.
Table 2.1 Strategic model components

| Demand / Supply | Data | Class of vehicles | Sources |
| :--- | :--- | :--- | :--- |
| Demand | Background traffic | Car | STM |
|  | Light commercial vehicle | LCVM |  |
|  | Rigid trucks | FMM |  |
|  | Articulated trucks (non <br> Port Botany and <br> Moorebank IMT) | FMM |  |
| Supply | Port Botany and |  |  |
| Moorebank IMT | Articulated trucks | FMM |  |
| Highway Network | All | RMS networks as used in the STM <br> highway assignment |  |

These data sources have all been developed with the same geographic coverage and modelling zoning system (2006 travel zones) to provide a compatible set of travel demand trip tables. An overview of each of these models is provided in the following sections.

### 2.2 Sydney Strategic Travel Model

The Sydney Strategic Travel Model (STM) is a State Government model that is owned and operated by BTS an independent entity with TfNSW. The STM has been developed over the last 15 to 20 years to represent the movement of people in Sydney Greater Metropolitan Area (GMA), Newcastle and Illawarra. The study area encompasses nearly 5.5 million people (2010) and represents some 20 million trips on a typical weekday (2010).

The STM is the States Government strategic forecasting tool used to support the evaluation of:

- Major infrastructure changes;
- Different population/employment growth and distribution scenarios;
- Service change;
- Pricing change; and
- Policy change.

The STM currently contains a series of demographic and behavioural models which collectively produce estimates of home based travel by travel purpose. The key attributes of the STM are as follows:

- Travel demand is modelled as person tours
- Tour-based models reflect the relationships and constraints between individual trips in terms of mode and destination choices.
- A tour in the STM is any travel from home to a primary destination and back to home. For example, while most employed people will only have one work tour on a working day, those who return home for lunch will have two tours. The Household Travel Surveys (HTS) indicates that in 92\% of cases, the outward and return leg of a work tour are symmetrical in terms of mode, so for modelling purposes, symmetry is assumed.
- The tours modelled in the STM do not include any side trips made along the way, and any non-homebased tours. For example, someone on the way to work may drop off children at the school, then, during work may go to a meeting at another location then back to the primary work place, and after work may go shopping before returning to home. These side trips are currently modelled in the STM for car driver mode by factoring the tours by purpose using factors based on the HTS.

The model is implemented in two stages as follows:

- Population Model - the population is segmented into groups based on socio-demographics that influence travel choices, as well as on the basis of car ownership and licence holding. These segments are grown into the future based on population, employment and other projections and trends. This segmentation occurs at the model wide level and the travel zone level.
- Travel Model - a series of travel models in EMME have been developed that represent travel by purpose, of travel frequency, mode and destination choice, calibration based on the Journey-to-Work and HTS data, addition of freight movements, and assignment of travel to the road and public transport networks.

The process is further documented in the 'Sydney Strategic Travel Model (STM) - Modelling future travel patterns - February 2011 Release - Bureau of Transport Statistics.

The net result of the process is that the STM together with the LCVM and FMM provide traffic forecasts for vehicles on the road network. This demand is estimated at a 24 hour level and then is allocated to four model time periods as follows:

- AM peak (0700-0900)
- PM peak (1500-1800)
- Inter peak (0900-1500)
- Evening/night time period (1800-0700)

The STM has been supplied to the study from BTS and the assumptions relating to this model are detailed in Appendix A.

The STM was supplied with a 2011 base year and future networks for 2016 to 2041 in five year increments. Table 2.2 lists the changes that the STM road network should contain as per the documentation supplied with the model. It is noted that the form/alignment of some of the projects identified in Table 2.2 may differ from the latest planning documentation and this is because the detailed investigations around these projects are still underway.

Table 2.2: Official network changes

| Year | Road | Detail |
| :---: | :---: | :---: |
| 2016 | Hunter Motorway | Four-lane expressway from F3 to Branxton |
|  | M2 widening | Widening from Windsor Road to Delhi Road |
|  | M5 widening | Widening Camden Valley Way to King Georges Road |
|  | Western Sydney Employment Hub | Link Roads to the M7 Motorway |
|  | Great Western Highway widening | Widening the highway to four/three lanes between Emu Plains and Mount Victoria. |
|  | South West Rail Link via East Hills | There are some changes to the road network around Edmondson Park that are likely to be related to this project (i.e. links to rail stations, etc.). |
| 2021 | WestConnex Stage 1: M5 East Duplication | Duplication from M5 East to King Georges Road <br> It is noted that the changes included in the 2021 network extend to parts of the WestConnex project beyond the M5 East duplication such as the Sydney Airport Access Link, etc (as per the WestConnex Sydney's next motorway priority, October 2012, RMS document). |
|  | North West Rail Link to Rouse Hill | There are changes to the 2021 model road network around Kellyville which is likely to be associated with this project. |
| 2026 | WestConnex Stage 2: M4 Extension and M4 Widening | M4 widening and extension from Parramatta to Haberfield |
|  | NW Growth Centre | The 2026 model road network includes changes to links in the area to the north west of the M7 which are likely to be related to this project. |
| 2031 | M2 to F3 Tunnel | Connection between M2 and F3 at Wahroonga |
|  | SW Growth Centre | This is seen in the model as various network changes (i.e. new links, upgraded links, etc) to the west of the Hume Highway and the M7. |

The changes between each of the forecast years are shown in Appendix B. However there are changes to the road network which are not covered in Table 2.2 (i.e. not discussed in the documentation provided with the model). The most notable of these changes is the extension of Cambridge Avenue to Campbell Town Road which first appears in 2026 and is also present in the 2031 network. This is the only change that is likely to have a significant bearing on the results of the investigations relating to the Moorebank Intermodal Terminal Development. Discussions with Roads and Maritime Services Indicate that this extension is not currently part of the future 2031 network. Therefore the modelling undertaken for this study has removed this extension from the model network.

### 2.3 Sydney Light Commercial Vehicle Model

Similar to the STM the Sydney Light Commercial Vehicle Model (LCVM) is owned and operated by BTS an independent entity within TfNSW. The model has been developed ton the same premise as the STM as a strategic forecasting tool used to support the evaluation of transport interventions.

The LCVM produces light commercial vehicle demand based on the Austroads vehicle classes 1 and 2 that relate to light commercial vehicle movements such as delivery vans. The model coverage is the same as the STM and includes the Sydney Greater Metropolitan Area (GMA), Newcastle and Illawarra. The model is calibrated to a 2011 base year, and produces forecasts at five yearly intervals to 2046. To maintain consistency, the LCVM is based around the 2006 travel zone system and utilises the same population and employment data as the STM.

The LCVM is based on a trip attraction / production modelling combined with a trip distribution model. The trip attraction model is based on the zonal level details for

- household forecasts based on August 2012 Release: BTS Population Forecasts
- employment forecasts based on August 2012 Release: BTS Employment Forecasts
- trip attraction rates for households, office, industrial, retail and hospitality based on Service Vehicle Attraction Rate study, 1999 (SVAR)and the LCV Trip Attraction Rates study, 2009 (LTAR)

The trip production is based on assuming the over a 24 hour period that each zones produces the same numbers as it attracts. The trip distribution model is based on a gravity model that uses the trips attracted and produced by each zone in conjunction with a friction factor that combines travel times with calibrated parameters that align with the trip distribution observed in the base year. The 24 hour trip matrices are converted to the four model periods based factors derived from the LCV Trip Attraction Rates study, 2009 (LTAR).

Table 2.3 Time period factors in LCVM

|  | AM peak <br> $(0700-0900)$ | Inter peak <br> $(0900-1500)$ | PM peak <br> $(1500-1800)$ | Evening / Night <br> Time (1800-0700) |
| :--- | :---: | :---: | :---: | :---: |
| Proportion of 24 <br> hour demand | 0.16 | 0.61 | 0.13 | 0.10 |

Due to the nature and to some extent ambiguities of LCVs, there is a risk of double-counting, since the STM car demand actually includes 'some' LCV trips in its estimates of total travel movements, through the data provided from the Household Travel Survey (HTS). While this HTS data for LCVs provides a wealth of detailed information for use in the STM, it does not necessarily provide the most accurate estimate of total LCV movements. Fundamentally, the HTS sample is household (not business) based and the survey expansion variables used are designed to optimize the accuracy of trips for personal (not business) travel. With the February 2014 release of LCVM forecasts, BTS compared the 2011 base year LCVM estimates with HTS estimates. The key finding from this analysis was that, for 2011, the HTS captured $35 \%$ of total LCV movements. As a result, the LCVM estimates should be factored by 0.65 (65\%) to take into account the overlap in travel demand in the LCVM matrices with the STM car demand. Further details of the LCVM as provided by BTS are provided in Appendix A.

### 2.4 Sydney Freight Movement Model

Similar to the STM the Sydney Freight Movement Model (FMM) is owned and operated by BTS an independent entity within TfNSW. The model has been developed ton the same premise as the STM as a strategic forecasting tool used to support the evaluation of transport interventions.

The FMM produces heavy commercial vehicle demand based on the splitting demand between rigid and articulated vehicles. The model coverage is the same as the STM and includes the Sydney Greater Metropolitan Area (GMA), Newcastle and Illawarra. The model is calibrated to a 2011 base year, and produces forecasts at five yearly intervals to 2036. To maintain consistency, the FMMs based around the 2006 travel zone system and utilise the same employment data as the STM.

The FMM consists of a number of sub-models as follows:

- Production (and consumption) models which estimate freight produced (and consumed) based on employment and other data.
- A two stage distribution model which estimates freight movements based upon distribution patterns between industry classes, and then between freight areas based on accessibility (employment and travel time).
- Freight vehicle trip models which estimate the number of trips of different mode types given this freight distribution.
- Vehicle assignment model based on assigned the vehicle demand onto the STM network, which estimate the volume of freight vehicles on road sections, given the freight vehicle trip distribution.

The assignment to the road network is based on allocating loads to either rigid or articulated heavy vehicles, which are then assigned to the road network. This method is used for the estimating of heavy goods movements across the strategic model area except for special generators.

The method is revised for special generators such as Port Botany. The movement of freight to and from Port Botany is driven by the growth of import and export activities which is projected to rise at rates above those for general freight movements. This has been recognised in the FMM together with the role of intermodal terminals have in servicing the movement of freight to and from Port Botany. The operation of Ports are typically measured in twenty-foot equivalent unit (TEUs) containers, with Port Botany set to expand from its current 2 million TEUs in financial year 2011/12 to over 7 million TEUs by 2031.

The assumed Port Botany of freight vehicle split between rigid and articulated, the level of back-loading and TEU's per truck are shown in Table 2.4.

Table 2.4 Vehicle characteristics - Port Botany

| Vehicle characteristics | 2011 | 2021 | 2031 | 2041 |
| :--- | :---: | :---: | :---: | :---: |
| Rigid vehicle (\% of Total HV) | $9 \%$ | $9 \%$ | $9 \%$ | $9 \%$ |
| Articulated vehicle (\% of Total HV) | $91 \%$ | $91 \%$ | $91 \%$ | $91 \%$ |
| Back-loading | $11.3 \%$ | $13.8 \%$ | $16.3 \%$ | $18.8 \%$ |
| TEUs/Truck (laden movements) | 2.04 | 2.14 | 2.16 | 2.18 |
| TEUs/Rigid | 1.00 | 1.00 | 1.00 | 1.00 |
| TEUs/Articulated | 2.14 | 2.25 | 2.27 | 2.30 |

The assumed level of daily operation and split of movements over the day for Port Botany in the FMM are shown in Table 2.5.

Table 2.5 Operational characteristics - Port Botany

| Operational characteristics | 2011 | 2021 | 2031 | 2041 |
| :--- | :---: | :---: | :---: | :---: |
| Annual Operational Days | 303 | 313 | 323 | 333 |
| AM peak (0700-0900) | $13.3 \%$ | $13.3 \%$ | $11.9 \%$ | $9.2 \%$ |
| Inter peak (0900-1500) | $41.1 \%$ | $41.1 \%$ | $37.3 \%$ | $27.6 \%$ |
| PM peak (1500-1800) | $15.0 \%$ | $17.1 \%$ | $16.8 \%$ | $13.8 \%$ |
| Night time (1800-0700) | $30.6 \%$ | $28.6 \%$ | $34.0 \%$ | $49.4 \%$ |

Port Botany is assumed to be serviced by rail using the following inter modal terminals, and the FMM also includes the other IMT (in addition to Moorebank):

- Minto (TZ2006 = 1261)
- Yennora $($ TZ2006 $=1826)$
- Enfield $($ TZ2006 $=1598)$
- Moorebank (TZ2006 = 1120)
- Eastern Creek $($ TZ2006 $=2185)$

The locations of these zones in the model is shown in Figure 2.1.


Figure 2.1: Intermodal terminals
The articulated truck demand to and from the intermodal terminals in the FMM is shown in Table 2.6. The Moorebank IMT has significantly more truck movements than any of the other IMT's with Eastern Creek having the second highest volume of freight movements.

Table 2.6: $\quad 2031$ FMM articulated truck totals to/from intermodal terminals

| Site | Movement | $\begin{aligned} & \text { AM peak } \\ & \text { (0700-0900) } \end{aligned}$ | $\begin{aligned} & \text { Inter peak } \\ & \text { (0900-1500) } \end{aligned}$ | $\begin{aligned} & \text { PM peak } \\ & \text { (1500-1800) } \end{aligned}$ | Evening / Night Time (1800-0700) | Daily Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minto | From | 28 | 94 | 40 | 76 | 238 |
|  | To | 29 | 97 | 39 | 79 | 244 |
| Yennora | From | 28 | 96 | 36 | 77 | 237 |
|  | To | 25 | 88 | 39 | 70 | 222 |
| Enfield | From | 10 | 33 | 13 | 26 | 82 |
|  | To | 9 | 33 | 14 | 27 | 82 |
| Eastern Creek | From | 44 | 151 | 60 | 121 | 376 |
|  | To | 43 | 144 | 61 | 122 | 371 |
| Moorebank | From | 136 | 466 | 194 | 372 | 1,168 |
|  | To | 139 | 476 | 190 | 379 | 1,184 |

Figures 2.2 and 2.3 show the distribution of articulated trucks from each of the intermodal terminals (IMT's) in the AM and PM peaks respectively in the FMM. These figures show that there is some overlap between the IMT catchments; Moorebank and Minto are the first and second most popular origins/destinations for freight in the model respectively. Freight movements to/from other intermodal terminals are significantly lower.


Figure 2.2: Distribution of articulated truck trips from the IMT's in 2031 AM peak


Figure 2.3: Distribution of articulated truck trips from the IMT's in 2031 PM peak

### 2.5 Summary of strategic models

The strategic models provided by BTS have been reviewed to identify the scale of trip making related to the model has a whole and specifically related to the movements to/from the zones representing the Moorebank IMT and Port Botany zones (i.e. Zone 1120 represents the Moorebank IMT and zones 426 and 556 represent Port Botany).

The scale of the trips for car, LCV, rigid and articulated trucks for the whole of the model and for movements to and from Moorebank and Port Botany are shown in Tables 2.6 to 2.9.

Table 2.7 STM Car/LCV trips in 2031

| Movement | AM peak <br> $(0700-0900)$ | Inter peak <br> $(0900-1500)$ | PM peak <br> $(\mathbf{1 5 0 0 - 1 8 0 0 )}$ | Evening / <br> Night Time <br> $(\mathbf{1 8 0 0 - 0 7 0 0 )}$ | Daily Total |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Total Trips | $2,419,566$ | $4,591,602$ | $3,738,389$ | $3,473,856$ | $14,223,413$ |
| From Moorebank | 153 | 756 | 1,433 | 870 | 3,212 |
| To Moorebank | 1,246 | 861 | 335 | 774 | 3,216 |
| From Port Botany | 120 | 792 | 1,757 | 1,035 | 3,704 |
| To Port Botany | 1,584 | 948 | 302 | 858 | 3,692 |

Table 2.8 LCV trips in 2031

| Movement | AM peak <br> $(0700-0900)$ | Inter peak <br> $(0900-1500)$ | PM peak <br> $(1500-1800)$ | Evening / <br> Night Time <br> $(\mathbf{1 8 0 0 - 0 7 0 0 )}$ | Daily Total |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Total Trips | 171,851 | 655,183 | 139,629 | 105,658 | $1,072,320$ |
| From Moorebank | 84 | 320 | 68 | 53 | 524 |
| To Moorebank | 83 | 320 | 69 | 50 | 522 |
| From Port Botany | 99 | 378 | 80 | 63 | 619 |
| To Port Botany | 97 | 380 | 81 | 63 | 620 |

Table 2.9 FMM Rigid truck trips in 2031

| Movement | AM peak <br> $(0700-0900)$ | Inter peak <br> $(0900-1500)$ | PM <br> peak(1500- <br> $1800)$ | Evening / <br> Night Time <br> $(1800-0700)$ | Daily Total |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Total Trips | 45,391 | 147,390 | 57,329 | 81,411 | 331,521 |
| From Moorebank | 60 | 323 | 125 | 177 | 684 |
| To Moorebank | 101 | 329 | 126 | 183 | 738 |
| From Port Botany | 95 | 263 | 132 | 402 | 891 |
| To Port Botany | 119 | 389 | 149 | 212 | 868 |

Table 2.10 FMM Articulated truck trips in 2031

| Movement | AM peak <br> $(0700-0900)$ | Inter peak <br> $(0900-1500)$ | PM peak <br> $(1500-1800)$ | Evening / <br> Night Time <br> $(1800-0700)$ | Daily Total |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Total Trips | 17,463 | 59,203 | 24,377 | 48,956 | 149,998 |
| From Moorebank | 136 | 466 | 194 | 373 | 1,168 |
| To Moorebank | 139 | 476 | 190 | 379 | 1,184 |
| From Port Botany | 786 | 2,187 | 1,097 | 3,344 | 7,414 |
| To Port Botany | 836 | 2,860 | 1,209 | 2,287 | 7,192 |

The daily distribution of origins and destinations for articulated trucks to and from Moorebank and Port Botany as represented in the 2031 FMM matrices are shown in Table 2.10. The distribution of articulated trucks to and from the Moorebank zone in the FMM is localised and generally relates to locations within 2 to 3 kilometres of the intermodal terminal. The distributions of articulated trucks to and from the Port Botany zone in the FMM has a wider distribution (than for Moorebank) across the greater Sydney area, and many of the articulated truck trips travel between the industrial precinct at Wetherill Park (just north of Moorebank IMT) and Port Botany.

Table 2.11: FMM Distribution of articulated truck trips tolfrom Port Botany and Moorebank
To Moorebank


To Port Botany


From Moorebank


From Port Botany


## 3. Articulated truck demand

### 3.1 Introduction

The strategic models provide the framework for the analysis of the strategic traffic changes relating to the provision of the Moorebank Intermodal Terminal Project.

Deloitte were commissioned to undertake the task of determining the impact of the opening of Moorebank Intermodal terminal and assess the resulting articulated truck movements to and from Port Botany and Moorebank. To carry out this task Deloitte employed economic modelling to project future import and export demand and distribution across the Sydney metropolitan area. The information supplied related to the following scenarios:

- 'Base Case' : Port Botany operating without Moorebank Intermodal Terminal
- 'Project Case’ : Port Botany operating without Moorebank Intermodal Terminal

The level of import and export activity is outlined below together with the related truck movements.

### 3.2 Import and export demand

The assumed level of import and export activity on the road network related to the port and Moorebank Intermodal Terminal is summarised in Table 3.1.

Table 3.1 Import and export demand road based TEUS/year

| Scenario | 2018 | 2020 | 2025 | 2030 | 2035 | 2040 |
| :--- | ---: | ---: | ---: | ---: | ---: | :---: |
| 'Base Case' |  |  |  |  |  |  |
| Port Botany | $1,574,677$ | $1,787,546$ | $2,414,936$ | $3,206,501$ | $4,205,204$ | $5,465,247$ |
| 'Project Case' | $1,468,186$ | $1,368,107$ | $1,366,106$ | $2,157,671$ | $3,156,374$ | $4,416,417$ |
| Port Botany | 106,491 | 419,439 | $1,048,830$ | $1,048,830$ | $1,048,830$ | $1,048,830$ |
| Moorebank | $1,574,677$ | $1,787,546$ | $2,414,936$ | $3,206,501$ | $4,205,204$ | $5,465,247$ |
| Total |  |  |  |  |  |  |
| Supplied by Deloitte - Appendix C provides the distribution of TEU locations by Local Government Area |  |  |  |  |  |  |

This demand is assumed to be distributed on to the road network with both Port Botany and Moorebank operating 7 days per week and for 50 weeks a year resulting in yearly TEUs being divided by 350 to give daily operations.

The level of TEUs shown in Table 3.1 were then converted to truck movements based on allocating loads to articulated and B-Double trucks. This was undertaken by Deloitte's and supplied to Parsons Brinckerhoff in the form of truck movements specific to Port Botany and Moorebank for the 'Base Case' and 'Project Case' scenarios as shown in Table 3.2.

Table $3.2 \quad$ Daily Truck Movements - Round Trips

| Scenario | Vehicle Type | 2018 | 2020 | 2025 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 'Base Case' |  |  |  |  |  |  |  |
| Port Botany | Semi-trailer | 1,566 | 1,892 | 2,402 | 3,190 | 4,183 | 5,436 |
|  | B-Double | 696 | 790 | 1,068 | 1,418 | 1,859 | 2,416 |
|  | Total | 2,262 | 2,682 | 3,470 | 4,608 | 6,042 | 7,852 |
| 'Project Case' |  |  |  |  |  |  |  |
| Port Botany | Semi-trailer | 1,460 | 1,361 | 1,359 | 2,146 | 3,140 | 4,393 |
|  | B-Double | 649 | 605 | 604 | 954 | 1,395 | 1,953 |
|  | Total | 2,109 | 1,966 | 1,963 | 3,100 | 4,535 | 6,346 |
| Reduction to Port Botany |  | 153 | 716 | 1,507 | 1,508 | 1,507 | 1,506 |
| Moorebank | Semi-trailer | 127 | 499 | 1,248 | 1,248 | 1,248 | 1,248 |
|  | B-Double | 21 | 83 | 208 | 208 | 208 | 208 |
|  | Total | 148 | 582 | 1456 | 1456 | 1456 | 1456 |
| Total | Semi-trailer | 1,587 | 1,860 | 2,607 | 3,394 | 4,388 | 5,641 |
|  | B-Double | 670 | 688 | 812 | 1,162 | 1,603 | 2,161 |
|  | Total | 2,257 | 2,548 | 3,419 | 4,556 | 5,991 | 7,802 |

Supplied by Deloitte, Appendix C provides the distribution of daily truck movements by Local Government Area Note: 1 round trip results in the trip matrices of 1 trip to the site and 1 trip from the site.

The forecast truck movements supplied by Deloitte does not align with the strategic model years and therefore the demand in Table 3.2 for 2030 and 2035 has been interpolated to estimate truck movements in 2031. Since the Moorebank Intermodal Terminal import and export movements remain unchanged from 2025 the interpolation only applies to movements relating to Port Botany. The daily truck movements in Table 3.2 have been incorporated as articulated trips within the FMM trip matrices for the assignment process by replacing the original trips with the quantum and distribution defined by Deloitte. The remaining articulated trip movements remain unchanged.

### 3.3 Interstate demand

The Moorebank Intermodal Terminal is assumed to capture the interstate movements from Chullora once it closes from 2030 onwards. In the 'Base Case' it is assumed that Chullora continues to operate with a capacity of 350,000 TEUs per annum. In the 'Project Case' case it is assumed that Chullora closes from 2030 and that the freight activities transfer to Moorebank. The level of truck trips related to the transfer of the interstate traffic to Moorebank is as follows:

- 410 daily truck movements in 2030
- 430 daily truck movements in 2035
- 460 daily truck movements in 2040

The road based freight trips that service Chullora are assumed to move to Moorebank with the distribution remaining the same as those used in the FMM when Chullora was operational.

### 3.4 Background traffic

Other vehicles utilise and impact on the operation of the road network. This is known as the background traffic since it does not change with respect to the 'Base Case' and 'Project Case' scenarios. This traffic is comprises cars, LCVs, rigid and articulated goods vehicles. This traffic has been sourced from the STM, LVC and FMM trip matrices and is assigned to the road networks provided.

### 3.5 Time profile

The strategic modelling for the project has utilised the time periods that are compatible with the STM structure which is based on modelling the travel demand for the following four time periods:

- AM peak (0700-0900)
- PM peak (1500-1800)
- Inter peak (0900-1500)
- Evening/night time period (1800-0700)

The Moorebank Intermodal Terminal is expected to operate 24 hours per day from 2030 onwards.
To distribute the total daily volume of IMEX traffic to/from Port Botany and Moorebank specified by Deloitte across the four model time periods, it was assumed that these distributions would follow the same pattern as IMEX traffic to/from Port Botany across the time periods in the FMM model (see Table 3.3).
Table 3.3 FMM distribution of articulated trips to/from Port Botany across time periods

|  | AM Peak | Inter-peak | PM Peak | Evening period |
| :--- | :---: | :---: | :---: | :---: |
| From Port Botany | $11 \%$ | $29 \%$ | $15 \%$ | $45 \%$ |
| To Port Botany | $11 \%$ | $40 \%$ | $17 \%$ | $32 \%$ |

Interstate traffic was assumed to have a uniform hourly arrival/departure profile. This was due to the longer distances that interstate trucks are required to travel and the greater likelihood that the arrival/departure of these trucks would be more random (and therefore equally likely to occur at any time of the day) than traffic travelling from within the Sydney area.

Background traffic is assumed to have the time profiles as defined in the strategic models.

### 3.6 Truck distributions for Port Botany and Moorebank

The truck distribution for the movement of freight to Port Botany and Moorebank as presented in Tables 3.1 and 3.2 is based on the following assumptions.

- Import and export movements are to be based on the demand split defined by Deloitte for each of the Local Government Areas (LGA) within the Sydney Greater Metropolitan Area (GMA).
- For the six of the LGA's with the highest proportion of trips to/from Moorebank (i.e. Penrith, Blacktown, Liverpool, Fairfield, Campbelltown and Camden) a further breakdown by postcode was provided by Deloitte. Details of this breakdown by postcode are provided in Appendix D.
- Within each LGA (or postcode where provided) it is assumed that the trips are spread across each of the Travel Area Zones (TAZ) in line with the FMM distribution.
- Interstate trucks are assumed to have the ultimate trip end (origin/destination) that reflect the FMM forecast share for the Chullora facility.

The daily distribution of truck movements to and from Port Botany in the 'Base Case' scenario is shown in Table 3.4, while for the 'Project Case' scenario is shown in Table 3.5 and 3.6 for Port Botany and Moorebank. These distributions relate to the movement of truck trips to the strategic model zone.

Table 3.4: 'Base Case’ articulated truck distributions tolfrom Port Botany
From Port Botany


To Port Botany


Table 3.5: 'Project Case' articulated truck distributions tolfrom Port Botany
From Port Botany


To Port Botany


Table 3.6: 'Project Case' articulated truck distributions to/from Moorebank
From Moorebank


To Moorebank


## 4. Strategic network performance

### 4.1 Introduction

Performance of the strategic network in the 'Base Case' and 'Project Case' scenarios has compared using the following metrics:

- Network wide performance based vehicle kilometres and hours travelled
- Key corridor flows on the following roads:
- M5 Motorway
- M2 Motorway
- M7 Motorway
- Foreshore Road / Botany Road
- Pennant Hills Road
- M1 Motorway (to Newcastle)
- General Holmes Drive
- Hume and Cumberland Highway

The key corridors are shown in Figure 4.1.

### 4.2 Network performance

The performance of the whole network can be assessed by considering the vehicle kilometres and hours travelled in each of the assignments by the users of the road network. Table 4.1 and 4.2 compares the vehicle kilometres travelled (VKT) and vehicle hours travelled (VHT) across the modelled network by class of vehicle and time period for the 'Base Case' and 'Project Case'.

The results in indicate that:

- the 'Project Case' results in a decrease in both VKT and VHT across the network as a whole compared to the 'Base Case', with most of the reductions seen in articulated truck movements. Although articulated truck trips to and from Port Botany see the greatest reduction in VKT and VHT, other (i.e. background) articulated truck traffic are also expected to see decreases in VKT and VHT under the 'Project Case'.
- on an average weekday the implementation of the 'Project Case' results in a reduction of 45,460 vehicle kilometres travelled and 3,800 vehicle hours travelled by all vehicles across the network
- on an average weekday the implementation of the 'Project Case' results a reduction of articulated truck vehicle kilometres travelled of 36,185 and 670 fewer vehicle hours travelled.
- assuming that Port Botany and Moorebank operate for 350 days per year this is an annual reduction of $12,665,365$ vehicle kilometres and 234,160 vehicle hours travelled by articulated trucks to and from Port Botany and Moorebank. (This annual savings calculation is an approximation based on applying the calculation of savings on an average weekday to 350 days, but it is noted that only a maximum of 260 will be working days. However it is not possible to determine the impact of the project on non-working days as the strategic models are setup to model an average weekday.)

It is noted that while there appears to be a slight increase in VKT for rigid trucks and cars/LCV under the 'Project Case', these modes see reductions in VHT under the 'Project Case'. This is likely to be the result of rerouting of car/LCV and rigid truck movements in the 'Project Case' scenario model to use routes that are longer but require less time.


Figure $4.1 \quad$ Strategic assessment corridors

Table 4.1 Comparison of vehicle kilometres travelled in 2031

| Scenario |  | AM peak (0700-0900) | $\begin{gathered} \text { Inter peak } \\ (0900-1500) \end{gathered}$ | PM peak (1500-1800) | Evening / Night Time (1800-0700) | Daily Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 'Base Case' |  |  |  |  |  |  |
| Back'd | Cars/LCV | 26,372,160 | 44,427,270 | 35,339,960 | 32,255,885 | 138,395,280 |
|  | Rigid | 1,081,310 | 3,498,060 | 1,365,460 | 1,948,635 | 7,893,460 |
|  | Articulated | 707,500 | 2,412,920 | 984,585 | 1,936,065 | 6,041,070 |
| Port Botany | Articulated | 42,840 | 134,645 | 61,155 | 149,670 | 388,310 |
| 'Project Case' |  |  |  |  |  |  |
| Back'd | Cars/LCV | 26,373,920 | 44,430,700 | 35,342,360 | 32,258,965 | 138,405,950 |
|  | Rigid | 1,081,410 | 3,498,000 | 1,365,575 | 1,948,265 | 7,893,250 |
|  | Articulated | 705,055 | 2,406,070 | 981,100 | 1,929,115 | 6,021,335 |
| Port Botany | Articulated | 28,335 | 89,135 | 40,480 | 98,745 | 256,690 |
| Moorebank | Articulated | 28,335 | 89,135 | 40,480 | 98,745 | 256,690 |
| Difference relative to 'Base Case' |  |  |  |  |  |  |
| Back'd | Cars/LCV | 1,760 | 3,430 | 2,400 | 3,080 | 10,670 |
|  | Rigid | 100 | -60 | 115 | -365 | -205 |
|  | Articulated | -2,450 | -6,845 | $-3,485$ | -6,955 | -19,735 |
| Port Botany | Articulated | -14,510 | -45,510 | -20,675 | -50,925 | -131,620 |
| Moorebank | Articulated | 10,785 | 33,425 | 15,610 | 35,615 | 95,430 |
| Total | Cars/LCV | 1,760 | 3,430 | 2,400 | 3,080 | 10,670 |
|  | Rigid | 100 | -60 | 115 | -365 | -205 |
|  | Articulated | -6,170 | -18,930 | -8,550 | -22,265 | -55,920 |

Table 4.2 Comparison of vehicle hours travelled in 2031

| Scenario |  | AM peak (0700-0900) | Inter peak (0900-1500) | $\begin{aligned} & \text { PM peak } \\ & (1500-1800) \end{aligned}$ | Evening / Night Time (1800-0700) | Daily Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 'Base Case' |  |  |  |  |  |  |
| Back'd | Cars/LCV | 958,400 | 1,131,115 | 1,115,095 | 715,835 | 3,920,445 |
|  | Rigid | 32,640 | 77,245 | 36,215 | 37,615 | 183,710 |
|  | Articulated | 15,945 | 43,075 | 20,095 | 31,240 | 110,355 |
| Port Botany | Articulated | 1,440 | 2,950 | 1,695 | 2,830 | 8,910 |
| 'Project Case' |  |  |  |  |  |  |
| Back'd | Cars/LCV | 957,520 | 1,130,495 | 1,114,420 | 715,480 | 3,917,915 |
|  | Rigid | 32,610 | 77,185 | 36,180 | 37,585 | 183,565 |
|  | Articulated | 17,205 | 45,670 | 21,590 | 33,685 | 118,145 |
| Port Botany | Articulated | 940 | 1,920 | 1,105 | 1,835 | 5,800 |
| Moorebank | Articulated | 390 | 820 | 485 | 740 | 2,440 |
| Difference relative to 'Base Case' |  |  |  |  |  |  |
| Back'd | Cars/LCV | -880 | -620 | -675 | -355 | -2,530 |
|  | Rigid | -30 | -60 | -30 | -25 | -145 |
|  | Articulated | -75 | -150 | -95 | -130 | -450 |
| Port Botany | Articulated | -495 | -1,030 | -590 | -995 | -3,110 |
| Moorebank | Articulated | 390 | 820 | 485 | 740 | 2,440 |
| Total | Cars/LCV | -880 | -620 | -675 | -355 | -2,530 |
|  | Rigid | -30 | -60 | -30 | -25 | -145 |
|  | Articulated | -180 | -355 | -200 | -385 | -1,120 |

Figure 4.2 shows the change in articulated truck volumes on the network between the 'Project Case' and the 'Base Case'. This plot shows that the introduction of the Moorebank Intermodal Terminal:

- would result in reductions in articulated truck volumes through the Sydney CBD and inner city suburbs, on the M4 and the M5 east of the Moorebank Avenue interchange.
- would result in an increase in articulated truck flows, particularly on the M7, Hume Highway and Mamre Road south of the M4 as well as the M5 between Moorebank avenue interchange and the M7.

Figure 4.3 shows the net difference of articulated truck volumes relating to Port Botany and Moorebank only on the network. Comparing this to Figure 4.2 confirms that the changes in articulated truck volumes on the network are generally the result of changes at Port Botany and Moorebank; the changes to background articulated truck traffic is not significant.

Appendix E shows the change in articulated truck movements to/from Port Botany and Moorebank between the 'Base Case and the 'Project Case 'scenarios on corridors of interest. In general:

- The reductions in truck movements are generally experienced closer to the Sydney CBD (i.e. the M5 east of Moorebank Avenue, General Holmes Drive, Foreshore Road as well as the M2)
- The increases in truck movements are mostly seen in the corridors immediately around the Moorebank development (i.e. M7 south of the M4, and the Hume Highway).
- Some of the increases in truck movements (such as the increase on the M1 to Newcastle) are due to the shift of some articulated truck movements from Chullora to Moorebank in the Project Case (to account for the shift of interstate traffic to Moorebank from Chullora in 2031).

Figure 4.4 shows the contribution of Moorebank-traffic to total articulated truck flows on the network. As expected Moorebank traffic makes up a large portion of all articulated truck movements on parts of the network closer to Moorebank and in some cases closer to the other origin/destination zone. Moorebank traffic accounts for up to $20 \%$ of the articulated truck volumes on the M7 and up to $34 \%$ of the articulated truck traffic on the Hume highway

The Figures in Appendix F show the change in speed between the 'Base Case and 'Project Case' scenarios for each of the model time periods. In general the road links with reduced volumes (as per Figure 4.2) experience improved travel speeds in the 'Project Case' than the base case and conversely roads that see increased articulated truck movements in the "Project Case' experience degraded travel speeds in the 'Project Case' than the 'Base Case'. It is noted that the change in speed is small, with a maximum change of about $4 \mathrm{~km} / \mathrm{hr}$ on the wider network (the road links closer to Moorebank experience greater changes; up to 8 $\mathrm{km} / \mathrm{hr}$ ). This is to be expected as the changes attributed to the project would only have a small impact on a network as large as the Sydney road network.


Figure 4.2: Comparison of articulated truck volumes ('Project Case' versus 'Base Case')


Figure 4.3: Comparison of articulated truck volumes to/from Port Botany and Moorebank only ('Project Case' versus 'Base Case')


Figure 4.4 Percentage of articulated truck traffic tolfrom Moorebank (of all articulated truck flows on links - 'Project Case')

## Appendix A

Strategic modelling assumptions


## A1. Sydney Strategic Travel Model

The Sydney Strategic Travel Model (STM) was supplied to the project with the following documentation of the key assumptions. These assumptions have been reproduced from information supplied by BTS.

## A1.1 Model version

STM 2.5 based on the calculation of travel demand using 7 travel purposes, 7 travel modes, 2690 travel zones, 4 times of day) The purposes and modes are as follows:

Travel purposes:

- Work (commute from home to work and back)
- Business
- Primary education
- Secondary education
- Tertiary education
- Shopping
- Other

Travel mode

- Car driver
- Car passenger
- Train / Light rail / Ferry
- Bus
- Cycle
- Walk
- Taxi

The four time periods modelled are as follows:

- AM peak period (0700-0900)
- Inter peak period (0900-1500)
- PM peak (1500-1800)
- Evening/night time period (1800-0700)


## A1.2 Network assumptions

The STM network is based on the Long Term Transport Master Plan and includes the following changes in the supply network. Assumptions are for scenario modelling purposes and do not necessarily reflect Government policy).

Table A1.1 Network assumptions

| Year | Road | Rail / Light Rail | Bus / Ferry |
| :---: | :---: | :---: | :---: |
| 2006 | - Network version July $2009$ | - Network version ITIS March 2007 | - Network version ITIS March 2007 |
| 2011 | - Lane Cove Tunnel <br> - Inner West Busway (Iron Cove Bridge duplication) <br> - F3 widening <br> - Hume Highway widening | - Enhanced 2009 timetable network <br> - Cronulla duplication <br> - ECRL | - 131500 bus network and 2011 ferry network |
| 2016 | - Hunter Motorway (F3Branxton) <br> - M2 widening <br> - M5 widening <br> - W-Sydney Employment Hub <br> - Gt.Western Highway widening | - SWRL via East Hills <br> - LRT Dulwich Hill extension | - Bus route adjustments in SWRL sector, revised ferry network for 2016 |
| 2021 | - WestConnex Stage 1: M5 East Duplication | - North West Rail Link to Rouse Hill <br> - CBD and South East Light Rail | - CBD Bus plan, Regional level 1 and level 2 bus network, bus route adjustments in NWRL |
| 2026 | - WestConnex Stage 2: <br> M4 Extension and M4 Widening <br> NW Growth Centre | - 2021 heavy rail base (20 trains/h over SHB and City Circle) | and SWRL sectors, bus priority, <br> - revised ferry network |
| 2031 | - M2 to F3 Tunnel <br> - SW Growth Centre | - 2021 heavy rail base (20 trains/h over SHB and City Circle) |  |
| 2036 | - F6 <br> - NW Growth Centre | - 2036 heavy rail base (20 trains/h over SHB and City Circle) |  |
| 2041 | - M2 extension via Gladesville Bridge to M4 East <br> Spit bridge upgrade | - 2036 heavy rail base (20 trains/h over SHB and City Circle) |  |
| All <br> years <br> Travel Costs | - Fuel and toll costs rise with CPI | - MyZone fare system <br> - Fares rise with CPI, light rail treated as heavy rail for fare calculation purpose | - MyZone fare system <br> - Fares rise with CPI |

## A1.3 Land use assumptions

Table A1.2 Land use assumptions

| Year | GMA Population - <br> Aug 2012 BTS Forecasts | GMA Employment - <br> Aug 2012 BTS Forecasts |
| :--- | :---: | :---: |
| 2006 | $5,133,000$ | $2,467,000$ |
| 2011 | $5,578,000$ | $2,685,000$ |
| 2016 | $5,961,000$ | $2,904,000$ |
| 2021 | $6,331,000$ | $3,095,000$ |
| 2026 | $6,705,000$ | $3,271,000$ |
| 2031 | $7,077,000$ | $3,432,000$ |
| 2036 | $7,443,000$ | $3,595,000$ |
| 2041 | $7,805,000$ | $3,752,000$ |
| 2046 | $8,165,000$ | $3,901,00$ |

## A1.4 Heavy vehicle demand assumptions

BTS Freight Movement Model (FMM) - Freight Forecast December 2013 release.

## A1.5 Behavioural assumptions

- Behavioural models estimated using Household Travel Survey data up to and including 2008 and Journey to Work data up to and including 2006 Census.
- Assumed 1\% growth in real income per annum
- Travel behaviour responses to times, costs and modes within synthetic household classes (128 different types) assumed not to vary over time, although the number of people within each household class will vary along with demographic change and socio-economic change.


## A1.6 Cautions

- Aside from acknowledging that these forecasts are the product of the set of assumptions listed above, none of which may occur in reality, and which may not reflect government policy, users should also be aware of some other limitations inherent in Strategic Travel Models such as the STM:
- The STM is a simplification of reality. It breaks the GMR into 2,690 travel zones, and further by 128 population segments within each travel zone. These 350,000 segments by travel zone represent over 5 million people in the GMR, and thus involve using averages and simplifying assumptions to predict behaviour and access to the transport system.
- The STM does not currently apply a capacity constraint on public transport use. What this means is that in effect, each public transport vehicle is infinitely large. It is possible to identify where services are over capacity by dividing predicted demand by known supply. The BTS believes that the most likely response to congestion on public transport is a shift of travel time, not of mode, thus it stands by the STM's 2 or 3.5 hour peak estimates of travel demand by mode.
- Whilst the STM has been validated to ensure that it reproduces reasonable estimates of current travel behaviour, it has not been calibrated to match base year travel in this implementation.


## A1.7 Fitness for purpose

The STM is a strategic multi-modal modelling tool incorporating the latest population and employment forecasts. The STM has been successfully used to inform evidence-based policy development and decisionmaking in strategic, metropolitan scale land use and transport scenario modelling projects.

For specific projects, the STM results should be used as a starting point to produce estimates of overall demand in response to alternative land use and/or transport supply scenarios. However, the STM, due to its limitations as a strategic modelling tool, may need to be supplemented with more detailed analyses for project evaluation purposes.

## A2. BTS Light Commercial Vehicle forecasts - February 2014 release

## A2.1 Introduction

This report documents the methodology and output of the February 2014 Release Bureau of Transport Statistics (BTS) Light Commercial Vehicle Forecasts. The methodology and output of the February 2014 Release BTS Heavy Vehicle Forecasts are documented in a separate report.

For the purposes of these forecasts, Light Commercial Vehicles (LCVs) refer to Class 1 or 2 vehicles under the Austroads vehicle classification system, but excluding bicycles and motorcycles (see Figure A2.1). The base and forecast year trip estimates relate solely to usage of LCVs for load-bearing commercial activities and services. This includes direct movements of goods for commercial purposes ('Light Goods Vehicles'), and movements of goods which are used for commercial operations but are not themselves for sale e.g. tools of trade ('Service Vehicles'). Movements of an LCV for personal reasons are excluded, irrespective of whether goods or tools of trade are carried.

AUSTROADS Vehicle Classification System


Figure A2.1 Austroads Vehicle Classification System

## A2.2 Methodology

The BTS light commercial vehicle forecasts are produced from the Light Commercial Vehicle Model (LCVM). The LCVM produces base year and forecast estimates of LCV travel movements for the Sydney Greater Metropolitan Area (GMA) at travel zone level. For the February 2014 Release, the base year is changed from 2006 to 2011 and the forecasts are at five yearly intervals to 2046 (including 2006). The zonal system used is BTS's 2006 Travel Zones.

## A2.2.1 Trip Attraction

The methodology for estimating LCV movements is based on LCV attraction rates i.e. the rate of attraction of LCVs to (1) households and (2) businesses, measured by the number of employees. These attraction rates are applied to the number of households and amount of employment in each travel zone to obtain the total number of LCVs attracted to the zone i.e.

## LCV trips attracted to zone = Trips attracted to households in zone + Trips attracted to businesses in zone , where

Trips attracted to households in zone = the number of households in zone LCV attraction rate for households, and

Trips attracted to businesses in zone $=$ the amount of employment in zone LCV attraction rate for businesses

To estimate trip attractions for the February 2014 Release Light Commercial Vehicle Forecasts, the following household and employment forecasts were used:

- Household forecasts - the August 2012 Release BTS Population Forecasts (which includes household forecasts).
- Employment forecasts - the August 2012 Release BTS Employment Forecasts.

The attraction rates used were based on two BTS studies of LCV attraction rates: the Service Vehicle Attraction Rate study (SVAR, 1999) and the LCV Trip Attraction Rates study (LTAR, 2009). For households, a single household attraction rate was used. For businesses, there were separate attraction rates used for the categories 'Office', 'Industrial', 'Retail' and 'Hospitality', as the SVAR study had established that there were significantly different attraction rates for these broad categories. The linkage between ANZSIC industry classes and these categories is shown in Table A2.1 below.

Table A2.1 LCV Business Attraction Rate Categories

| ANZSIC Code | ANZSIC Description | LCV Attraction Rate Category |
| :--- | :--- | :--- |
| A | Agriculture, Forestry and Fishing | Industry |
| B | Mining | Industry |
| C | Manufacturing | Industry |
| D | Electricity, Gas, Water and Waste Services | Industry |
| E | Construction | Industry |
| F | Wholesale Trade | Industry |
| G | Retail Trade | Retail |
| H | Accommodation and Food Services | Hospitality |
| I | Transport, Postal and Warehousing | Industry |


| J | Information Media and Telecommunications | Office |
| :--- | :--- | :--- |
| K | Financial and Insurance Services | Office |
| L | Rental, Hiring and Real Estate Services | Office |
| M | Professional, Scientific and Technical Services | Office |
| N | Administrative and Support Services | Office |
| O | Public Administration and Safety | Office |
| P | Education and Training | Office |
| Q | Health Care and Social Assistance | Office |
| R | Arts and Recreation Services | Office |
| S | Other Services | Office |

The attraction rates used for the February 2014 Release forecasts are shown in Table A2.2 below.

Table A2.2: LCV Attraction Rates

| Rate | Value | Unit |
| :--- | :--- | :--- |
| Household Attraction Rate | 0.188 | Per household per weekday |
| Business Attraction Rate (Office) | 0.115 | Per employee per weekday |
| Business Attraction Rate (Industrial) | 0.237 | Per employee per weekday |
| Business Attraction Rate (Retail) | 0.319 | Per employee per weekday |
| Business Attraction Rate (Hospitality) | 0.177 | Per employee per weekday |
| Source: SVAR\&LTAR |  |  |

Once trip attractions are established, we apply a factor to allow for 'dead running'. A dead running trip is the 'away' trip from an initial trip made for commercial purposes. It most commonly refers to cases where freight is delivered to a location, and the freight carrying vehicle then returns empty to its original loading location. However, for consistency, BTS also applies the concept to light goods and service vehicle movements. If a plumber, say, travels to a household to do work, the subsequent trip away from the household is regarded as having been generated by the initial trip to the household.

It is important to understand that the dead running factor is not simply double the number of trips attracted to a household or business i.e. that it is not the case that for every trip attraction there is a concomitant away trip. The following example shows why this is so.

1


Figure A2.2 An example of LCV Vehicle tour
In this example, there are three trips. Our same plumber, say, travels from his base to do work at a household. He then travels to another household to do work, then travels back to base. There are thus two trips attracted to households for commercial purposes. If we were to apply the simple assumption that every trip attraction generated a concomitant away trip, we would estimate that four trips resulted from these two attractions, which is obviously wrong. This is because the 'away' trip from the first household (Trip 2) is actually an attraction to the second household, and to count it solely as an away trip can lead to doublecounting. Thus, for this example, the dead running factor is actually 0.5 i.e. the total number of trips $=$ total trip attractions (2) * $(1+0.5)=3$.

The actual dead running factor for LCVs used in the February 2014 Release was 0.5 . This was calculated by examining data from BTS's Household Travel Survey (HTS). The HTS provides detailed information on all trips made by a respondent in a day, and includes data from respondents driving LCVs for commercial purposes. As a result, it was possible to analyze the tour patterns for LCV drivers and quantify the average amount of dead running.

## A2.2.2 Trip production

To produce a zonal origin-destination matrix, it is necessary to estimate the number of trips produced (i.e. generated) from a zone in addition to estimating the number of trips attracted to the zone. Currently, BTS has no production rate data to complement its attraction rate data for LCVs. As a result, it used the assumption that within a 24 hour period the number of LCV trips produced from a zone is identical to the number attracted.

## A2.2.3 Trip distribution

Once LCV trip productions and attractions have been estimated for each travel zone, the movements between zones (i.e. the origin-destination matrix) are estimated using a gravity model. Unlike the BTS heavy vehicle origin-destination matrices, the LCV matrix is not adjusted by a matrix estimation process. Matrix estimation uses counts of vehicles on the road network to produce a 'maximum likelihood' estimation of vehicle movements based on observed data. For heavy vehicles, BTS has undertaken a number of classified count studies to obtain such counts for rigid and articulated trucks, and consequently is able to use matrix estimation to estimate its heavy vehicle origin-destination matrices. However, equivalent counts for LCVs are not available, and as a result the matrix estimation process cannot be applied to the LCV origin-destination matrices.

$$
T_{i j}=T_{i} \times \frac{A_{j} \times F F_{i j}}{\sum A_{j} \times F F_{i j}}
$$

Where:

$$
T_{i j}=T_{i} \times \frac{A_{j} \times F F_{i j}}{\sum A_{j} \times F F_{i j}}
$$

Friction factors are used to represent travel time or impedance in the gravity model, as follows:
$F F_{i j}=T T_{i j}{ }^{\alpha} \times \exp \left(\beta \times T T_{i j}\right)$

Where is the travel time between zone and, and and are calibrated parameters.

The trip distribution process was implemented in CUBE using travel times skimmed from standard Sydney Strategic Travel Model runs. A trip length distribution was used to perform friction factor calibration. In the absence of observed trip length data for LCVs, the average trip length and trip length distribution from HTS LCV analysis was used. The resulting parameters for the friction factor equation were:
$\alpha=-0.02$
$\beta=-0.148$


Figure A2.3 LCV Trip Distribution Comparisons in 5 Minutes Bin
Estimated versus observed plots are useful in determining if the parameters are set up properly. A high R2 indicates a good degree of fit. Figure 2.2 shows the trip length distribution from HTS versus LCVM in 5 minutes bin.

## A2.2.4 Time Period Estimation

The direct output from the LCV gravity model is LCV trips by origin zone and destination zone on an average weekday. Time period factors are then used to disaggregate average weekday trips to trips in individual time periods. These factors were derived from the LTAR (2009) study, where the time of each LCV trip attracted to a household or business was collected. The factors used are shown in Table 2.3 below.

Table A2.2 Time period factors used for the February 2010 Release LCV estimates

| Am Peak | Inter Peak | Pm Peak |  |
| :--- | :--- | :--- | :--- |
| 7.00am -9.00am | $9.00 \mathrm{am}-3.00 \mathrm{pm}$ | $3.00 \mathrm{pm}-6.00 \mathrm{pm}$ | $6.00 \mathrm{pm}-7.00 \mathrm{am}$ |
| 0.16 | 0.61 | 0.13 | 0.10 |

Source: LTAR, 2009

## A2.2.5 Sydney Airport

Sydney Airport is the largest LCV trip generator within Sydney GMA. BTS conducted a video camera study around the Sydney Airport Precinct over two consecutive weekdays in 2013. The study provides detailed classified traffic counts on Domestic and International Terminal access roads. There are more than 10,000 LCV trips to/from International and Domestic terminals daily in the study period. The projected future growth of airport LCV traffic is based on the reported airport passenger forecasts.

## A2.3 LCV Model Results

Table 3.1 compares 2011 LCV trip estimates from the BTS February 2014 Release with the earlier BTS release ('the BTS February 2010 Forecasts'). The comparisons show that a slightly higher number of trips in the current model relative to the old model. This can be largely attributed to more service employment in the 2010 land use forecast.

Table A2.3 Total LCV trips and Average Trip Length on Average Weekday, 2011

| 2011 | BTS February 2010 <br> Release estimates | BTS February 2014 <br> Release estimates | Difference |
| :--- | :--- | :--- | :--- |
| Total trips (Weekday) | $1,259,621$ | $1,301,791$ | $+3.3 \%$ |
| Average Trip Length (km) | $\mathbf{1 1}$ | $\mathbf{1 4}$ | $+27.3 \%$ |

The average trip length from the revised model estimates is calibrated against the trip length from HTS LCV analysis.

## A2.3.1 Comparison with external data

The VKT (Vehicle Kilometres Travelled) estimates associated with the February 2014 Release trip estimates for 2011 can be compared with the ABS Survey of Motor Vehicle Use (SMVU) VKT estimates released in 2012, as shown in Table A2.4 below.

Table A2.4 Total Business Kilometres Travelled by LCVs (Sydney SD)

|  | SMVU | BTS February 2010 <br> Release estimates | Difference |
| :--- | :--- | :--- | :--- |
| Annual VKT (million) | 4,344 | 3,677 | $-15 \%$ |

It is important to note that the figure of 4,344 million annual business VKT for the SMVU shown in Table 3.2 is a BTS estimate of what the SMVU data would be if it used the same definition of LCV trips as applied by BTS $^{1}$. However, this SMVU estimate only provides an indicative comparison with the BTS estimates, as it is not possible to directly compare SMVU and BTS estimates of VKT for LCVs, due to the factor that some trips are treated differently in the two data sets.

It should also be noted that ABS reports an increase of more than 40\% LCV annual business VKT from 2006 to 2011; whereas Road and Maritime Service's (RMS) vehicle registration data show that the registered LCVs for Sydney GMA increased around 8\% in the same time period. It should be noted that the SMVU estimates are subject to a Relative Standard Error (RSE) of 12.9\%. The vehicle registration data from RMS is considered to be more reliable.

## A2.3.2 Comparison with the Household Travel Survey (HTS)

The BTS Strategic Travel Model (STM) includes LCV trips in its estimate of total travel movements, where the LCV trip data is obtained from BTS's Household Travel Survey (HTS). While this HTS data for LCVs provides a wealth of detailed information for use in the STM, it does not necessarily reflect the true number of total LCV movements. This is because the HTS sample is household, not business, based, and the survey expansion variables that are applied are designed to optimize the accuracy of trips for personal, not business, reasons.

The number of business trips included in the STM is estimated by analysing 3-years (2009, 2010 and 2011) of pooled HTS data. Vehicles with the following body type are considered to be LCV:

- 4 Van / Pvan / Ute
- 41 Goods Van
- 42 Panel Van
- 43 Utility

A business trip is defined as a trip with the purpose of:

- Go to work
- Return to work
- Work related business

For the February 2014 Release LCV forecasts, BTS compared the 2011 base year LCV estimates with HTS estimates for the same year. This analysis showed that for 2011 the HTS captured $35 \%$ of total LCV movements. As a result, the LCV data from LCVM should be factored by $65 \%$ to take into account the overlapping when assign STM car demand and LCV demand together.

## A2.4 LCV Forecasts

The key inputs to BTS's forecasts of LCV movements are:

- Forecasts of households by travel zone.
- Forecasts of employment by industry group by travel zone.

[^1]The household and employment forecasts used for the February 2014 Release LCV Forecasts were the BTS August 2009 Release Population and Employment Forecasts, respectively.

The forecasts of LCV movements are produced by:

- -Calculating future zonal trip ends based on household and employment forecasts. Note: Both household and business LCV attraction rates are assumed to be constant in future years.
- Using the Fratar method to forecast (back-cast) future (2006) trip tables based on zonal growth factors and the base 2011 trip table.

Figure A2.4 shows the future growth of land use and the total number of LCVs. It can be seen that the growth is LCV is consistent with the land use growth.


Figure A2.4 LCV and Land Use Growth

## A2.5 Trip tables

Field names and descriptions for BTS's LCV trip tables for the February 2014 Release LCV forecasts are shown in Appendix 1.

## A2.6 References

Service Vehicle Attraction Rates (SVAR), consultancy report to the Transport Data Centre, 1999.
Final report for the light commercial vehicle trip attraction rates study for the Transport Data Centre (LTAR), consultancy report to the Transport Data Centre, 2009.

## A2.7 Appendix 1 BTS LCV trip table

| Field Name | Description |
| :---: | :---: |
| O_TZ06 | Origin 2006 Travel Zone |
| O_SLA06 | Origin 2006 SLA |
| O_LGA06 | Origin 2006 LGA |
| O_SSD06 | Origin 2006 SSD |
| O_SD06 | Origin 2006 SD |
| O_SUBREGION_METRO | Origin Metropolitan Strategy Subregion |
| D_TZ06 | Destination 2006 Travel zone |
| D_SLA06 | Destination 2006 SLA |
| D_LGA06 | Destination 2006 LGA |
| D_SSD06 | Destination 2006 SSD |
| D_SD06 | Destination 2006 SD |
| D_SUBREGION_METRO | Destination Metropolitan Strategy Subregion |
| ROAD_DISTANCE_KM | Road distance in km between O_TZ06 and D_TZ06 |
| TRIPS_2006_AMPEAK | The number of trips in 2006 AM Peak 2h |
| TRIPS_2006_INTERPEAK | The number of trips in 2006 Inter-Peak 2 h |
| TRIPS_2006_PMPEAK | The number of trips in 2006 PM Peak 2h |
| TRIPS_2006_EVENING | The number of trips in 2006 Night Time Period 2h |
| .. | $\ldots$ |
| TRIPS_2046_AMPEAK | The number of trips in 2046 AM Peak |
| TRIPS_2046_INTERPEAK | The number of trips in 2046 Inter-Peak |
| TRIPS_2046_PMPEAK | The number of trips in 2046 PM Peak |
| TRIPS_2046_EVENING | The number of trips in 2046 Night Time Period |
| O_TZ06_NAME | Origin 2006 Travel Zone name |
| O_SLA06_NAME | Origin 2006 SLA name |
| O_LGA06_NAME | Origin 2006 LGA name |
| O_SSD06_NAME | Origin 2006 SSD name |
| O_SD06_NAME | Origin 2006 SD name |
| O_SUBREGION_METRO_NAME | Origin Metropolitan Strategy Subregion name |
| D_TZ06_NAME | Destination 2006 Travel zone name |
| D_SLA06_NAME | Destination 2006 SLA name |
| D_LGA06_NAME | Destination 2006 LGA name |
| D_SSD06_NAME | Destination 2006 SSD name |
| D_SD06_NAME | Destination 2006 SD name |
| D_SUBREGION_METRO_NAME | Destination Metropolitan Strategy Subregion name |

## Appendix B

STM Network comparisons



## B1. Changes in the 2016 Network (from the 2011 network)



## B2. Changes in the 2021 network (from the 2016 network)



## B3. Changes to the 2026 network (from the 2021 network)



## B4. Changes to the 2031 network (from the2026 network)



## Appendix C

Deloitte Distribution Data (by LGA)


## C1. Deloitte distribution data

The distribution assumptions used in this assessment are based on information supplied by Deloitte to Parsons Brinckerhoff. The distribution data was supplied at the level of Local Government Areas (LGA) for the Sydney Greater Metropolitan Area. The data was supplied broken down into TEUS and truck level based on the Deloitte's analysis of loading factors and splits of loads to articulated and B-Double trucks as outlined in section 3.

This appendix details the supplied data as shown in Table C. 1 to C.9.

Table C1.1 Road distribution for 'Base Case’ scenario for Port Botany - Volume (TEUs)

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 374 | 391 | 432 | 443 | 439 | 445 | 448 | 448 | 507 | 569 | 633 | 701 | 771 | 1,179 | 1,705 |
| Auburn | 26,675 | 28,887 | 33,179 | 35,484 | 36,716 | 39,058 | 41,416 | 43,782 | 49,522 | 55,534 | 61,833 | 68,431 | 75,344 | 115,164 | 166,561 |
| Bankstown | 22,893 | 24,499 | 27,796 | 29,351 | 29,972 | 31,449 | 32,876 | 34,243 | 38,732 | 43,434 | 48,361 | 53,521 | 58,928 | 90,072 | 130,271 |
| Baulkham Hills | 67,523 | 71,832 | 76,392 | 81,215 | 86,317 | 91,714 | 97,422 | 103,459 | 108,508 | 113,795 | 119,334 | 125,136 | 131,213 | 166,214 | 210,362 |
| Blacktown | 445,030 | 479,002 | 515,176 | 553,685 | 594,667 | 638,271 | 684,654 | 733,979 | 769,792 | 807,305 | 846,599 | 887,758 | 930,871 | 1,179,182 | 1,492,389 |
| Botany Bay | 103,423 | 107,010 | 110,705 | 114,509 | 118,424 | 122,453 | 126,597 | 130,858 | 137,085 | 143,608 | 150,442 | 157,601 | 165,101 | 208,304 | 262,813 |
| Burwood | 5,352 | 5,645 | 6,307 | 6,552 | 6,573 | 6,769 | 6,934 | 7,066 | 7,992 | 8,962 | 9,979 | 11,044 | 12,159 | 18,586 | 26,881 |
| Camden | 21,929 | 25,971 | 30,290 | 34,902 | 39,826 | 45,083 | 50,695 | 56,682 | 61,831 | 67,180 | 72,740 | 78,525 | 84,549 | 118,742 | 161,193 |
| Campbelltown | 33,840 | 39,315 | 44,954 | 50,760 | 56,735 | 62,880 | 69,199 | 75,692 | 83,980 | 92,708 | 101,894 | 111,557 | 121,717 | 180,751 | 255,924 |
| Canada Bay | 1,420 | 1,497 | 1,672 | 1,737 | 1,742 | 1,793 | 1,837 | 1,871 | 2,117 | 2,374 | 2,643 | 2,925 | 3,220 | 4,922 | 7,119 |
| Canterbury | 3,811 | 4,013 | 4,475 | 4,639 | 4,645 | 4,771 | 4,875 | 4,954 | 5,603 | 6,284 | 6,996 | 7,743 | 8,525 | 13,031 | 18,846 |
| Fairfield | 110,466 | 120,008 | 130,081 | 140,712 | 151,932 | 163,770 | 176,260 | 189,436 | 201,355 | 213,845 | 226,934 | 240,651 | 255,024 | 337,881 | 442,504 |
| Holroyd | 68,825 | 72,872 | 77,014 | 81,249 | 85,576 | 89,995 | 94,504 | 99,102 | 106,612 | 114,486 | 122,739 | 131,390 | 140,457 | 192,753 | 258,827 |
| Hornsby | 16,955 | 17,781 | 19,741 | 20,366 | 20,282 | 20,713 | 21,026 | 21,211 | 23,991 | 26,904 | 29,955 | 33,152 | 36,501 | 55,792 | 80,692 |
| Hunters Hill | 340 | 352 | 384 | 390 | 380 | 380 | 376 | 369 | 417 | 468 | 521 | 576 | 634 | 970 | 1,403 |
| Hurstville | 2,442 | 2,577 | 2,879 | 2,992 | 3,002 | 3,093 | 3,169 | 3,231 | 3,654 | 4,098 | 4,563 | 5,050 | 5,560 | 8,498 | 12,290 |
| Kogarah | 1,431 | 1,454 | 1,506 | 1,519 | 1,510 | 1,513 | 1,509 | 1,499 | 1,617 | 1,742 | 1,872 | 2,008 | 2,151 | 2,973 | 4,025 |
| Ku-ring-gai | 471 | 505 | 573 | 605 | 619 | 650 | 680 | 709 | 802 | 899 | 1,001 | 1,108 | 1,220 | 1,865 | 2,697 |
| Lane Cove | 1,601 | 1,677 | 1,860 | 1,916 | 1,905 | 1,943 | 1,968 | 1,981 | 2,241 | 2,513 | 2,798 | 3,097 | 3,410 | 5,212 | 7,538 |
| Leichhardt | 1,095 | 1,173 | 1,334 | 1,411 | 1,443 | 1,518 | 1,590 | 1,660 | 1,877 | 2,105 | 2,344 | 2,594 | 2,856 | 4,365 | 6,314 |
| Liverpool | 155,660 | 161,727 | 167,986 | 174,441 | 181,098 | 187,963 | 195,042 | 202,341 | 212,214 | 222,556 | 233,388 | 244,735 | 256,620 | 325,074 | 411,418 |
| Manly | 220 | 212 | 202 | 191 | 178 | 164 | 148 | 129 | 136 | 142 | 149 | 156 | 163 | 206 | 260 |
| Marrickville | 9,813 | 10,100 | 5,977 | 6,250 | 10,975 | 11,191 | 11,385 | 11,553 | 12,467 | 13,424 | 14,426 | 15,476 | 16,576 | 22,914 | 26,509 |
| Mosman | 782 | 758 | 731 | 699 | 662 | 621 | 574 | 521 | 545 | 571 | 599 | 627 | 657 | 829 | 1,046 |
| North Sydney | 5,406 | 5,064 | 4,677 | 4,243 | 3,756 | 3,213 | 2,611 | 1,943 | 2,036 | 2,133 | 2,234 | 2,341 | 2,452 | 3,094 | 3,903 |
| Parramatta | 74,474 | 76,440 | 78,404 | 80,362 | 82,310 | 84,243 | 86,156 | 88,044 | 92,340 | 96,840 | 101,553 | 106,491 | 111,662 | 141,448 | 179,019 |
| Penrith | 278,077 | 299,354 | 322,012 | 346,134 | 371,808 | 399,125 | 428,185 | 459,091 | 481,492 | 504,955 | 529,532 | 555,277 | 582,244 | 737,557 | 933,463 |
| Pittwater | 1,095 | 1,144 | 1,264 | 1,298 | 1,286 | 1,305 | 1,316 | 1,318 | 1,490 | 1,671 | 1,861 | 2,059 | 2,267 | 3,466 | 5,012 |
| Randwick | 47,432 | 49,296 | 51,229 | 53,235 | 55,316 | 57,474 | 59,713 | 62,034 | 64,986 | 68,078 | 71,318 | 74,712 | 78,267 | 98,748 | 124,588 |
| Rockdale | 6,230 | 6,537 | 7,003 | 7,324 | 7,570 | 7,902 | 8,239 | 8,581 | 9,260 | 9,970 | 10,715 | 11,495 | 12,312 | 17,019 | 23,044 |
| Ryde | 2,928 | 2,944 | 3,114 | 3,037 | 2,832 | 2,675 | 2,469 | 2,211 | 2,501 | 2,805 | 3,123 | 3,456 | 3,806 | 5,817 | 8,413 |
| Strathfield | 8,895 | 9,580 | 10,943 | 11,637 | 11,970 | 12,657 | 13,338 | 14,010 | 15,846 | 17,770 | 19,785 | 21,897 | 24,109 | 36,851 | 53,297 |
| Sutherland Shire | 8,699 | 8,916 | 5,252 | 5,466 | 5,496 | 5,671 | 5,824 | 5,951 | 6,731 | 7,549 | 8,405 | 9,302 | 10,241 | 15,654 | 22,640 |
| Sydney | 26,461 | 27,279 | 28,687 | 29,429 | 29,806 | 30,459 | 31,058 | 31,595 | 34,093 | 36,710 | 39,451 | 42,323 | 45,332 | 62,663 | 84,844 |
| Warringah | 4,250 | 4,507 | 5,064 | 5,292 | 5,345 | 5,543 | 5,723 | 5,882 | 6,653 | 7,461 | 8,307 | 9,194 | 10,122 | 15,472 | 22,378 |
| Waverley | 502 | 487 | 469 | 447 | 423 | 396 | 365 | 330 | 346 | 362 | 379 | 397 | 416 | 525 | 663 |
| Willoughby | 5,934 | 5,974 | 6,005 | 6,026 | 6,034 | 6,030 | 6,012 | 5,978 | 6,263 | 6,561 | 6,873 | 7,200 | 7,543 | 9,517 | 12,007 |
| Woollahra | 1,925 | 1,857 | 1,778 | 1,688 | 1,585 | 1,469 | 1,337 | 1,190 | 1,247 | 1,306 | 1,368 | 1,433 | 1,502 | 1,895 | 2,390 |
| TOTAL | 1,574,677 | 1,678,638 | 1,787,546 | 1,901,636 | 2,021,156 | 2,146,363 | 2,277,528 | 2,414,936 | 2,558,881 | 2,709,677 | 2,867,648 | 3,033,137 | 3,206,501 | 4,205,204 | 5,465,247 |

Table C1.2 Road distribution for 'Project Case’ scenario for Port Botany - Volume (TEUs)

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 340 | 375 | 405 | 417 | 427 | 433 | 437 | 438 | 497 | 558 | 623 | 690 | 761 | 1,169 | 1,683 |
| Auburn | 21,464 | 21,404 | 20,461 | 18,141 | 15,312 | 11,962 | 13,887 | 16,451 | 20,299 | 24,541 | 29,180 | 34,222 | 39,672 | 73,387 | 119,073 |
| Bankstown | 20,797 | 23,532 | 26,084 | 27,642 | 29,165 | 30,646 | 32,077 | 33,448 | 37,937 | 42,639 | 47,566 | 52,727 | 58,133 | 89,277 | 128,571 |
| Baulkham Hills | 62,350 | 61,258 | 59,745 | 57,767 | 55,277 | 52,225 | 57,275 | 63,487 | 68,881 | 74,493 | 80,336 | 86,424 | 92,769 | 128,895 | 173,886 |
| Blacktown | 410,932 | 408,490 | 402,915 | 393,830 | 380,825 | 363,456 | 402,513 | 450,401 | 488,670 | 528,483 | 569,936 | 613,122 | 658,141 | 914,430 | 1,233,611 |
| Botany Bay | 103,423 | 107,010 | 110,705 | 114,509 | 118,424 | 122,453 | 126,597 | 130,858 | 137,085 | 143,608 | 150,442 | 157,601 | 165,101 | 208,304 | 262,813 |
| Burwood | 4,862 | 5,423 | 5,919 | 6,170 | 6,396 | 6,596 | 6,765 | 6,902 | 7,828 | 8,798 | 9,815 | 10,880 | 11,995 | 18,422 | 26,530 |
| Camden | 19,423 | 20,035 | 19,905 | 18,947 | 17,068 | 14,169 | 17,421 | 21,805 | 25,876 | 30,240 | 34,901 | 39,862 | 45,128 | 76,340 | 116,758 |
| Campbelltown | 29,973 | 30,329 | 29,542 | 27,556 | 24,315 | 19,762 | 23,780 | 29,118 | 35,145 | 41,732 | 48,889 | 56,629 | 64,967 | 116,206 | 185,375 |
| Canada Bay | 1,290 | 1,438 | 1,569 | 1,636 | 1,695 | 1,748 | 1,792 | 1,828 | 2,073 | 2,330 | 2,599 | 2,881 | 3,177 | 4,879 | 7,026 |
| Canterbury | 3,462 | 3,854 | 4,199 | 4,369 | 4,520 | 4,649 | 4,757 | 4,839 | 5,488 | 6,169 | 6,881 | 7,628 | 8,410 | 12,916 | 18,600 |
| Fairfield | 97,295 | 92,108 | 85,087 | 76,066 | 64,865 | 51,291 | 60,379 | 72,662 | 84,034 | 96,010 | 108,614 | 121,874 | 135,816 | 216,852 | 320,093 |
| Holroyd | 63,551 | 55,930 | 50,375 | 43,921 | 36,535 | 28,186 | 32,373 | 38,012 | 44,494 | 51,400 | 58,745 | 66,540 | 74,802 | 123,709 | 187,227 |
| Hornsby | 15,403 | 17,079 | 18,526 | 19,180 | 19,736 | 20,184 | 20,514 | 20,718 | 23,499 | 26,412 | 29,463 | 32,660 | 36,008 | 55,300 | 79,639 |
| Hunters Hill | 646 | 338 | 361 | 367 | 370 | 370 | 367 | 360 | 408 | 459 | 512 | 568 | 626 | 961 | 1,384 |
| Hurstville | 4,643 | 4,832 | 2,702 | 2,817 | 2,922 | 3,014 | 3,092 | 3,156 | 3,579 | 4,023 | 4,488 | 4,975 | 5,485 | 8,423 | 12,130 |
| Kogarah | 1,389 | 1,435 | 1,473 | 1,487 | 1,496 | 1,499 | 1,496 | 1,486 | 1,604 | 1,729 | 1,859 | 1,995 | 2,138 | 2,960 | 3,997 |
| Ku-ring-gai | 428 | 485 | 538 | 570 | 602 | 633 | 663 | 692 | 785 | 883 | 985 | 1,092 | 1,203 | 1,848 | 2,662 |
| Lane Cove | 3,044 | 3,145 | 1,746 | 1,805 | 1,854 | 1,893 | 1,920 | 1,935 | 2,195 | 2,467 | 2,752 | 3,051 | 3,364 | 5,166 | 7,440 |
| Leichhardt | 2,081 | 1,127 | 1,252 | 1,329 | 1,405 | 1,479 | 1,551 | 1,621 | 1,839 | 2,067 | 2,305 | 2,555 | 2,817 | 4,327 | 6,231 |
| Liverpool | 143,040 | 129,143 | 114,024 | 97,619 | 79,861 | 60,680 | 68,738 | 79,706 | 90,837 | 102,356 | 114,292 | 126,674 | 139,531 | 212,046 | 301,420 |
| Manly | 220 | 212 | 202 | 191 | 178 | 164 | 148 | 129 | 136 | 142 | 149 | 156 | 163 | 206 | 260 |
| Marrickville | 9,527 | 9,969 | 10,373 | 10,630 | 10,868 | 11,087 | 11,282 | 11,452 | 12,366 | 13,323 | 14,325 | 15,375 | 16,475 | 22,813 | 30,809 |
| Mosman | 782 | 758 | 731 | 699 | 662 | 621 | 574 | 521 | 545 | 571 | 599 | 627 | 657 | 829 | 1,046 |
| North Sydney | 5,406 | 5,064 | 4,677 | 4,243 | 3,756 | 3,213 | 2,611 | 1,943 | 2,036 | 2,133 | 2,234 | 2,341 | 2,452 | 3,094 | 3,903 |
| Parramatta | 68,768 | 65,188 | 61,319 | 57,160 | 52,711 | 47,971 | 50,652 | 54,028 | 58,618 | 63,394 | 68,366 | 73,547 | 78,947 | 109,690 | 147,977 |
| Penrith | 256,771 | 229,759 | 210,632 | 187,113 | 158,737 | 125,002 | 146,678 | 176,093 | 200,947 | 226,709 | 253,442 | 281,211 | 310,081 | 473,364 | 675,236 |
| Pittwater | 2,081 | 2,144 | 1,186 | 1,222 | 1,251 | 1,272 | 1,284 | 1,287 | 1,460 | 1,641 | 1,830 | 2,029 | 2,237 | 3,435 | 4,947 |
| Randwick | 47,432 | 49,296 | 51,229 | 53,235 | 55,316 | 57,474 | 59,713 | 62,034 | 64,986 | 68,078 | 71,318 | 74,712 | 78,267 | 98,748 | 124,588 |
| Rockdale | 6,048 | 6,452 | 6,851 | 7,171 | 7,497 | 7,828 | 8,165 | 8,506 | 9,185 | 9,895 | 10,640 | 11,420 | 12,237 | 16,944 | 22,883 |
| Ryde | 2,660 | 2,827 | 2,922 | 2,860 | 2,756 | 2,607 | 2,409 | 2,160 | 2,450 | 2,754 | 3,072 | 3,405 | 3,754 | 5,766 | 8,303 |
| Strathfield | 8,081 | 9,202 | 10,269 | 10,959 | 11,648 | 12,334 | 13,014 | 13,684 | 15,521 | 17,445 | 19,460 | 21,572 | 23,784 | 36,525 | 52,602 |
| Sutherland Shire | 8,445 | 8,800 | 9,115 | 9,296 | 9,455 | 9,590 | 9,700 | 9,781 | 10,561 | 11,378 | 12,234 | 13,131 | 14,071 | 19,484 | 26,313 |
| Sydney | 25,688 | 26,924 | 28,064 | 28,812 | 29,518 | 30,175 | 30,777 | 31,319 | 33,817 | 36,434 | 39,175 | 42,047 | 45,055 | 62,387 | 84,253 |
| Warringah | 8,080 | 4,329 | 4,752 | 4,984 | 5,201 | 5,402 | 5,584 | 5,746 | 6,517 | 7,325 | 8,171 | 9,057 | 9,986 | 15,336 | 22,086 |
| Waverley | 502 | 487 | 469 | 447 | 423 | 396 | 365 | 330 | 346 | 362 | 379 | 397 | 416 | 525 | 663 |
| Willoughby | 5,934 | 5,974 | 6,005 | 6,026 | 6,034 | 6,030 | 6,012 | 5,978 | 6,263 | 6,561 | 6,873 | 7,200 | 7,543 | 9,517 | 12,007 |
| Woollahra | 1,925 | 1,857 | 1,778 | 1,688 | 1,585 | 1,469 | 1,337 | 1,190 | 1,247 | 1,306 | 1,368 | 1,433 | 1,502 | 1,895 | 2,390 |
| TOTAL | 1,468,186 | 1,418,012 | 1,368,107 | 1,302,880 | 1,220,668 | 1,119,963 | 1,228,699 | 1,366,106 | 1,510,051 | 1,660,847 | 1,818,819 | 1,984,307 | 2,157,671 | 3,156,374 | 4,416,417 |

Table C1.3 Road distribution for 'Project Case’ scenario for Moorebank - Volume (TEUs)

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Auburn | 2,770 | 6,342 | 10,675 | 15,277 | 20,416 | 26,098 | 26,522 | 26,315 | 28,206 | 29,977 | 31,637 | 33,193 | 34,655 | 40,761 | 45,316 |
| Bankstown | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Baulkham Hills | 4,796 | 10,210 | 16,294 | 23,107 | 30,710 | 39,169 | 39,837 | 39,672 | 39,328 | 39,005 | 38,702 | 38,418 | 38,151 | 37,032 | 36,194 |
| Blacktown | 31,610 | 68,082 | 109,886 | 157,532 | 211,570 | 272,592 | 279,965 | 281,448 | 279,005 | 276,716 | 274,568 | 272,551 | 270,656 | 262,719 | 256,777 |
| Botany Bay | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Burwood | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Camden | 2,506 | 5,936 | 10,385 | 15,955 | 22,758 | 30,914 | 33,273 | 34,877 | 35,955 | 36,939 | 37,839 | 38,664 | 39,421 | 42,402 | 44,435 |
| Campbelltown | 3,867 | 8,986 | 15,413 | 23,205 | 32,420 | 43,118 | 45,419 | 46,574 | 48,835 | 50,976 | 53,005 | 54,928 | 56,750 | 64,545 | 70,548 |
| Canada Bay | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Canterbury | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Fairfield | 12,554 | 27,291 | 44,393 | 64,056 | 86,486 | 111,908 | 115,321 | 116,225 | 116,767 | 117,278 | 117,759 | 118,212 | 118,639 | 120,447 | 121,818 |
| Holroyd | 4,889 | 16,572 | 26,283 | 36,986 | 48,714 | 61,496 | 61,831 | 60,802 | 61,825 | 62,787 | 63,690 | 64,541 | 65,342 | 68,712 | 71,253 |
| Hornsby | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hunters Hill | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hurstville | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Kogarah | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ku-ring-gai | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Cove | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Leichhardt | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Liverpool | 18,457 | 38,265 | 59,491 | 82,206 | 106,482 | 132,393 | 131,285 | 127,491 | 126,220 | 125,030 | 123,914 | 122,867 | 121,885 | 117,777 | 114,711 |
| Manly | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Marrickville | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mosman | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| North Sydney | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parramatta | 5,290 | 10,865 | 16,723 | 22,864 | 29,284 | 35,978 | 35,231 | 33,761 | 33,468 | 33,193 | 32,936 | 32,694 | 32,466 | 31,514 | 30,802 |
| Penrith | 19,752 | 68,077 | 109,895 | 157,569 | 211,650 | 272,732 | 280,146 | 281,665 | 279,220 | 276,929 | 274,780 | 272,762 | 270,865 | 262,921 | 256,975 |
| Pittwater | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Randwick | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Rockdale | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ryde | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Strathfield | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sutherland Shire | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sydney | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Warringah | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Waverley | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Willoughby | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Woollahra | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 106,491 | 260,625 | 419,439 | 598,756 | 800,488 | 1,026,400 | 1,048,830 | 1,048,830 | 1,048,830 | 1,048,830 | 1,048,830 | 1,048,830 | 1,048,830 | 1,048,830 | 1,048,830 |

Table C1.4 Road distribution for 'Base Case' scenario for Port Botany - Semi truck movements per day - round trips

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.6 | 0.6 | 0.7 | 0.8 | 1.2 | 1.7 |
| Auburn | 26.5 | 28.7 | 33.0 | 35.3 | 36.5 | 38.9 | 41.2 | 43.6 | 49.3 | 55.2 | 61.5 | 68.1 | 74.9 | 114.6 | 165.7 |
| Bankstown | 22.8 | 24.4 | 27.6 | 29.2 | 29.8 | 31.3 | 32.7 | 34.1 | 38.5 | 43.2 | 48.1 | 53.2 | 58.6 | 89.6 | 129.6 |
| Baulkham Hills | 67.2 | 71.5 | 76.0 | 80.8 | 85.9 | 91.2 | 96.9 | 102.9 | 107.9 | 113.2 | 118.7 | 124.5 | 130.5 | 165.3 | 209.3 |
| Blacktown | 442.7 | 476.5 | 512.5 | 550.8 | 591.5 | 634.9 | 681.0 | 730.1 | 765.7 | 803.1 | 842.1 | 883.1 | 926.0 | 1,173.0 | 1,484.5 |
| Botany Bay | 102.9 | 106.4 | 110.1 | 113.9 | 117.8 | 121.8 | 125.9 | 130.2 | 136.4 | 142.9 | 149.6 | 156.8 | 164.2 | 207.2 | 261.4 |
| Burwood | 5.3 | 5.6 | 6.3 | 6.5 | 6.5 | 6.7 | 6.9 | 7.0 | 8.0 | 8.9 | 9.9 | 11.0 | 12.1 | 18.5 | 26.7 |
| Camden | 21.8 | 25.8 | 30.1 | 34.7 | 39.6 | 44.8 | 50.4 | 56.4 | 61.5 | 66.8 | 72.4 | 78.1 | 84.1 | 118.1 | 160.3 |
| Campbelltown | 33.7 | 39.1 | 44.7 | 50.5 | 56.4 | 62.5 | 68.8 | 75.3 | 83.5 | 92.2 | 101.4 | 111.0 | 121.1 | 179.8 | 254.6 |
| Canada Bay | 1.4 | 1.5 | 1.7 | 1.7 | 1.7 | 1.8 | 1.8 | 1.9 | 2.1 | 2.4 | 2.6 | 2.9 | 3.2 | 4.9 | 7.1 |
| Canterbury | 3.8 | 4.0 | 4.5 | 4.6 | 4.6 | 4.7 | 4.8 | 4.9 | 5.6 | 6.3 | 7.0 | 7.7 | 8.5 | 13.0 | 18.7 |
| Fairfield | 109.9 | 119.4 | 129.4 | 140.0 | 151.1 | 162.9 | 175.3 | 188.4 | 200.3 | 212.7 | 225.7 | 239.4 | 253.7 | 336.1 | 440.2 |
| Holroyd | 68.5 | 72.5 | 76.6 | 80.8 | 85.1 | 89.5 | 94.0 | 98.6 | 106.1 | 113.9 | 122.1 | 130.7 | 139.7 | 191.7 | 257.5 |
| Hornsby | 16.9 | 17.7 | 19.6 | 20.3 | 20.2 | 20.6 | 20.9 | 21.1 | 23.9 | 26.8 | 29.8 | 33.0 | 36.3 | 55.5 | 80.3 |
| Hunters Hill | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 0.6 | 0.6 | 1.0 | 1.4 |
| Hurstville | 2.4 | 2.6 | 2.9 | 3.0 | 3.0 | 3.1 | 3.2 | 3.2 | 3.6 | 4.1 | 4.5 | 5.0 | 5.5 | 8.5 | 12.2 |
| Kogarah | 1.4 | 1.4 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.6 | 1.7 | 1.9 | 2.0 | 2.1 | 3.0 | 4.0 |
| Ku-ring-gai | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.2 | 1.9 | 2.7 |
| Lane Cove | 1.6 | 1.7 | 1.9 | 1.9 | 1.9 | 1.9 | 2.0 | 2.0 | 2.2 | 2.5 | 2.8 | 3.1 | 3.4 | 5.2 | 7.5 |
| Leichhardt | 1.1 | 1.2 | 1.3 | 1.4 | 1.4 | 1.5 | 1.6 | 1.7 | 1.9 | 2.1 | 2.3 | 2.6 | 2.8 | 4.3 | 6.3 |
| Liverpool | 154.8 | 160.9 | 167.1 | 173.5 | 180.1 | 187.0 | 194.0 | 201.3 | 211.1 | 221.4 | 232.2 | 243.4 | 255.3 | 323.4 | 409.3 |
| Manly | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 | 0.3 |
| Marrickville | 9.8 | 10.0 | 5.9 | 6.2 | 10.9 | 11.1 | 11.3 | 11.5 | 12.4 | 13.4 | 14.4 | 15.4 | 16.5 | 22.8 | 26.4 |
| Mosman | 0.8 | 0.8 | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 1.0 |
| North Sydney | 5.4 | 5.0 | 4.7 | 4.2 | 3.7 | 3.2 | 2.6 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 3.1 | 3.9 |
| Parramatta | 74.1 | 76.0 | 78.0 | 79.9 | 81.9 | 83.8 | 85.7 | 87.6 | 91.9 | 96.3 | 101.0 | 105.9 | 111.1 | 140.7 | 178.1 |
| Penrith | 276.6 | 297.8 | 320.3 | 344.3 | 369.8 | 397.0 | 425.9 | 456.7 | 479.0 | 502.3 | 526.7 | 552.4 | 579.2 | 733.7 | 928.5 |
| Pittwater | 1.1 | 1.1 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.5 | 1.7 | 1.9 | 2.0 | 2.3 | 3.4 | 5.0 |
| Randwick | 47.2 | 49.0 | 51.0 | 53.0 | 55.0 | 57.2 | 59.4 | 61.7 | 64.6 | 67.7 | 70.9 | 74.3 | 77.9 | 98.2 | 123.9 |
| Rockdale | 6.2 | 6.5 | 7.0 | 7.3 | 7.5 | 7.9 | 8.2 | 8.5 | 9.2 | 9.9 | 10.7 | 11.4 | 12.2 | 16.9 | 22.9 |
| Ryde | 2.9 | 2.9 | 3.1 | 3.0 | 2.8 | 2.7 | 2.5 | 2.2 | 2.5 | 2.8 | 3.1 | 3.4 | 3.8 | 5.8 | 8.4 |
| Strathfield | 8.8 | 9.5 | 10.9 | 11.6 | 11.9 | 12.6 | 13.3 | 13.9 | 15.8 | 17.7 | 19.7 | 21.8 | 24.0 | 36.7 | 53.0 |
| Sutherland Shire | 8.7 | 8.9 | 5.2 | 5.4 | 5.5 | 5.6 | 5.8 | 5.9 | 6.7 | 7.5 | 8.4 | 9.3 | 10.2 | 15.6 | 22.5 |
| Sydney | 26.3 | 27.1 | 28.5 | 29.3 | 29.6 | 30.3 | 30.9 | 31.4 | 33.9 | 36.5 | 39.2 | 42.1 | 45.1 | 62.3 | 84.4 |
| Warringah | 4.2 | 4.5 | 5.0 | 5.3 | 5.3 | 5.5 | 5.7 | 5.9 | 6.6 | 7.4 | 8.3 | 9.1 | 10.1 | 15.4 | 22.3 |
| Waverley | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.7 |
| Willoughby | 5.9 | 5.9 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 5.9 | 6.2 | 6.5 | 6.8 | 7.2 | 7.5 | 9.5 | 11.9 |
| Woollahra | 1.9 | 1.8 | 1.8 | 1.7 | 1.6 | 1.5 | 1.3 | 1.2 | 1.2 | 1.3 | 1.4 | 1.4 | 1.5 | 1.9 | 2.4 |
| TOTAL | 1,566 | 1,670 | 1,778 | 1,892 | 2,011 | 2,135 | 2,266 | 2,402 | 2,545 | 2,695 | 2,853 | 3,017 | 3,190 | 4,183 | 5,436 |

Table C1.5 Road distribution for 'Base Case' scenario for Port Botany - B-Double truck movements per day - round trips

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 | 0.5 | 0.8 |
| Auburn | 11.8 | 12.8 | 14.7 | 15.7 | 16.2 | 17.3 | 18.3 | 19.4 | 21.9 | 24.6 | 27.3 | 30.3 | 33.3 | 50.9 | 73.6 |
| Bankstown | 10.1 | 10.8 | 12.3 | 13.0 | 13.3 | 13.9 | 14.5 | 15.1 | 17.1 | 19.2 | 21.4 | 23.7 | 26.1 | 39.8 | 57.6 |
| Baulkham Hills | 29.9 | 31.8 | 33.8 | 35.9 | 38.2 | 40.5 | 43.1 | 45.7 | 48.0 | 50.3 | 52.8 | 55.3 | 58.0 | 73.5 | 93.0 |
| Blacktown | 196.7 | 211.8 | 227.8 | 244.8 | 262.9 | 282.2 | 302.7 | 324.5 | 340.3 | 356.9 | 374.3 | 392.5 | 411.5 | 521.3 | 659.8 |
| Botany Bay | 45.7 | 47.3 | 48.9 | 50.6 | 52.4 | 54.1 | 56.0 | 57.9 | 60.6 | 63.5 | 66.5 | 69.7 | 73.0 | 92.1 | 116.2 |
| Burwood | 2.4 | 2.5 | 2.8 | 2.9 | 2.9 | 3.0 | 3.1 | 3.1 | 3.5 | 4.0 | 4.4 | 4.9 | 5.4 | 8.2 | 11.9 |
| Camden | 9.7 | 11.5 | 13.4 | 15.4 | 17.6 | 19.9 | 22.4 | 25.1 | 27.3 | 29.7 | 32.2 | 34.7 | 37.4 | 52.5 | 71.3 |
| Campbelltown | 15.0 | 17.4 | 19.9 | 22.4 | 25.1 | 27.8 | 30.6 | 33.5 | 37.1 | 41.0 | 45.0 | 49.3 | 53.8 | 79.9 | 113.1 |
| Canada Bay | 0.6 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 | 1.0 | 1.2 | 1.3 | 1.4 | 2.2 | 3.1 |
| Canterbury | 1.7 | 1.8 | 2.0 | 2.1 | 2.1 | 2.1 | 2.2 | 2.2 | 2.5 | 2.8 | 3.1 | 3.4 | 3.8 | 5.8 | 8.3 |
| Fairfield | 48.8 | 53.1 | 57.5 | 62.2 | 67.2 | 72.4 | 77.9 | 83.8 | 89.0 | 94.5 | 100.3 | 106.4 | 112.7 | 149.4 | 195.6 |
| Holroyd | 30.4 | 32.2 | 34.0 | 35.9 | 37.8 | 39.8 | 41.8 | 43.8 | 47.1 | 50.6 | 54.3 | 58.1 | 62.1 | 85.2 | 114.4 |
| Hornsby | 7.5 | 7.9 | 8.7 | 9.0 | 9.0 | 9.2 | 9.3 | 9.4 | 10.6 | 11.9 | 13.2 | 14.7 | 16.1 | 24.7 | 35.7 |
| Hunters Hill | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.4 | 0.6 |
| Hurstville | 1.1 | 1.1 | 1.3 | 1.3 | 1.3 | 1.4 | 1.4 | 1.4 | 1.6 | 1.8 | 2.0 | 2.2 | 2.5 | 3.8 | 5.4 |
| Kogarah | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 | 0.9 | 1.0 | 1.3 | 1.8 |
| Ku-ring-gai | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 0.8 | 1.2 |
| Lane Cove | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 | 1.0 | 1.1 | 1.2 | 1.4 | 1.5 | 2.3 | 3.3 |
| Leichhardt | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.3 | 1.9 | 2.8 |
| Liverpool | 68.8 | 71.5 | 74.3 | 77.1 | 80.1 | 83.1 | 86.2 | 89.5 | 93.8 | 98.4 | 103.2 | 108.2 | 113.5 | 143.7 | 181.9 |
| Manly | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Marrickville | 4.3 | 4.5 | 2.6 | 2.8 | 4.9 | 4.9 | 5.0 | 5.1 | 5.5 | 5.9 | 6.4 | 6.8 | 7.3 | 10.1 | 11.7 |
| Mosman | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.5 |
| North Sydney | 2.4 | 2.2 | 2.1 | 1.9 | 1.7 | 1.4 | 1.2 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 | 1.1 | 1.4 | 1.7 |
| Parramatta | 32.9 | 33.8 | 34.7 | 35.5 | 36.4 | 37.2 | 38.1 | 38.9 | 40.8 | 42.8 | 44.9 | 47.1 | 49.4 | 62.5 | 79.1 |
| Penrith | 122.9 | 132.3 | 142.4 | 153.0 | 164.4 | 176.5 | 189.3 | 203.0 | 212.9 | 223.2 | 234.1 | 245.5 | 257.4 | 326.1 | 412.7 |
| Pittwater | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 | 1.5 | 2.2 |
| Randwick | 21.0 | 21.8 | 22.6 | 23.5 | 24.5 | 25.4 | 26.4 | 27.4 | 28.7 | 30.1 | 31.5 | 33.0 | 34.6 | 43.7 | 55.1 |
| Rockdale | 2.8 | 2.9 | 3.1 | 3.2 | 3.3 | 3.5 | 3.6 | 3.8 | 4.1 | 4.4 | 4.7 | 5.1 | 5.4 | 7.5 | 10.2 |
| Ryde | 1.3 | 1.3 | 1.4 | 1.3 | 1.3 | 1.2 | 1.1 | 1.0 | 1.1 | 1.2 | 1.4 | 1.5 | 1.7 | 2.6 | 3.7 |
| Strathfield | 3.9 | 4.2 | 4.8 | 5.1 | 5.3 | 5.6 | 5.9 | 6.2 | 7.0 | 7.9 | 8.7 | 9.7 | 10.7 | 16.3 | 23.6 |
| Sutherland Shire | 3.8 | 3.9 | 2.3 | 2.4 | 2.4 | 2.5 | 2.6 | 2.6 | 3.0 | 3.3 | 3.7 | 4.1 | 4.5 | 6.9 | 10.0 |
| Sydney | 11.7 | 12.1 | 12.7 | 13.0 | 13.2 | 13.5 | 13.7 | 14.0 | 15.1 | 16.2 | 17.4 | 18.7 | 20.0 | 27.7 | 37.5 |
| Warringah | 1.9 | 2.0 | 2.2 | 2.3 | 2.4 | 2.5 | 2.5 | 2.6 | 2.9 | 3.3 | 3.7 | 4.1 | 4.5 | 6.8 | 9.9 |
| Waverley | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.1 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 |
| Willoughby | 2.6 | 2.6 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 | 2.6 | 2.8 | 2.9 | 3.0 | 3.2 | 3.3 | 4.2 | 5.3 |
| Woollahra | 0.9 | 0.8 | 0.8 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 1.1 |
| TOTAL | 696 | 742 | 790 | 841 | 894 | 949 | 1,007 | 1,068 | 1,131 | 1,198 | 1,268 | 1,341 | 1,418 | 1,859 | 2,416 |

Table C1.6 Road distribution for 'Project Case’ scenario for Port Botany - Semi Truck movements per day - round trips

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.6 | 0.6 | 0.7 | 0.8 | 1.2 | 1.7 |
| Auburn | 21.4 | 21.3 | 20.4 | 18.0 | 15.2 | 11.9 | 13.8 | 16.4 | 20.2 | 24.4 | 29.0 | 34.0 | 39.5 | 73.0 | 118.4 |
| Bankstown | 20.7 | 23.4 | 25.9 | 27.5 | 29.0 | 30.5 | 31.9 | 33.3 | 37.7 | 42.4 | 47.3 | 52.4 | 57.8 | 88.8 | 127.9 |
| Baulkham Hills | 62.0 | 60.9 | 59.4 | 57.5 | 55.0 | 52.0 | 57.0 | 63.2 | 68.5 | 74.1 | 79.9 | 86.0 | 92.3 | 128.2 | 173.0 |
| Blacktown | 408.8 | 406.3 | 400.8 | 391.8 | 378.8 | 361.5 | 400.4 | 448.0 | 486.1 | 525.7 | 566.9 | 609.9 | 654.7 | 909.6 | 1,227.1 |
| Botany Bay | 102.9 | 106.4 | 110.1 | 113.9 | 117.8 | 121.8 | 125.9 | 130.2 | 136.4 | 142.9 | 149.6 | 156.8 | 164.2 | 207.2 | 261.4 |
| Burwood | 4.8 | 5.4 | 5.9 | 6.1 | 6.4 | 6.6 | 6.7 | 6.9 | 7.8 | 8.8 | 9.8 | 10.8 | 11.9 | 18.3 | 26.4 |
| Camden | 19.3 | 19.9 | 19.8 | 18.8 | 17.0 | 14.1 | 17.3 | 21.7 | 25.7 | 30.1 | 34.7 | 39.7 | 44.9 | 75.9 | 116.1 |
| Campbelltown | 29.8 | 30.2 | 29.4 | 27.4 | 24.2 | 19.7 | 23.7 | 29.0 | 35.0 | 41.5 | 48.6 | 56.3 | 64.6 | 115.6 | 184.4 |
| Canada Bay | 1.3 | 1.4 | 1.6 | 1.6 | 1.7 | 1.7 | 1.8 | 1.8 | 2.1 | 2.3 | 2.6 | 2.9 | 3.2 | 4.9 | 7.0 |
| Canterbury | 3.4 | 3.8 | 4.2 | 4.3 | 4.5 | 4.6 | 4.7 | 4.8 | 5.5 | 6.1 | 6.8 | 7.6 | 8.4 | 12.8 | 18.5 |
| Fairfield | 96.8 | 91.6 | 84.6 | 75.7 | 64.5 | 51.0 | 60.1 | 72.3 | 83.6 | 95.5 | 108.0 | 121.2 | 135.1 | 215.7 | 318.4 |
| Holroyd | 63.2 | 55.6 | 50.1 | 43.7 | 36.3 | 28.0 | 32.2 | 37.8 | 44.3 | 51.1 | 58.4 | 66.2 | 74.4 | 123.1 | 186.2 |
| Hornsby | 15.3 | 17.0 | 18.4 | 19.1 | 19.6 | 20.1 | 20.4 | 20.6 | 23.4 | 26.3 | 29.3 | 32.5 | 35.8 | 55.0 | 79.2 |
| Hunters Hill | 0.6 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 0.6 | 0.6 | 1.0 | 1.4 |
| Hurstville | 4.6 | 4.8 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.1 | 3.6 | 4.0 | 4.5 | 4.9 | 5.5 | 8.4 | 12.1 |
| Kogarah | 1.4 | 1.4 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.6 | 1.7 | 1.8 | 2.0 | 2.1 | 2.9 | 4.0 |
| Ku-ring-gai | 0.4 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.2 | 1.8 | 2.6 |
| Lane Cove | 3.0 | 3.1 | 1.7 | 1.8 | 1.8 | 1.9 | 1.9 | 1.9 | 2.2 | 2.5 | 2.7 | 3.0 | 3.3 | 5.1 | 7.4 |
| Leichhardt | 2.1 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.5 | 1.6 | 1.8 | 2.1 | 2.3 | 2.5 | 2.8 | 4.3 | 6.2 |
| Liverpool | 142.3 | 128.5 | 113.4 | 97.1 | 79.4 | 60.4 | 68.4 | 79.3 | 90.4 | 101.8 | 113.7 | 126.0 | 138.8 | 210.9 | 299.8 |
| Manly | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 | 0.3 |
| Marrickville | 9.5 | 9.9 | 10.3 | 10.6 | 10.8 | 11.0 | 11.2 | 11.4 | 12.3 | 13.3 | 14.2 | 15.3 | 16.4 | 22.7 | 30.6 |
| Mosman | 0.8 | 0.8 | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 1.0 |
| North Sydney | 5.4 | 5.0 | 4.7 | 4.2 | 3.7 | 3.2 | 2.6 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 3.1 | 3.9 |
| Parramatta | 68.4 | 64.8 | 61.0 | 56.9 | 52.4 | 47.7 | 50.4 | 53.7 | 58.3 | 63.1 | 68.0 | 73.2 | 78.5 | 109.1 | 147.2 |
| Penrith | 255.4 | 228.5 | 209.5 | 186.1 | 157.9 | 124.3 | 145.9 | 175.2 | 199.9 | 225.5 | 252.1 | 279.7 | 308.4 | 470.9 | 671.7 |
| Pittwater | 2.1 | 2.1 | 1.2 | 1.2 | 1.2 | 1.3 | 1.3 | 1.3 | 1.5 | 1.6 | 1.8 | 2.0 | 2.2 | 3.4 | 4.9 |
| Randwick | 47.2 | 49.0 | 51.0 | 53.0 | 55.0 | 57.2 | 59.4 | 61.7 | 64.6 | 67.7 | 70.9 | 74.3 | 77.9 | 98.2 | 123.9 |
| Rockdale | 6.0 | 6.4 | 6.8 | 7.1 | 7.5 | 7.8 | 8.1 | 8.5 | 9.1 | 9.8 | 10.6 | 11.4 | 12.2 | 16.9 | 22.8 |
| Ryde | 2.6 | 2.8 | 2.9 | 2.8 | 2.7 | 2.6 | 2.4 | 2.1 | 2.4 | 2.7 | 3.1 | 3.4 | 3.7 | 5.7 | 8.3 |
| Strathfield | 8.0 | 9.2 | 10.2 | 10.9 | 11.6 | 12.3 | 12.9 | 13.6 | 15.4 | 17.4 | 19.4 | 21.5 | 23.7 | 36.3 | 52.3 |
| Sutherland Shire | 8.4 | 8.8 | 9.1 | 9.2 | 9.4 | 9.5 | 9.6 | 9.7 | 10.5 | 11.3 | 12.2 | 13.1 | 14.0 | 19.4 | 26.2 |
| Sydney | 25.6 | 26.8 | 27.9 | 28.7 | 29.4 | 30.0 | 30.6 | 31.2 | 33.6 | 36.2 | 39.0 | 41.8 | 44.8 | 62.1 | 83.8 |
| Warringah | 8.0 | 4.3 | 4.7 | 5.0 | 5.2 | 5.4 | 5.6 | 5.7 | 6.5 | 7.3 | 8.1 | 9.0 | 9.9 | 15.3 | 22.0 |
| Waverley | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.7 |
| Willoughby | 5.9 | 5.9 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 5.9 | 6.2 | 6.5 | 6.8 | 7.2 | 7.5 | 9.5 | 11.9 |
| Woollahra | 1.9 | 1.8 | 1.8 | 1.7 | 1.6 | 1.5 | 1.3 | 1.2 | 1.2 | 1.3 | 1.4 | 1.4 | 1.5 | 1.9 | 2.4 |
| TOTAL | 1,460 | 1,411 | 1,361 | 1,296 | 1,214 | 1,114 | 1,222 | 1,359 | 1,502 | 1,652 | 1,809 | 1,974 | 2,146 | 3,140 | 4,393 |

Table C1.7 Road distribution for 'Project Case' scenario for Port Botany - B-Double truck movements per day - round trips

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.5 | 0.7 |
| Auburn | 9.5 | 9.5 | 9.0 | 8.0 | 6.8 | 5.3 | 6.1 | 7.3 | 9.0 | 10.8 | 12.9 | 15.1 | 17.5 | 32.4 | 52.6 |
| Bankstown | 9.2 | 10.4 | 11.5 | 12.2 | 12.9 | 13.5 | 14.2 | 14.8 | 16.8 | 18.9 | 21.0 | 23.3 | 25.7 | 39.5 | 56.8 |
| Baulkham Hills | 27.6 | 27.1 | 26.4 | 25.5 | 24.4 | 23.1 | 25.3 | 28.1 | 30.5 | 32.9 | 35.5 | 38.2 | 41.0 | 57.0 | 76.9 |
| Blacktown | 181.7 | 180.6 | 178.1 | 174.1 | 168.4 | 160.7 | 178.0 | 199.1 | 216.0 | 233.6 | 252.0 | 271.1 | 291.0 | 404.3 | 545.4 |
| Botany Bay | 45.7 | 47.3 | 48.9 | 50.6 | 52.4 | 54.1 | 56.0 | 57.9 | 60.6 | 63.5 | 66.5 | 69.7 | 73.0 | 92.1 | 116.2 |
| Burwood | 2.1 | 2.4 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.5 | 3.9 | 4.3 | 4.8 | 5.3 | 8.1 | 11.7 |
| Camden | 8.6 | 8.9 | 8.8 | 8.4 | 7.5 | 6.3 | 7.7 | 9.6 | 11.4 | 13.4 | 15.4 | 17.6 | 20.0 | 33.8 | 51.6 |
| Campbelltown | 13.3 | 13.4 | 13.1 | 12.2 | 10.7 | 8.7 | 10.5 | 12.9 | 15.5 | 18.4 | 21.6 | 25.0 | 28.7 | 51.4 | 82.0 |
| Canada Bay | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 | 0.9 | 1.0 | 1.1 | 1.3 | 1.4 | 2.2 | 3.1 |
| Canterbury | 1.5 | 1.7 | 1.9 | 1.9 | 2.0 | 2.1 | 2.1 | 2.1 | 2.4 | 2.7 | 3.0 | 3.4 | 3.7 | 5.7 | 8.2 |
| Fairfield | 43.0 | 40.7 | 37.6 | 33.6 | 28.7 | 22.7 | 26.7 | 32.1 | 37.2 | 42.4 | 48.0 | 53.9 | 60.0 | 95.9 | 141.5 |
| Holroyd | 28.1 | 24.7 | 22.3 | 19.4 | 16.2 | 12.5 | 14.3 | 16.8 | 19.7 | 22.7 | 26.0 | 29.4 | 33.1 | 54.7 | 82.8 |
| Hornsby | 6.8 | 7.6 | 8.2 | 8.5 | 8.7 | 8.9 | 9.1 | 9.2 | 10.4 | 11.7 | 13.0 | 14.4 | 15.9 | 24.4 | 35.2 |
| Hunters Hill | 0.3 | 0.1 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.4 | 0.6 |
| Hurstville | 2.1 | 2.1 | 1.2 | 1.2 | 1.3 | 1.3 | 1.4 | 1.4 | 1.6 | 1.8 | 2.0 | 2.2 | 2.4 | 3.7 | 5.4 |
| Kogarah | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 | 0.9 | 0.9 | 1.3 | 1.8 |
| Ku-ring-gai | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.5 | 0.8 | 1.2 |
| Lane Cove | 1.3 | 1.4 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 | 1.0 | 1.1 | 1.2 | 1.3 | 1.5 | 2.3 | 3.3 |
| Leichhardt | 0.9 | 0.5 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.2 | 1.9 | 2.8 |
| Liverpool | 63.2 | 57.1 | 50.4 | 43.2 | 35.3 | 26.8 | 30.4 | 35.2 | 40.2 | 45.3 | 50.5 | 56.0 | 61.7 | 93.7 | 133.3 |
| Manly | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Marrickville | 4.2 | 4.4 | 4.6 | 4.7 | 4.8 | 4.9 | 5.0 | 5.1 | 5.5 | 5.9 | 6.3 | 6.8 | 7.3 | 10.1 | 13.6 |
| Mosman | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.5 |
| North Sydney | 2.4 | 2.2 | 2.1 | 1.9 | 1.7 | 1.4 | 1.2 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 | 1.1 | 1.4 | 1.7 |
| Parramatta | 30.4 | 28.8 | 27.1 | 25.3 | 23.3 | 21.2 | 22.4 | 23.9 | 25.9 | 28.0 | 30.2 | 32.5 | 34.9 | 48.5 | 65.4 |
| Penrith | 113.5 | 101.6 | 93.1 | 82.7 | 70.2 | 55.3 | 64.8 | 77.9 | 88.8 | 100.2 | 112.0 | 124.3 | 137.1 | 209.3 | 298.5 |
| Pittwater | 0.9 | 0.9 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.5 | 2.2 |
| Randwick | 21.0 | 21.8 | 22.6 | 23.5 | 24.5 | 25.4 | 26.4 | 27.4 | 28.7 | 30.1 | 31.5 | 33.0 | 34.6 | 43.7 | 55.1 |
| Rockdale | 2.7 | 2.9 | 3.0 | 3.2 | 3.3 | 3.5 | 3.6 | 3.8 | 4.1 | 4.4 | 4.7 | 5.0 | 5.4 | 7.5 | 10.1 |
| Ryde | 1.2 | 1.2 | 1.3 | 1.3 | 1.2 | 1.2 | 1.1 | 1.0 | 1.1 | 1.2 | 1.4 | 1.5 | 1.7 | 2.5 | 3.7 |
| Strathfield | 3.6 | 4.1 | 4.5 | 4.8 | 5.1 | 5.5 | 5.8 | 6.0 | 6.9 | 7.7 | 8.6 | 9.5 | 10.5 | 16.1 | 23.3 |
| Sutherland Shire | 3.7 | 3.9 | 4.0 | 4.1 | 4.2 | 4.2 | 4.3 | 4.3 | 4.7 | 5.0 | 5.4 | 5.8 | 6.2 | 8.6 | 11.6 |
| Sydney | 11.4 | 11.9 | 12.4 | 12.7 | 13.0 | 13.3 | 13.6 | 13.8 | 15.0 | 16.1 | 17.3 | 18.6 | 19.9 | 27.6 | 37.2 |
| Warringah | 3.6 | 1.9 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.5 | 2.9 | 3.2 | 3.6 | 4.0 | 4.4 | 6.8 | 9.8 |
| Waverley | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.1 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 |
| Willoughby | 2.6 | 2.6 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 | 2.6 | 2.8 | 2.9 | 3.0 | 3.2 | 3.3 | 4.2 | 5.3 |
| Woollahra | 0.9 | 0.8 | 0.8 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | 1.1 |
| TOTAL | 649 | 627 | 605 | 576 | 540 | 495 | 543 | 604 | 668 | 734 | 804 | 877 | 954 | 1,395 | 1,953 |

Table C1.8 Road distribution for 'Project Case’ scenario for Moorebank - Semi Truck movements per day - round trips

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Auburn | 3.3 | 7.5 | 12.7 | 18.2 | 24.3 | 31.0 | 31.6 | 31.3 | 33.6 | 35.7 | 37.6 | 39.5 | 41.2 | 48.5 | 53.9 |
| Bankstown | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Baulkham Hills | 5.7 | 12.1 | 19.4 | 27.5 | 36.5 | 46.6 | 47.4 | 47.2 | 46.8 | 46.4 | 46.0 | 45.7 | 45.4 | 44.1 | 43.1 |
| Blacktown | 37.6 | 81.0 | 130.7 | 187.4 | 251.7 | 324.3 | 333.0 | 334.8 | 331.9 | 329.2 | 326.6 | 324.2 | 322.0 | 312.5 | 305.5 |
| Botany Bay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Burwood | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Camden | 3.0 | 7.1 | 12.4 | 19.0 | 27.1 | 36.8 | 39.6 | 41.5 | 42.8 | 43.9 | 45.0 | 46.0 | 46.9 | 50.4 | 52.9 |
| Campbelltown | 4.6 | 10.7 | 18.3 | 27.6 | 38.6 | 51.3 | 54.0 | 55.4 | 58.1 | 60.6 | 63.1 | 65.3 | 67.5 | 76.8 | 83.9 |
| Canada Bay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Canterbury | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Fairfield | 14.9 | 32.5 | 52.8 | 76.2 | 102.9 | 133.1 | 137.2 | 138.3 | 138.9 | 139.5 | 140.1 | 140.6 | 141.1 | 143.3 | 144.9 |
| Holroyd | 5.8 | 19.7 | 31.3 | 44.0 | 57.9 | 73.2 | 73.6 | 72.3 | 73.5 | 74.7 | 75.8 | 76.8 | 77.7 | 81.7 | 84.8 |
| Hornsby | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Hunters Hill | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Hurstville | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Kogarah | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ku-ring-gai | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Lane Cove | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Leichhardt | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Liverpool | 22.0 | 45.5 | 70.8 | 97.8 | 126.7 | 157.5 | 156.2 | 151.7 | 150.1 | 148.7 | 147.4 | 146.2 | 145.0 | 140.1 | 136.5 |
| Manly | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Marrickville | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Mosman | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| North Sydney | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Parramatta | 6.3 | 12.9 | 19.9 | 27.2 | 34.8 | 42.8 | 41.9 | 40.2 | 39.8 | 39.5 | 39.2 | 38.9 | 38.6 | 37.5 | 36.6 |
| Penrith | 23.5 | 81.0 | 130.7 | 187.4 | 251.8 | 324.4 | 333.3 | 335.1 | 332.2 | 329.4 | 326.9 | 324.5 | 322.2 | 312.8 | 305.7 |
| Pittwater | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Randwick | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Rockdale | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ryde | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Strathfield | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sutherland Shire | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sydney | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Warringah | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Waverley | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Willoughby | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Woollahra | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TOTAL | 127 | 310 | 499 | 712 | 952 | 1,221 | 1,248 | 1,248 | 1,248 | 1,248 | 1,248 | 1,248 | 1,248 | 1,248 | 1,248 |

Table C1.9 Road distribution for 'Project Case’ scenario for Moorebank - B-Double truck movements per day - round trips

| LGA | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2035 | 2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ashfield | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Auburn | 0.5 | 1.3 | 2.1 | 3.0 | 4.0 | 5.2 | 5.3 | 5.2 | 5.6 | 5.9 | 6.3 | 6.6 | 6.9 | 8.1 | 9.0 |
| Bankstown | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Baulkham Hills | 1.0 | 2.0 | 3.2 | 4.6 | 6.1 | 7.8 | 7.9 | 7.9 | 7.8 | 7.7 | 7.7 | 7.6 | 7.6 | 7.3 | 7.2 |
| Blacktown | 6.3 | 13.5 | 21.8 | 31.2 | 41.9 | 54.0 | 55.5 | 55.8 | 55.3 | 54.9 | 54.4 | 54.0 | 53.7 | 52.1 | 50.9 |
| Botany Bay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Burwood | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Camden | 0.5 | 1.2 | 2.1 | 3.2 | 4.5 | 6.1 | 6.6 | 6.9 | 7.1 | 7.3 | 7.5 | 7.7 | 7.8 | 8.4 | 8.8 |
| Campbelltown | 0.8 | 1.8 | 3.1 | 4.6 | 6.4 | 8.5 | 9.0 | 9.2 | 9.7 | 10.1 | 10.5 | 10.9 | 11.3 | 12.8 | 14.0 |
| Canada Bay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Canterbury | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Fairfield | 2.5 | 5.4 | 8.8 | 12.7 | 17.1 | 22.2 | 22.9 | 23.0 | 23.2 | 23.3 | 23.3 | 23.4 | 23.5 | 23.9 | 24.2 |
| Holroyd | 1.0 | 3.3 | 5.2 | 7.3 | 9.7 | 12.2 | 12.3 | 12.1 | 12.3 | 12.4 | 12.6 | 12.8 | 13.0 | 13.6 | 14.1 |
| Hornsby | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Hunters Hill | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Hurstville | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Kogarah | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ku-ring-gai | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Lane Cove | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Leichhardt | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Liverpool | 3.7 | 7.6 | 11.8 | 16.3 | 21.1 | 26.2 | 26.0 | 25.3 | 25.0 | 24.8 | 24.6 | 24.4 | 24.2 | 23.4 | 22.7 |
| Manly | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Marrickville | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Mosman | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| North Sydney | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Parramatta | 1.0 | 2.2 | 3.3 | 4.5 | 5.8 | 7.1 | 7.0 | 6.7 | 6.6 | 6.6 | 6.5 | 6.5 | 6.4 | 6.2 | 6.1 |
| Penrith | 3.9 | 13.5 | 21.8 | 31.2 | 42.0 | 54.1 | 55.5 | 55.8 | 55.4 | 54.9 | 54.5 | 54.1 | 53.7 | 52.1 | 50.9 |
| Pittwater | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Randwick | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Rockdale | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ryde | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Strathfield | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sutherland Shire | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sydney | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Warringah | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Waverley | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Willoughby | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Woollahra | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TOTAL | 21 | 52 | 83 | 119 | 159 | 203 | 208 | 208 | 208 | 208 | 208 | 208 | 208 | 208 | 208 |

## Appendix D

Deloitte Distribution Data (by Postcode)


## D1. Allocation by postcode

Table D1.1 Percentage allocation by postcode (for 6 of the LGA's with the greatest volume of traffic tolfrom Moorebank)

| LGA | Postcode | Percentage of LGA volume | LGA | Postcode | Percentage of LGA volume |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Penrith | 2759 | 76.2\% | Fairfield | 2169 | 48.1\% |
|  | 2750 | 13.7\% |  | 2165 | 16.3\% |
|  | 2760 | 9.3\% |  | 2161 | 13.6\% |
|  | 2178 | 0.3\% |  | 2166 | 8.7\% |
|  | 2747 | 0.2\% |  | 2163 | 7.3\% |
|  | 2749 | 0.1\% |  | 2175 | 5.5\% |
| Blacktown | 2766 | 42.8\% |  | 2177 | 0.2\% |
|  | 2148 | 24.7\% | Campbelltown | 2566 | 52.5\% |
|  | 2147 | 11.0\% |  | 2565 | 44.5\% |
|  | 2770 | 9.2\% |  | 2560 | 3.3\% |
|  | 2761 | 6.4\% | Camden | 2567 | 99.2\% |
|  | 2760 | 3.6\% |  | 2570 | 0.4\% |
|  | 2765 | 2.0\% |  | 2179 | 0.3\% |
| Liverpool | 2170 | 75.6\% |  | 2557 | 0.1\% |
|  | 2173 | 20.2\% |  |  |  |
|  | 2171 | 3.6\% |  |  |  |
|  | 2178 | 0.2\% |  |  |  |
|  | 2556 | 0.1\% |  |  |  |
|  | 2179 | 0.1\% |  |  |  |

## Appendix E

Change in articulated truck volumes on key corridors



Figure D1.1 Change in articulated vehicle flows to/from Port Botany and Moorebank on the M5 between Sydney Airport and Hume Highway


Figure D1.2 Change in articulated vehicle flows tolfrom Port Botany and Moorebank on the M5 between Hume Highway and Narellan Road


Figure D1.3 Change in articulated vehicle flows tolfrom Port Botany and Moorebank on the M7 between the M5 and M4


Figure D1.4 Change in articulated vehicle flows tolfrom Port Botany and Moorebank on General Holmes Drive between Botany Road and The Grand Parade


Figure D1.5 Change in articulated vehicle flows tolfrom Port Botany and Moorebank on Foreshore Road/Botany Road between Southern Cross Road and
Bumborah Point Road


Figure D1.6 Change in articulated vehicle flows tolfrom Port Botany and Moorebank on the M2 between Delhi Road and Abbott Road


Figure D1.7 Change in articulated vehicle flows tolfrom Port Botany and Moorebank on Pennant Hills Road/Cumberland Highway between James Ruse Drive and the M1


Figure D1.8 Change in articulated vehicle flows tolfrom Port Botany and Moorebank on the M1 north of Cumberland Highway


Figure D1.9 Change in articulated vehicle flows to/from Port Botany and Moorebank on the Hume HighwaylCumberland between the M5 and the M4

## Appendix F

Change in speed



Figure D1.1
Change in speed, 2031 AM Peak ('Project Case’ versus 'Base Case')


Figure D1.2 Change in speed, 2031 inter-peak period ('Project Case’ versus 'Base Case')


Figure D1.3
Change in speed, 2031 PM peak ('Project Case versus ‘Base Case')


Figure D1.4
Change in speed, 2031 night time period ('Project Case versus 'Base Case')

## Appendix K

Deloitte EIS - Supporting
Information

## Deloitte.

# Moorebank Intermodal Company <br> EIS - Supporting Information <br> 18 September 2014 

## FINAL



## Liability limited by a scheme approved under Professional Standards Legislation.

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## Glossary

| Acronym | Description |
| :---: | :---: |
| \$ | Australian dollars unless stated otherwise |
| " ' or ft | Foot, a unit of length |
| ACBPS | Australian Customs and Border Protection Services |
| ACFS | Australian Container Freight Services |
| ARTC | Australian Rail Track Corporation Ltd |
| BITRE | Bureau of Infrastructure, Transport and Regional Economics |
| BTS | NSW Bureau of Transport Statistics |
| BWSGA | Broader Western Sydney Growth Area |
| DAE | Deloitte Access Economics, a team within Deloitte Touche Tohmatsu |
| DC | Distribution centre |
| ECP | Empty container park |
| FAK | Freight of all kinds |
| FCL | Full container load |
| FEU | Forty-foot equivalent unit, a measure used for capacity in container transportation |
| GDP | Gross domestic product |
| GSP | Gross state product |
| Ha | Hectare, a metric unit of area |
| IMEX | Import-export |
| IMT | Intermodal terminal |
| LCL | Less than container load |
| LGA | Local government areas |
| m | Metres, a metric unit of length |
| MIC | Moorebank Intermodal Company Ltd |
| NSW | New South Wales |


| Acronym | Description |
| :--- | :--- |
| PBLIS | Port Botany Landside Improvement Strategy |
| Pick and <br> Pack | Part of a complete supply chain management process commonly used in the <br> distribution of retail goods. It involves processing quantities of product <br> delivered by truck or train by picking relevant products for each final <br> destination (e.g. retail outlet) and re-packaging them for delivery. |
| PUD | Pickup and delivery |
| SPC | Sydney Ports Corporation |
| sq m | Square metre, a metric unit of area |
| SSFL | Southern Sydney Freight Line |
| Stack run | Stack runs are where the transport operator runs containers to its depot at night <br> and progressively distributes containers to customers over the following one to <br> three days. This generally improves delivery reliability and has been adopted as <br> standard practice by a number of large transport operators servicing the port |
| SWGC | South West Growth Centre |
| TEU | Twenty-foot equivalent unit, a measure used for capacity in container <br> transportation |

## 1 Introduction

The purpose of this document is to consolidate the various technical notes that have been developed and / or provided to supplement existing reports and data prepared by Deloitte. The technical notes were prepared, in order to inform, in the first instance, the preparation of the Moorebank Intermodal Terminal (Moorebank IMT) Environmental Impact Statement (EIS).

The contents of this document arise from direct requests for additional information or clarification from MIC. The focus of the technical notes has generally been to set out the approach or detailed methodology behind the assumptions and data that have used from reports that Deloitte has prepared and submitted to Moorebank Intermodal Company (MIC).
The document is therefore not a standalone document, nor is it a complete set of detailed explanations behind all of the assumptions and data provided throughout the project.

## 2 Port Botany forecasts

Market growth expectations for container volumes through Port Botany in the original Detailed Business Case (DBC) were based on forecasts developed by Sydney Ports Corporation (SPC). These forecasts were developed according to number of growth scenarios for containerised freight movements, ranging from a low growth scenario of $4.8 \%$, to a high growth scenario of $7.2 \%$. A "likely" (or medium) growth rate SPC developed of $6.7 \%$, which resulted in a forecasted Port volume of approximately 7 million TEU by 2030-31, was adopted in the analysis.
The extent to which these high growth rates could be maintained has been a much discussed subject within the freight industry. On the one hand, there was a view that structural changes within the economy that led to high levels of imports would reach an equilibrium state and growth rates would decline to levels more closely aligned with economic growth. Other views suggested that the high reliance on imports would continue into the foreseeable future as shipping rates remained low and supply chain efficiency improved, thereby allowing an everincreasing range of products to be transported to Australia from overseas' markets.

With these issues in mind, the Port Botany throughput revised forecast from the 2013 NSW Draft Freight Strategy was used, with the Port's volumes growing to 4.9 million TEU by 2030, implying an annual growth rate of around $4.8 \%$. As part of an update to Moorebank demand in December 2013, a high level analysis of the relationship between Gross State Product (GSP) and Port throughput indicated that the scenario outlined above be considered adequate given future GSP growth.
It is noted that since this analysis, Transport for NSW released the final NSW Freight and Ports Strategy. In their assessment of the future freight task, they maintained a reduced growth demand forecast at 4.9 million TEU by 2030 and provided an updated expected forecast of 7.0 million TEU by 2030 as outlined in the figure overleaf. The demand forecasts in the 2013 Moorebank Demand Update have been based on 4.9 million TEU throughput which is consistent with the more conservative reduced growth forecast.

Finally, the scope of demand analysis covered the Sydney Greater Metropolitan Area (GMA) which accounts for around $93 \%$ of all container import movements ${ }^{1}$ and $75 \%$ of all container export movements ${ }^{2}$ bringing the container landside freight task to just less than 4 million TEU by 2030-31 for the Sydney GMA.

Figure 1 : NSW container volume forecasts 2020-2040 (Transport for NSW) ${ }^{3}$


Source: NSW Freight and Ports Strategy 2013

## 3 Spatial Distribution

### 3.1 Updated Data Sets

Demand estimates for Moorebank IMT in the EIS are underpinned by postcode level import data provided by the Australian Customs and Border Protection Service (ACBPS).

The initial demand data sets developed for the Moorebank IMT development were derived utilising data sourced from ACBPS in 2011. Following this work, MIC engaged Deloitte to obtain new container data from ACBPS and subsequently update the demand analysis. ACBPS was able to provide more comprehensive data for movements since 2010. The new data set provided in September 2013 includes the following additional information:

- Export data with cargo owner and freight forwarder post code
- Cargo type (for exports)
- Full data sets for import and export containers for financial years 2009 to 2013.

With the new data provided, Deloitte was able to derive a more precise picture of container origins and destinations for the Sydney metropolitan area - in particular, the change of actual container distribution between 2010 and 2013. While ACBPS data provided a current picture

[^2]of container distribution in Sydney, analysis of the NSW Bureau of Transport Statistics' (BTS) employment forecasts was also conducted to provide for a long-term picture of where growth was likely to occur up to 2046 for the transport and warehousing sector in Sydney.

The 2013 ACBPS distributions were forecasted for future periods using BTS' 2012 employment forecast dataset with the transport and warehousing employment growth estimates used as a proxy for future growth in container distribution at the LGA level.

It should be noted that the ACBPS data was provided at a postcode level and BTS employment forecasts were available at the Travel zone ( Tz ) level in its most disaggregated form. To ensure that datasets are of a similar level of detail, Local Government Areas (LGAs) as defined by the Australian Bureau of Statistics (ABS), were used to develop current and future freight distributions. This process resulted in 38 LGAs that form the possible catchment areas within the Sydney metropolitan area.

### 3.2 Addition of Industrial Lands data

As part of a separate project (Demand Refresh 2014), where Deloitte had been engaged by MIC to conduct a more comprehensive refresh to Moorebank demand as part of the MIC's ongoing procurement process, additional catchment analysis was carried out looking at other possible datasets to determine drivers and indicators for container distribution.

The project team identified analysis conducted by the NSW Department of Planning and Environment (DoP) on employment lands (Employment Lands Task Force Report 2011) which provided, amongst other things, a stocktake of developed and undeveloped industrial land across Sydney. The report also included discussion on the average lead time involved with the development of industrial land (10 to 15 years).

An area for improvement identified in the original forecast approach for container distributions using BTS data were the relatively low growth rates associated with LGAs in western Sydney that were regarded as growth hotspots for future freight activity - in particular for Blacktown, Camden, Campbelltown, Liverpool and Penrith. Conversely, Fairfield is already regarded as relatively developed with little future growth potential outside of significant industrial re-development. This view was supported by DoP allocation of future industrial land with respect to the Broader Western Sydney Employment Area (WSEA) and South West Growth Centre (SWGC).

As such, the share of future developed industrial land for these LGAs were used as a proxy for future container freight distribution, as part of an alternative scenario showing a higher distribution skew towards Sydney's outer west. The remaining LGA container distribution shares were adjusted and re-distributed based on remaining forecast container volumes.

The revised distribution follows a linear interpolation between known container distributions in 2013 and the share of developed industrial land for the aforementioned LGAs in 2026 (based on a 15-year development lead time from 2011) before remaining constant for the remainder of the forecast period.

### 3.3 Updated Distribution

The following table compares the original estimated spatial distribution for Moorebank containers by LGA for 2030 with the modified spatial distribution by LGA based on the analysis using the updated data outlined above.

The key changes in the results are the reduction in the original estimates for 2030 for catchments closer to the east including Auburn, Holroyd, Parramatta and Fairfield and the increase in the estimated demand for LGA's with considerable industrial land development including Penrith, Blacktown, Campbelltown and Liverpool. The comparative results for each LGA are outlined in Table 1 below.

Table 1: Comparison of Moorebank IMT Demand by LGA at 2030

| LGA | Original Demand Update 2013 (2030) |  | Modified Demand Update 2013 based on selected DoP distribution (2030) |  |
| :---: | :---: | :---: | :---: | :---: |
|  | TEU | \% | TEU | \% |
| Ashfield | 0 | 0.0\% | 0 | 0.0\% |
| Auburn | 96,855 | 9.3\% | 34,655 | 3.3\% |
| Bankstown | 0 | 0.0\% | 0 | 0.0\% |
| Baulkham Hills | 17,659 | 1.7\% | 38,151 | 3.6\% |
| Blacktown | 233,150 | 22.3\% | 270,656 | 25.8\% |
| Botany Bay | 0 | 0.0\% | 0 | 0.0\% |
| Burwood | 0 | 0.0\% | 0 | 0.0\% |
| Camden | 12,017 | 1.1\% | 39,421 | 3.8\% |
| Campbelltown | 40,111 | 3.8\% | 56,750 | 5.4\% |
| Canada Bay | 0 | 0.0\% | 0 | 0.0\% |
| Canterbury | 0 | 0.0\% | 0 | 0.0\% |
| Fairfield | 200,352 | 19.2\% | 118,639 | 11.3\% |
| Holroyd | 142,169 | 13.6\% | 65,342 | 6.2\% |
| Hornsby | 0 | 0.0\% | 0 | 0.0\% |
| Hunters Hill | 0 | 0.0\% | 0 | 0.0\% |
| Hurstville | 0 | 0.0\% | 0 | 0.0\% |
| Kogarah | 0 | 0.0\% | 0 | 0.0\% |
| Ku-ring-gai | 0 | 0.0\% | 0 | 0.0\% |
| Lane Cove | 0 | 0.0\% | 0 | 0.0\% |
| Leichhardt | 0 | 0.0\% | 0 | 0.0\% |
| Liverpool | 109,415 | 10.5\% | 121,885 | 11.6\% |
| Manly | 0 | 0.0\% | 0 | 0.0\% |
| Marrickville | 0 | 0.0\% | 0 | 0.0\% |
| Mosman | 0 | 0.0\% | 0 | 0.0\% |
| North Sydney | 0 | 0.0\% | 0 | 0.0\% |
| Parramatta | 70,012 | 6.7\% | 32,466 | 3.1\% |
| Penrith | 124,200 | 11.9\% | 270,865 | 25.8\% |
| Pittwater | 0 | 0.0\% | 0 | 0.0\% |
| Randwick | 0 | 0.0\% | 0 | 0.0\% |
| Rockdale | 0 | 0.0\% | 0 | 0.0\% |
| Ryde | 0 | 0.0\% | 0 | 0.0\% |
| Strathfield | 0 | 0.0\% | 0 | 0.0\% |
| Sutherland Shire | 0 | 0.0\% | 0 | 0.0\% |
| Sydney | 0 | 0.0\% | 0 | 0.0\% |
| Warringah | 0 | 0.0\% | 0 | 0.0\% |
| Waverley | 0 | 0.0\% | 0 | 0.0\% |
| Willoughby | 0 | 0.0\% | 0 | 0.0\% |
| Woollahra | 0 | 0.0\% | 0 | 0.0\% |
| Total | 1,045,940 | 100.0\% | 1,048,830 | 100.0\% |

The following maps illustrate the changes in local government areas representing the primary demand catchment areas for IMEX cargo for Moorebank for 2030 between the original analysis and the updated analysis using the new data sets. Figure 2, the original demand analysis by LGA can be compared to Figure $\mathbf{3}$ with the modified analysis in the maps below.

Figure 2 : Original demand update 2013 distribution


Figure 3 : Modified demand update 2013 based on selected DoP distribution


## 4 Truck Trip Generation

The following section steps through the underlying assumptions and the approach taken to derive the possible number of trucks generated daily from the Moorebank Intermodal terminal as a result of the rail terminal operations and the warehousing operations onsite.

### 4.1 Assumptions

The assumptions used in the Calculation of Daily Truck Generation at Moorebank IMT are split into two areas:

1. Truck operations for container movements on and off site
2. Truck operations for warehousing related activities - palletised cargo

Table 2: Terminal Truck Assumptions

| Assumption |  | Basis of assumption |
| :---: | :---: | :---: |
| Container movement off site | 80\% | The amount of available warehousing on site can handle approximately $20 \%$ of cargo. |
| Full container movement to warehousing on-site Freight All Kinds (FAK) | 10\% | Assumption on possible lessors of warehousing operating within the market. |
| Container movement to warehousing on-site Inventory (Inv) | 10\% | Assumption on possible lessors of warehousing operating within the market. |
| Terminal operations | 52 weeks per year | Reflecting current operations at Port and other IMT's. |
| Split between Semi-Trailer and B-Double | 80\% / 20\% | Emerging profile at Port Botany. |
| Semi Trailer <br> - TEU Carrying Capacity <br> - Utilisation <br> - Average TEUs carried | $\begin{aligned} & \cdot 2 \\ & \cdot 80 \% \\ & \cdot 1.6 \end{aligned}$ | Emerging profile at Port Botany - known capacity of vehicle and growth in FEU. |
| B-Double <br> - TEU Carrying Capacity Utilisation <br> Average TEUs carried | $\begin{aligned} & \cdot 3 \\ & \cdot 80 \% \\ & \cdot 2.4 \end{aligned}$ | Emerging profile at Port Botany - known capacity of vehicle and growth in FEU. |
| Truck load matching for Semi-Trailer | 30\% | Market disaggregation by operator, customer and geography will limit backloading opportunities. A maximum of $30 \%$ backloading has been assumed. This has been applied only to Semi trailers moving containers off site. The effective backloading rate across all Moorebank volume is therefore significantly lower. |
| Truck distribution | 85\% - Weekday $15 \%$ - Weekend | Majority of warehouse and distribution facilities operate 5 or 6 day week operations. Truck movements into and out of Port Botany reflect this profile. |
| Estimated peak hour multiplier of daily traffic | 4.2\% | The $4.2 \%$ represents $1 / 24$ of the daily flow, i.e. with a flat 24 hour profile, one hour $=$ 4.2\%. Agreed with Roads and Maritime Services (RMS) that it is probable that the 'gate bookings' would be less in the AM peak hour as shippers attempted to avoid peak hour congestion. |

Table 3 : Warehousing related truck assumptions

| Assumption |  | Basis of assumption |
| :---: | :---: | :---: |
| Equivalent pallets loads per TEU for domestic distribution | 25 | Container mass limit and cubic capacity will generate average general freight volume of 10-12 tonne per TEU - average food and beverage or retail pallet load is approximately $300-500 \mathrm{~kg}$. |
| Truck fleet for palletised cargo - outbound | $\begin{aligned} & 34 \% \text { - Semi-trailer } \\ & 66 \% \text { - Rigid } \end{aligned}$ | Estimate only based on market knowledge. |
| Truck fleet for palletised cargo - inbound | 100\% - Rigid | Estimate only based on market knowledge. |
| Pallets per Semi-Trailer | 20 | Dimensions of standard pallet and truck and applicable weight restrictions. |
| Pallets per Rigid | 8 | Dimensions of standard pallet and truck and applicable weight restrictions. |
| Truck load matching for Semi-Trailer | None | It has been assumed that market disaggregation by operator, customer and geography will limit backloading opportunities. |
| Truck distribution | 95\% - Weekday <br> 5\% - Weekend | Majority of the market receiving palletised goods does not operate weekend loading/unloaded operations. |
| Estimated peak hour multiplier of daily traffic | 4.2\% | The $4.2 \%$ represents $1 / 24$ of the daily flow, i.e. with a flat 24 hour profile, one hour $=$ $4.2 \%$. Agreed with the RMS that it is probable that the 'gate bookings' would be less in the AM peak hour as shippers attempted to avoid peak hour congestion. |

### 4.2 Approach to Estimating Truck Trips

In order to estimate the daily heavy vehicles generated from the Moorebank IMT the forecast volumes for the terminal at 2030 were derived. These estimates were broken down into three categories for containers both arriving and departing the site by rail:

- Full container load (FCL) movements arriving or departing the terminal by rail and moving directly offsite or onsite by road;
- FCL's moving within the site between the rail terminal and associated warehousing with all cargo arriving or leaving the warehouses by truck as deconsolidated or palletised cargo; and
- Empty (MT) containers. Warehouse related FCL's were further broken down equally into two segments: Freight all kinds (FAK) to be deconsolidated and delivered; and inventory (INV), which was assumed to be held in the warehouse for a period prior to delivery. It has been assumed that FCL's and MT's would leave and return to the site on a combination of semi-trailers and b-doubles whilst FAK and Inventory would leave and return to the site on a mix of semi-trailers and rigid trucks.


## Consultation with Roads and Maritime Services (RMS)

Two sessions were undertaken, in February and April 2014, with representatives from RMS (Network Optimisation and Road Network Analysis team) to review both the approach and Liability limited by a scheme approved under Professional Standards Legislation.
results. They undertook their own analysis based on the underlying demand volumes and assumptions as documented and during a meeting with RMS personnel, they indicated that they reached similar outcomes.

### 4.2.1 IMEX and Interstate throughput

The terminal is anticipated to handle 500,000 TEU ( 250,000 TEU inbound and 250,000 TEU outbound) of interstate and close to 1.1 million TEU (547,000 TEU inbound and 499,000 outbound) of IMEX throughput when it reaches full capacity. It is not expected that this would occur before 2040, particularly for interstate traffic. The demand modelling estimated that, by 2030, the Moorebank IMT would be handling approximately 1.046 million TEUs of IMEX cargo per annum (two-way total) and handling approximately 328,000 TEUs of interstate cargo per annum (two-way total) and by 2050 the Terminal would be handling approximately 1.046 million TEUs of IMEX cargo per annum (two-way total) and handling approximately 406,000 TEUs of interstate cargo per annum (two-way total). It is assumed that 94,000 TEU would be transhipped between rail services utilising the terminal. These containers would therefore not be transported between the rail terminal and the warehousing operations on or off site.

### 4.3 Movements requiring transport off site

Utilising the demand estimates for the respective IMEX and interstate markets, the following steps were taken to identify the nature of the movements into and out of Moorebank IMT and whether the movements were as containers (direct movements to and from the site) or as deconsolidated palletised cargo (via the warehouses). The second consideration was whether or not the internal movements relating to the warehousing on site generated a surplus or a shortfall of empty containers as this would determine whether there would be a requirement to move additional empty containers to and from the site by road.

Table 4 : Onsite empty container imbalance

|  | Loaded TEU ex rail <br> into Warehouse | Loaded TEU for rail <br> out of Warehouse | Empty TEU surplus <br> (shortfall) <br> generated |
| :--- | :---: | :---: | :---: |
| IMEX | 109,400 | 34,600 | 74,800 |
| Interstate 2030 | 24,000 | 24,000 | 0 |
| Interstate 2050 | 29,800 | 29,800 | 0 |

Once these flows were determined then the calculation of the associated truck movements could be estimated.

### 4.3.1 IMEX market

1. Of the 1.374 million TEUs expected to be handled through the terminal in 2030, the breakdown between IMEX and interstate are as follows:
1,374,000 TEUs = 1,046,000 IMEX TEUs + 328,000 interstate TEUs
2. Of the 1.046 million IMEX TEUs handled, the breakdown between full imports, full exports and empty containers are as follows:
1,046,000 TEUs = 547,000 full import TEUs + 173,000 full export TEUs + (326,000 empty TEUs
3. Of the 1.046 million total TEUs in 2030 (and 2050), the breakdown between containers inbound and containers outbound are as follows:
1,046,000 TEUs $=547,000$ inbound TEUs $+499,000$ outbound TEUs
4. Of the 547,000 TEUs containers arriving by rail at the site, the breakdown between loaded and empty containers is as follows:
547,000 TEUs = 547,000 loaded TEUs + 0 empty TEUs
5. Of the 499,000 TEUs containers leaving the site by rail, the breakdown between loaded and empty containers is as follows:
499,000 TEUs $=173,000$ loaded TEUs $+326,000$ empty TEUs
6. It was assumed that $80 \%$ of the loaded total TEU would move to and from the site as containers and $20 \%$ of the loaded total TEU would move through the onsite warehousing. The surplus or shortfall of empty containers were all assumed to move directly to and from the site:
547,000 loaded TEUs from site $=(547,000 \times 80 \%$ direct to site) $+(547,000 \times 20 \%$ to onsite warehousing)
= 437,600 loaded TEUs direct + 109,400 TEUs via warehouses from site by road

173,000 loaded TEUs to site $=(173,000 \times 80 \%$ direct from site $)+(173,000 \times 20 \%$
from onsite warehousing)
= 138,400 loaded TEUs direct + 34,600 TEUs via warehouses to site by road

251,200 empty TEUs to and from site $=326,000$ empty containers from MB by rail + 0 empties into MB by rail - 74,800 surplus empty containers generated on site
7. As outlined above it was assumed that all of the empty containers less the onsite surplus and $80 \%$ of the loaded total TEU would move off the site as containers.

827,200 Direct TEUs $=251,200$ empty TEU's $+138,400$ loaded direct into terminal + 437,600 loaded TEUs direct out of terminal
8. The $20 \%$ going via warehouses was split equally, resulting in $10 \%$ going to warehousing onsite for destuffing (FAK) and direct delivery and $10 \%$ going to warehousing for destuffing and placement into inventory (Inv) for later delivery.

```
144,000 TEU's via warehouses =
    = 109,400 TEUs out of warehouses + 34,600 TEU's into warehouses
```

$$
\begin{aligned}
= & (109,400 \times 50 \% \text { FAK) leaving + (109,400 x } 50 \% \text { Inventory) leaving + } \\
& 34,600 \times 50 \% \text { FAK) arriving + (34,600 x } 50 \% \text { Inventory) arriving } \\
= & (54,700 \text { FAK and 54,700 Inv) leaving site from warehouses }+(17,300 \\
& \text { FAK and 17,300 Inv) arriving at site warehouses } \\
\text { Or }= & (54,700 \text { FAK and 17,300 FAK) TEUs into/out of warehouses } \\
& +(54,700 \text { Inv and 17,300 Inv) TEUs into/out of warehouses } \\
= & 72,000 \text { FAK TEUs and 72,000 Inv TEU's arriving and leaving via the } \\
& \quad \text { warehouses }
\end{aligned}
$$

9. This can be further summarised into the total number of IMEX ( 1.046 million) split into total FCL Direct $(827,200)$ plus total TEUs via the warehousing onsite $(144,000)$ plus empty containers generated onsite $(74,800)$ :

1,046,000 TEUs $=827,200$ containers direct to/from customers via road $+72,000$ FAK TEUs + 72,000 Inventory TEUs + 74,800 surplus onsite empty containers

### 4.3.2 Interstate Market - 2030

1. Of the 1.374 million TEUs expected to be handled through the terminal in 2030, the breakdown between IMEX and interstate are as follows:
```
1,374,000 TEUs = 1,046,000 IMEX TEUs + 328,000 interstate TEUs
```

2. Of the 328,000 interstate TEUs handled, the breakdown between full inbound, full outbound and empty containers are as follows:

## 328,000 TEUs = 120,000 full inbound TEUs + 120,000 full outbound TEUs + 88,000 empty

3. It was assumed that $80 \%$ of the loaded total TEU would move to and from the site as containers and $20 \%$ of the loaded total TEU would move through the onsite warehousing. The empty containers were all assumed to move directly to and from the site as there is no surplus or shortfall onsite:

$$
\begin{aligned}
& \text { 120,000 loaded TEUs to site }=(120,000 \times 80 \% \text { direct to site })+(120,000 \times 20 \% \text { to } \\
&\text { onsite warehousing }) \\
&= 96,000 \text { loaded TEUs direct }+24,000 \text { TEUs via } \\
& \text { warehouses }
\end{aligned}
$$

88,000 empty TEUs to and from site $=44,000$ empties into $M B+44,000$ empties out of MB
4. As outlined above it was assumed that all of the empty containers and $80 \%$ of the loaded total TEU would move off the site as containers.

```
280,000 Direct TEUs = 88,000 empty TEU's + 96,000 loaded direct into terminal+
96,000 loaded TEUs direct out of terminal
```

5. The $20 \%$ going via warehouses was split equally, resulting in $10 \%$ going to warehousing onsite for destuffing (FAK) and impending delivery and $10 \%$ going to warehousing for destuffing and placement into inventory for later delivery.
```
48,000 TEU's via warehouses =
    = 24,000 TEUs out of warehouses + 24,000 TEU's into warehouses
    = (24,000 x 50% FAK) leaving + (24,000 x 50% Inventory) arriving +
        (24,000 x 50% FAK) leaving + (24,000 x 50% Inventory) arriving
    = (12,000 FAK and 12,000 Inv) leaving site from warehouses + (12,000
        FAK and 12,000 Inv) arriving at site warehouses
    = 24,000 TEUs leaving and 24,000 TEUs arriving via the warehouses
Or
    = (12,000 FAK and 12,000 FAK) TEUs into/out of warehouses
        + (12,000 Inv and 12,000 Inv) TEUs into/out of warehouses
    = 24,000 FAK TEUs and 24,000 Inv TEU's arriving and leaving via the
        warehouses
```

6. Therefore the total number of Interstate TEU's $(328,000)$ can be split into total FCL Direct $(280,000)$ and total TEUs via the warehousing onsite $(48,000)$ :
```
328,000 TEUs = 280,000 containers direct to/from customers + 24,000 FAK TEUs
    + 24,000 Inventory TEUs
```


### 4.3.3 Interstate Market - 2050

1. Of the 1.452 million TEUs expected to be handled through the terminal in 2050, the breakdown between IMEX and interstate are as follows: 1,452,000 TEUs = 1,046,000 IMEX TEUs + 406,000 interstate TEUs
2. Of the 406,000 interstate TEUs handled, the breakdown between full inbound, full outbound and empty containers are as follows:
```
406,000 TEUs = 149,000 full inbound TEUs + 149,000 full outbound TEUs +
    108,000 empty
```

3. It was assumed that $80 \%$ of the loaded total TEU would move to and from the site as containers and $20 \%$ of the loaded total TEU would move through the onsite warehousing. The empty containers were all assumed to move directly to and from the site:
149,000 loaded TEUs to site $=(149,000 \times 80 \%$ direct to site $)+(149,000 \times 20 \%$ to onsite warehousing)
```
    = 119,200 loaded TEUs direct + 29,800 TEUs via
    warehouses
149,000 loaded TEUs from site = (149,000 x 80% direct from site) + (149,000 x
    20% from onsite warehousing)
    = 119,200 loaded TEUs direct + 29,800 TEUs via
    warehouses
```

108,000 empty TEUs to and from site $=54,000$ empties into $M B+54,000$ empties out of MB
4. As outlined above it was assumed that all of the empty containers and $80 \%$ of the loaded total TEU would move off the site as containers

346,400 Direct TEUs $=108,000$ empty TEU's $+119,200$ loaded direct into terminal + 119,200 loaded TEUs direct out of terminal
5. The $20 \%$ going via warehouses was split equally, resulting in $10 \%$ going to warehousing onsite for destuffing (FAK) and impending delivery and $10 \%$ going to warehousing for destuffing and placement into inventory for later delivery.

59,600 TEU's via warehouses $=$
= 29,800 TEUs out of warehouses + 29,800 TEU's into warehouses
$=(29,800 \times 50 \%$ FAK) leaving $+(29,800 \times 50 \%$ Inventory) leaving + (24,000 x 50\% FAK) arriving + (24,000 x 50\% Inventory) arriving
= (14,900 FAK and 14,900 Inv) leaving site from warehouses + (14,900 FAK and 14,900 Inv) arriving at site warehouses
= 29,800 TEUs leaving and 29,800 TEUs arriving via the warehouses
Or
= (14,900 FAK and 14,900 FAK) TEUs into/out of warehouses + (14,900 Inv and 14,900 Inv) TEUs into/out of warehouses
= 29,800 FAK TEUs and 29,800 Inv TEU's arriving and leaving via the warehouses
6. Therefore the total number of Interstate TEU's handled at the terminal at 2050 $(406,000)$ can be split into total FCL Direct $(346,400)$ and total TEUs via the warehousing onsite $(59,600)$ :

```
406,000 TEUs = 346,400 containers direct to/from customers + 29,800 FAK TEUs
    + 29,800 Inventory TEUs
```


### 4.3.4 Combined IMEX and Interstate at 2030

1. Of the 1.374 million TEUs expected to be handled through the terminal in 2030, the breakdown between IMEX and interstate are as follows: 1,374,000 TEUs = 1,046,000 IMEX TEUs + 328,000 interstate TEUs
2. Of the 1.374 million total TEUs in 2030, the breakdown between containers arriving at the site by rail and containers leaving the site by rail are as follows:
1,374,000 TEUs $=711,000$ inbound TEUs $+663,000$ outbound TEUs
3. Of the 711,000 TEUs containers leaving the site by road the breakdown between loaded and empty containers is as follows:
711,000 TEUs $=667,000$ loaded TEUs $+44,000$ empty TEUs
4. Of the 663,000 TEUs leaving the site by rail, 588,000 TEU's arrive at the site by road - the breakdown between loaded and empty containers is as follows:

588,200 TEUs $=293,000$ loaded TEUs $+295,000$ empty TEUs
5. It was assumed that $80 \%$ of the loaded total TEU would move to and from the site as containers and $20 \%$ of the loaded total TEU would move through the onsite warehousing. The empty containers (less surplus onsite) were all assumed to move directly to and from the site:
293,000 loaded TEUs to site $=(293,000 \times 80 \%$ direct to site $)+(293,000 \times 20 \%$ to onsite warehousing)
= 234,400 loaded TEUs direct + 58,600 TEUs via warehouses

667,000 loaded TEUs from site $=(667,000 \times 80 \%$ direct from site $)+(667,000 x$ 20\% from onsite warehousing)
$=533,600$ loaded TEUs direct $+133,400$ TEUs via warehouses

339,000 empty TEUs to and from site $=\mathbf{2 9 5 , 0 0 0}$ empties into $M B+44,000$ empties out of MB
6. As outlined above it was assumed that all of the empty containers, less any surplus generated through the matching of loads into and out of the warehouse and $80 \%$ of the loaded total TEU would move off the site as containers.

1,107,200 Direct TEUs $=414,000$ empty TEU's $-74,800$ surplus empties ex warehouse + 234,400 loaded direct into terminal + 533,600 loaded TEUs direct out of terminal
7. The $20 \%$ going via warehouses was split equally, resulting in $10 \%$ going to warehousing onsite for destuffing (FAK) and direct delivery and $10 \%$ going to warehousing for destuffing and placement into inventory for later delivery.

```
192,000 TEU's via warehouses =
    = 133,400 TEUs out of warehouses + 58,600 TEU's into warehouses
\(=(133,400 \times 50 \%\) FAK) leaving \(+(133,400 \times 50 \%\) Inventory) leaving + (58,600 x 50\% FAK) arriving + (58,600 x 50\% Inventory) arriving
```

$=(66,700$ FAK and 66,700 Inv) leaving site from warehouses + (29,300 FAK and 29,300 Inv) arriving at site warehouses

```
    = 96,000 TEUs leaving and 96,000 TEUs arriving via the warehouses
Or
    = (66,700 FAK and 29,300 FAK) TEUs into/out of warehouses
    + (66,700 Inv and 29,300 Inv) TEUs into/out of warehouses
    = 96,000 FAK TEUs and 96,000 Inv TEU's arriving and leaving via the
        warehouses
```

8. This can be further summarised into the total number of IMEX and Interstate TEU's ( 1.374 million) split into total FCL Direct $(1.108 \mathrm{~m})$ and total TEUs via the warehousing onsite $(192,000)$ plus empties from onsite $(74,800)$ :

## 1,374,000 TEUs $=1,107,200$ containers direct to/from customers $\mathbf{+}$ 96,000 FAK TEUs + 96,000 Inventory TEUs + 74,800 surplus empties from warehouses

### 4.3.5 Combined IMEX and Interstate at 2050

1. Of the 1.452 million TEUs expected to be handled through the terminal in 2050 , the breakdown between IMEX and interstate are as follows:
```
1,452,000 TEUs = 1,046,000 IMEX TEUs + 406,000 interstate TEUs
```

2. Of the 1.452 million total TEUs in 2050 , the breakdown between containers arriving at the site by rail and containers leaving the site by rail are as follows:
1,452,000 TEUs $=750,000$ inbound TEUs $+702,000$ outbound TEUs
3. Of the 750,000 TEUs containers leaving the site by road the breakdown between loaded and empty containers is as follows:
750,000 TEUs $=\mathbf{6 9 6}, 000$ loaded TEUs $\boldsymbol{+ 5 4 , 0 0 0}$ empty TEUs
4. Of the 702,000 TEUs leaving the site by rail, 627,200 TEU's arrive at the site by road - the breakdown between loaded and empty containers is as follows:

627,200 TEUs $=322,000$ loaded TEUs $+305,200$ empty TEUs
5. It was assumed that $80 \%$ of the loaded total TEU would move to and from the site as containers and $20 \%$ of the loaded total TEU would move through the onsite warehousing. The empty containers (less surplus onsite) were all assumed to move directly to and from the site:
322,000 loaded TEUs to site $=(322,000 \times 80 \%$ direct to site $)+(322,000 \times 20 \%$ to onsite warehousing)
= 257,600 loaded TEUs direct $+64,400$ TEUs via warehouses

696,000 loaded TEUs from site $=(696,000 \times 80 \%$ direct from site $)+(696,000 x$ $20 \%$ from onsite warehousing)
= 556,800 loaded TEUs direct + 139,200 TEUs via warehouses

359,200 empty TEUs to and from site $=305,200$ empties into $M B+54,000$ empties out of MB
6. As outlined above it was assumed that all of the empty containers, less any surplus generated through the matching of loads into and out of the warehouse and $80 \%$ of the loaded total TEU would move off the site as containers.

1,173,600 Direct TEUs $=434,000$ empty TEU's $-74,800$ surplus empties ex warehouse + 257,600 loaded direct into terminal + 556,800 loaded TEUs direct out of terminal
7. The $20 \%$ going via warehouses was split equally, resulting in $10 \%$ going to warehousing onsite for destuffing (FAK) and direct delivery and $10 \%$ going to warehousing for destuffing and placement into inventory for later delivery.

```
203,600 TEU's via warehouses =
    = 139,200 TEUs out of warehouses + 64,400 TEU's into warehouses
    = (139,200 x 50% FAK) leaving + (139,200 x 50% Inventory) leaving +
        (64,400 x 50% FAK) arriving + (64,400 x 50% Inventory) arriving
    = (69,600 FAK and 69,600 Inv) leaving site from warehouses + (32,200
        FAK and 32,200 Inv) arriving at site warehouses
Or
    = (69,600 FAK and 32,200 FAK) TEUs into/out of warehouses
    + (69,600 Inv and 32,200 Inv) TEUs into/out of warehouses
    = 101,800 FAK TEUs and 101,800 Inv TEU's arriving and leaving via the
        warehouses
```

8. This can be further summarised into the total number of IMEX and Interstate TEU's ( 1.452 million) split into total FCL Direct ( 1.174 million) and total TEUs via the warehousing onsite $(203,600)$ plus empties from onsite $(74,000)$ :
```
1,452,000 TEUs = 1,173,600 containers direct to/from customers + 101,800 FAK
                                    TEUs + 101,800 Inventory TEUs + 74,800 surplus empties from
                                    warehouses
```


### 4.3.6 Summary

A summary of the various components is outlined in Table 5 below for volumes at 2030 and in Table 6 for volumes at 2050.

Table 5 : Summary of terminal throughput at 2030

|  |  | $\begin{aligned} & \text { IMEX } \\ & \text { '000 TEU } \end{aligned}$ | Interstate '000 TEU | Total '000 TEU |  | $\begin{aligned} & \text { FAK (pack/ } \\ & \text { unpack) } \\ & \text { '000 TEU } \end{aligned}$ | Warehouse Inventory 'O00TEU |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pathway split/share |  |  |  |  | 80\% | 10\% | 10\% |
| Inbound to site by rail from port | Full | 547.000 | 120.000 | 667.000 | 533.600 | 66.700 | 66.700 |
|  | Empty | - | 44.000 | 44.000 | 44.000 |  |  |
|  | Total | 547.000 | 164.000 | 711.000 | 577.600 |  |  |
| Outbound from site by rail to port | Full | 173.000 | 120.000 | 293.000 | 234.400 | 29.300 | 29.300 |
|  | Empty | 326.000 | 44.000 | 370.000 | 370.000 |  |  |
|  | Total | 499.000 | 164.000 | 663.000 | 604.400 |  |  |
|  | Totals | 1,046.000 | 328.000 | 1,374.000 | 1,182.000 | 96.000 | 96.000 |

Table 6 : Summary of Terminal throughput at 2050

|  |  | $\begin{gathered} \text { IMEX } \\ \text { '000 TEU } \end{gathered}$ | Interstate 'OOO TEU | Total OOO TEU |  | $\begin{gathered} \text { FAK (pack/ } \\ \text { unpack) } \\ \text { '000 TEU } \end{gathered}$ | Warehouse Inventory '000TEU |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pathway split/share |  |  |  |  | 80\% | 10\% | 10\% |
| Inbound to site by rail from port | Full | 547.000 | 149.000 | 696.000 | 556.800 | 69.600 | 69.600 |
|  | Empty | - | 54.000 | 54.000 | 54.000 |  |  |
|  | Total | 547.000 | 203.000 | 750.000 | 610.800 |  |  |
| Outbound from site by rail to port | Full | 173.000 | 149.000 | 322.000 | 257.600 | 32.200 | 32.200 |
|  | Empty | 326.000 | 54.000 | 380.000 | 306.000 |  |  |
|  | Total | 499.000 | 203.000 | 702.000 | 637.600 |  |  |
|  | Totals | 1,046.000 | 406.000 | 1,452.000 | 1,248.400 | 101.800 | 101.800 |

The following diagrams illustrate the flows of TEU for each of the IMEX and Interstate markets at 2030 and when the terminal is close to capacity at 2050. Each diagram depicts both the empty and full containers arriving and leaving the terminal by rail and whether the containers stay within the site for handling through the warehouse, or leave the site for unpacking or packing at a customer site.

The volumes for the IMEX market are the same for both 2030 and 2050 as it is assumed that the IMEX terminal will reach capacity close to 2030. Full size diagrams are included in Appendix A.

Figure 4 : Moorebank IMEX flows for 2030


Figure 5: Moorebank Interstate flows for 2030


Figure 6 : Moorebank Terminal interstate container flows at 2050


Full size diagrams are included at Appendix A.

### 4.4 Direct FCL and empty container movements

### 4.4.1 IMEX Market

The demand analysis has determined likely future demand for IMEX traffics through the terminal. This total demand has then been allocated to cargo moving in the container between the terminal and the customer directly or via the onsite warehouse for consolidation/deconsolidation. In addition, empty containers move between the terminal and offsite locations. A different transport profile has been assumed for containers (whether loaded or empty) moving directly from the terminal to an offsite location. As the IMEX terminal is anticipated to reach capacity around 2030, the estimates for IMEX truck generation at 2030 have also been used to represent the situation at 2050. The calculations for estimating the number of direct movements and associated truck trips is set out below.

437,600 TEUs leaving the site by road (imports) $=(547,000$ full import TEUs $x$ 80\%)

389,600 TEUs arriving at the site by road (exports) $=(173,000$ full export TEUs $x$ 80\%) + 251,200 empty export TEUs

1. It is assumed that the terminal would be operational 52 weeks per year. 437,600 import TEUs $\div 52=8,415$ TEUs leaving the IMT by road per week

389,600 export TEUs $\div 52=7,492$ TEUs arriving at the IMT by road per week
2. It was assumed that trucks moving containers in and out of Moorebank IMT will comprise $80 \%$ semi-trailers and $20 \%$ B-Doubles:

Semi-Trailer TEUs (80\% of TEU's arriving at or leaving the terminal):
8,415 TEUs $x$ 80\% $=6,732$ TEUs out on a Semi
7,492 TEUs x 80\% = 5,994 TEUs in on a Semi
B-Double TEUs (20\% of TEU's arriving at or leaving the terminal):
8,415 TEUs $\times 20 \%=1,683$ TEUs out on a B-Double
7,492 TEUs x 20\% = 1,498 TEUs in on a B-Double
3. Each Semi-Trailer truck is assumed to have the capacity to carry 2 TEUs with an utilisation of $80 \%$ on average resulting in an average 1.6 TEUs per Semi-Trailer truck. B-double trucks will have the capacity to carry 3 TEUs, and with an average utilisation of $80 \%$ the resulting average TEUs per B-Double truck is 2.4. Using these factors, the weekly total loaded truck movements can be derived.

6,732 TEUs out on a Semi $\div 1.6$ TEUs per Semi $=4,208$ Semis out of terminal/per week

5,994 TEUs in on a Semi $\div$ 1.6 TEUs per Semi $=3,746$ Semis into terminal per week

1,683 TEUs out on B-Double $\div 2.4$ TEUs per B-Double $=701$ B-Doubles out of terminal per week

1,498 TEUs in on B-Double $\div 2.4$ TEUs per B-Double $=624$ B-Doubles into terminal per week
4. In addition, each outbound movements outlined above will also generate an inbound movement. It is assumed that some load matching would occur, i.e. rather than every truck having to do an empty return journey to its origin, a portion of the journeys could be loaded both ways. For example, some outbound full import movements could be matched with full export or empty containers inbound, the remainder of the trucks would arrive empty. It was assumed that this load matching would be limited to only $30 \%$ of loaded Semi Trailer truck movements (generated off the direction with the more significant volume). All other movements would generate an empty running leg into or out of the terminal.

To generate the empty running trips for each truck type:

```
Empty running trips in = loaded trips out X (1-\% load matching factor)
Empty running trips out = loaded trips in - (loaded trips out - empty running
trips in)
Therefore:
```

4,208 loaded semis outbound X (1-30\% matched loads) $=\mathbf{2 , 9 4 5}$ semis running
empty into terminal per week

3,746 loaded semis inbound - (4,208 loaded semis outbound - 2,945 empty semis inbound) $=\mathbf{2 , 4 8 4}$ semis running empty out of terminal

701 loaded B-Doubles outbound X (1-0\% matched loads) $=701$ B-Doubles running empty into terminal per week

624 loaded B-Doubles inbound X (1-0\% matched loads) = 624 B-Doubles empty out of terminal per week

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips in + loaded trips in + empty trips out

| Total B-Double movements | $=701$ loads out +701 empty in +624 loads in + |
| ---: | :--- |
|  | 624 empty out |
|  | $=1,326$ trips out $+1,326$ trips in |
|  | $=2,651$ trips |
| Total semi movements | $=4,208$ loads out $+2,945$ empty in $+3,746$ loads |
| in $+2,484$ empty out |  |
|  | $=6,692$ trips out $+6,692$ trips in |
|  | $=13,383$ trips |

5. It was then assumed that $85 \%$ of container truck movements would occur on weekdays and $15 \%$ would occur on weekends based on current profiles at Port Botany. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday.
(2,651 B-Double trips per week X 85\%) $\div 5=451$ B-Double movements per weekday
(13,383 semi trips per week $X 85 \%) \div 5=2,275$ Semi movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 7 below.

Table 7 : Total inbound and outbound IMEX moves per week and per weekday (2030)

| Truck Status | Direction on <br> road | Truck Type | Trucks per <br> week <br> (a) | Average trucks <br> per Weekday <br> (b) |
| :---: | :---: | :---: | :---: | :---: |
|  | Loaded | Outbound | B-Double | 701 |

6. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. This is used because whilst the daily hours of operation may be less than 24 hours, there is an expectation that there would be a desire to avoid peak hour congestion - as a result the peak hour number \% would reduce, however the proportion of interpeak and offpeak volumes could be slightly higher on an hourly basis. This approach was discussed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ (for each direction) x $4.2 \%=$ trucks on and off site per hour in AM peak

451 B-Double movements per weekday $\div 2 \times 4.2 \%=9$ B-Double truck movements in AM peak hour in each direction

## 2,275 Semi movements per weekday $\div 2 \times 4.2 \%=48$ Semi truck movements in AM peak hour in each direction

Table 8 : Average weekday inbound and outbound IMEX Articulated truck movements

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | B-Double | 225 | 9 |
|  | Inbound | Semi | 1,138 | 48 |
|  |  | B-Double | 225 | 9 |

### 4.4.2 Interstate Market - 2030

The demand analysis also determined likely future demand for interstate traffic through the terminal. This total demand has then been allocated to cargo moving in the container between the terminal and the customer directly or via the onsite
warehouse for consolidation/deconsolidation. In addition, empty containers move between the terminal and offsite locations. A different transport profile has been assumed for containers (whether loaded or empty) moving directly from the terminal to an offsite location. To align the terms used between the IMEX and Interstate traffics, inbound movements into Sydney have been referred to as imports to the terminal, movements out of the terminal by rail have been referred to as exports. The calculations for estimating the number of direct movements and associated truck trips is set out below.

140,000 TEUs leaving the site by road (imports) $=(120,000$ full import TEUs $x$ 80\%) + 44,000 empty import TEUs

```
140,000 arriving at the site by road (exports) = (120,000 full export TEUs x 80%)
+ 44,000 empty export TEUs
```

1. It is assumed that the terminal would be operational 52 weeks per year.

140,000 import TEUs $\div 52=2,692$ TEUs leaving the IMT by road per week

140,000 export TEUs $\div 52=2,692$ TEUs arriving at the IMT by road per week
2. It was assumed that trucks moving containers in and out of Moorebank IMT will comprise $80 \%$ semi-trailers and $20 \%$ B-Doubles:

Semi-Trailer TEUs (80\% of TEU's arriving at or leaving the terminal):
2,692 TEUs $\times 80 \%=2,154$ TEUs out on a Semi
2,692 TEUs $\times 80 \%=2,154$ TEUs in on a Semi

B-Double TEUs (20\% of TEU's arriving at or leaving the terminal):

2,692 TEUs x 20\% = 538 TEUs out on a B-Double

2,692 TEUs x 20\% = 538 TEUs in on a B-Double
3. Each Semi-Trailer truck is assumed to have the capacity to carry 2 TEUs with an utilisation of $80 \%$ on average resulting in an average 1.6 TEUs per Semi-Trailer truck. B-double trucks will have the capacity to carry 3 TEUs, and with an average utilisation of $80 \%$ the resulting average TEUs per B-Double truck is 2.4. Using these factors, the weekly total loaded truck movements can be derived.

```
2,154 TEUs out on a Semi \div 1.6 TEUs per Semi = 1,346 Semis out of terminal/per
week
```

2,154 TEUs in on a Semi $\div 1.6$ TEUs per Semi $=1,346$ Semis into terminal per week

## 538 TEUs out on B-Double $\div 2.4$ TEUs per B-Double $=224$ B-Doubles out of terminal per week

538 TEUs in on B-Double $\div 2.4$ TEUs per $B$-Double $=224$ B-Doubles into terminal per week
4. In addition, each outbound movements outlined above will also generate an inbound movement. It is assumed that some load matching would occur, i.e. rather than every truck having to do an empty return journey to its origin, a portion of the journeys could be loaded both ways. For example, some outbound full import movements could be matched with full export or empty containers inbound, the remainder of the trucks would arrive empty. It was assumed that this load matching would be limited to only $30 \%$ of loaded Semi Trailer truck movements (generated off the direction with the more significant volume). All other movements would generate an empty running leg into or out of the terminal.

To generate the empty running trips for each truck type:
Empty running trips in = loaded trips out X (1-\% load matching factor)
Empty running trips out = loaded trips in - (loaded trips out - empty running trips in)

Therefore:

1,346 loaded semis outbound X (1-30\% matched loads) = 942 semis running empty into terminal per week

1,346 loaded semis inbound - (1,346 loaded semis outbound - 942 empty semis inbound) $\mathbf{=} 942$ semis running empty out of terminal

224 loaded B-Doubles outbound X (1-0\% matched loads) = 224 B-Doubles running empty into terminal per week

224 loaded B-Doubles inbound X (1-0\% matched loads) = 224 B-Doubles empty out of terminal per week

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips in + loaded trips in + empty trips out

Total B-Double movements = 224 loads out +224 empty in +224 loads in + 224 empty out
=449 trips out +449 trips in
$=897$ trips

```
Total semi movements
= 1,346 loads out + 942 empty in + 1,346 loads in
+942 empty out
= 2,288 trips out + 2,288 trips in
=4,577 trips
```

5. It was then assumed that $85 \%$ of container truck movements would occur on weekdays and $15 \%$ would occur on weekends based on current profiles at Port Botany. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday.
(897 B-Double trips per week X 85\%) $\div 5$ = 153 B-Double movements per weekday

## (4,577 semi trips per week $X 85 \%$ ) $\mathbf{5}=778$ Semi movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 9.

Table 9 : Total inbound and outbound interstate moves per week and per weekday (2030)

| Truck Status | Direction on road | Truck Type | Trucks pe week <br> (a) | Average trucks per Weekday <br> (b) |
| :---: | :---: | :---: | :---: | :---: |
| Loaded | Outbound | B-Double | 224 | 38 |
|  |  | Semi | 1,346 | 229 |
| Empty | Inbound | B-Double | 224 | 38 |
|  |  | Semi | 942 | 160 |
| Loaded | Inbound | B-Double | 224 | 38 |
|  |  | Semi | 1,346 | 229 |
| Empty | Outbound | B-Double | 224 | 38 |
|  |  | Semi | 942 | 160 |
| Total Truck movements | Outbound | B-Double | 449 | 76 |
|  |  | Semi | 2,288 | 389 |
|  | Inbound | B-Double | 449 | 76 |
|  |  | Semi | 2,288 | 389 |

6. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is based on one $24^{\text {th }}$ of the daily value. This is used because whilst the daily hours of operation may be less than 24 hours, there is an expectation that there would be a desire to avoid peak hour congestion - as a result the peak hour number \% would reduce, however the proportion of interpeak and offpeak volumes could be slightly higher on an hourly basis. This approach was agreed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ (for each direction) x 4.2\% = trucks on and off site per hour in AM peak

153 B-Double movements per weekday $\div 2 \times 4.2 \%=3$ B-Double truck movements in AM peak hour in each direction

778 Semi movements per weekday $\div 2 \times 4.2 \%=16$ Semi truck movements in AM peak hour in each direction

Table 10 : Average weekday interstate inbound and outbound Articulated truck movements

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | B-Double | 76 | 3 |
|  | Inbound | Semi | 389 | 16 |
|  |  | B-Double | 76 | 3 |

### 4.4.3 Interstate Market - 2050

1. The calculations for estimating the number of direct movements and associated truck trips for the interstate market at 2050 is set out below.

173,200 TEUs leaving the site by road (imports) $=(149,000$ full import TEUs $x$ 80\%) + 54,000 empty import TEUs

173,200 arriving at the site by road (exports) = (149,000 full export TEUs x 80\%) + 54,000 empty export TEUs
2. It is assumed that the terminal would be operational 52 weeks per year.

173,200 import TEUs $\div 52=3,331$ TEUs leaving the IMT by road per week

173,200 export TEUs $\div 52=3,331$ TEUs arriving at the IMT by road per week
3. It was assumed that trucks moving containers in and out of Moorebank IMT will comprise $80 \%$ semi-trailers and $20 \%$ B-Doubles:

Semi-Trailer TEUs (80\% of TEU's arriving at or leaving the terminal):

3,331 TEUs $\times 80 \%=2,665$ TEUs out on a Semi

3,331 TEUs $\times 80 \%=2,665$ TEUs in on a Semi

B-Double TEUs (20\% of TEU's arriving at or leaving the terminal):

3,331 TEUs x 20\% = 666 TEUs out on a B-Double

3,331 TEUs x 20\% = 666 TEUs in on a B-Double
4. Each Semi-Trailer truck is assumed to have the capacity to carry 2 TEUs with an utilisation of $80 \%$ on average resulting in an average 1.6 TEUs per Semi-Trailer truck. B-double trucks will have the capacity to carry 3 TEUs, and with an average
utilisation of $80 \%$ the resulting average TEUs per B-Double truck is 2.4. Using these factors, the weekly total loaded truck movements can be derived.

2,665 TEUs out on a Semi $\div 1.6$ TEUs per Semi $=1,665$ Semis out of terminal/per week

2,665 TEUs in on a Semi $\div 1.6$ TEUs per Semi $=1,665$ Semis into terminal per week

666 TEUs out on B-Double $\div 2.4$ TEUs per B-Double $=278$ B-Doubles out of terminal per week

666 TEUs in on B-Double $\div 2.4$ TEUs per B-Double $=278$ B-Doubles into terminal per week
5. In addition, each outbound movements outlined above will also generate an inbound movement. It is assumed that some load matching would occur, i.e. rather than every truck having to do an empty return journey to its origin, a portion of the journeys could be loaded both ways. For example, some outbound full import movements could be matched with full export or empty containers inbound, the remainder of the trucks would arrive empty. It was assumed that this load matching would be limited to only $30 \%$ of loaded Semi Trailer truck movements (generated off the direction with the more significant volume). All other movements would generate an empty running leg into or out of the terminal.

To generate the empty running trips for each truck type:
Empty running trips in = loaded trips out X (1-\% load matching factor)
Empty running trips out = loaded trips in - (loaded trips out - empty running trips in)

Therefore:

1,665 loaded semis outbound $X$ (1-30\% matched loads) $=1,166$ semis running empty into terminal per week

1,665 loaded semis inbound - (1,665 loaded semis outbound - 1,166 empty semis inbound) $=1,166$ semis running empty out of terminal

278 loaded B-Doubles outbound X (1-0\% matched loads) $=278$ B-Doubles running empty into terminal per week

## 278 loaded B-Doubles inbound X (1-0\% matched loads) $=278$ B-Doubles empty out of terminal per week

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

```
Total trips per week = loaded trips out + empty trips in + loaded trips in + empty
trips out
\begin{tabular}{rl} 
Total B-Double movements & \(=278\) loads out +278 empty in +278 loads in + \\
& 278 empty out \\
& \(=555\) trips out +555 trips in \\
& \(=1,110\) trips \\
Total semi movements & \(=1,665\) loads out \(+1,166\) empty in \(+1,665\) loads \\
& in \(+1,166\) empty out \\
& \(=2,831\) trips out \(+2,831\) trips in \\
& \(=5,662\) trips
\end{tabular}
```

6. It was then assumed that $85 \%$ of container truck movements would occur on weekdays and $15 \%$ would occur on weekends based on current profiles at Port Botany. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday.

## (1,110 B-Double trips per week X $85 \%$ ) $\div 5=189$ B-Double movements per weekday

(5,662 semi trips per week $X 85 \%$ ) $\div 5=963$ Semi movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 11.

Table 11: Total inbound and outbound interstate related moves per week and per weekday (2050)

| Truck Status | Direction on road | Truck Type | Trucks per week (a) | Average trucks per Weekday <br> (b) |
| :---: | :---: | :---: | :---: | :---: |
| Loaded | Outbound | B-Double | 278 | 47 |
|  |  | Semi | 1,665 | 283 |
| Empty | Inbound | B-Double | 278 | 47 |
|  |  | Semi | 1,166 | 198 |
| Loaded | Inbound | B-Double | 278 | 47 |
|  |  | Semi | 1,665 | 283 |
| Empty | Outbound | B-Double | 278 | 47 |
|  |  | Semi | 1,166 | 198 |
| Total Truck movements | Outbound | B-Double | 555 | 94 |
|  |  | Semi | 2,831 | 481 |
|  | Inbound | B-Double | 555 | 94 |
|  |  | Semi | 2,831 | 481 |

7. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is based on one $24^{\text {th }}$ of the daily value. This is used because whilst the daily hours of operation may
be less than 24 hours, there is an expectation that there would be a desire to avoid peak hour congestion - as a result the peak hour number \% would reduce, however the proportion of interpeak and offpeak volumes could be slightly higher on an hourly basis. This approach was agreed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ (for each direction) x $4.2 \%=$ trucks on and off site per hour in AM peak

189 B-Double movements per weekday $\div 2 \times 4.2 \%=4$ B-Double truck movements in AM peak hour in each direction

963 Semi movements per weekday $\div 2 \times 4.2 \%=20$ Semi truck movements in AM peak hour in each direction

Table 12 : Average weekday interstate inbound and outbound Articulated truck movements

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | B-Double | 94 | 4 |
|  | Inbound | Semi | 481 | 20 |
|  |  | B-Double | 94 | 4 |

### 4.4.4 Combined IMEX and Interstate movements at 2030

1. As outlined above, the demand analysis has determined likely future demand for both IMEX and interstate markets where Sydney is either an origin or a destination. For the purposes of simplification all international and interstate cargo destined for the Sydney market is referred to in the following as imports - all international and interstate cargo leaving the Sydney market is referred to as exports.

577,600 TEUs leaving the site by road (imports) $=$ 533,600 full import TEUs + 44,000 empty import TEUs

529,600 TEUs arriving at the site by road (exports) $=234,400$ full export TEUs +
295,200 empty export TEUs
2. It is assumed that the terminal would be operational 52 weeks per year. 577,600 import TEUs $\div 52=11,108$ TEUs leaving the IMT by road per week 529,600 export TEUs $\div 52=10,185$ TEUs arriving at the IMT by road per week
3. It was assumed that trucks moving containers in and out of Moorebank IMT will comprise $80 \%$ semi-trailers and $20 \%$ B-Doubles:

Semi-Trailer TEUs (80\% of TEU's arriving at or leaving the terminal):

```
11,108 TEUs \(\times 80 \%=8,886\) TEUs out on a Semi
10,185 TEUs \(\times 80 \%=8,148\) TEUs in on a Semi
B-Double TEUs (20\% of TEU's arriving at or leaving the terminal):
11,108 TEUs \(\times 20 \%=2,222\) TEUs out on a B-Double
10,185 TEUs x \(20 \%=2,037\) TEUs in on a B-Double
```

4. Each Semi-Trailer truck is assumed to have the capacity to carry 2 TEUs with an utilisation of $80 \%$ on average resulting in an average 1.6 TEUs per Semi-Trailer truck. B-double trucks will have the capacity to carry 3 TEUs, and with an average utilisation of $80 \%$ the resulting average TEUs per B-Double truck is 2.4. Using these factors, the weekly total loaded truck movements can be derived.

8,886 TEUs out on a Semi $\div 1.6$ TEUs per Semi $=5,554$ Semis out of terminal/per week

8,148 TEUs in on a Semi $\div$ 1.6 TEUs per Semi $=5,092$ Semis into terminal per week

2,222 TEUs out on B-Double $\div 2.4$ TEUs per B-Double $=926$ B-Doubles out of terminal per week

2,037 TEUs in on B-Double $\div 2.4$ TEUs per B-Double $=849$ B-Doubles into terminal per week
5. In addition, each outbound movements outlined above will also generate an inbound movement. It is assumed that some load matching would occur, i.e. rather than every truck having to do an empty return journey to its origin, a portion of the journeys could be loaded both ways. For example, some outbound full import movements could be matched with full export or empty containers inbound, the remainder of the trucks would arrive empty. It was assumed that this load matching would be limited to only $30 \%$ of loaded Semi Trailer truck movements (generated off the direction with the more significant volume). All other movements would generate an empty running leg into or out of the terminal.

To generate the empty running trips for each truck type:
Empty running trips in = loaded trips out X (1-\% load matching factor)

Empty running trips out = loaded trips in - (loaded trips out - empty running trips in)

Therefore:

5,554 loaded semis outbound $X(1-30 \%$ matched loads) $=3,888$ semis running
empty into terminal per week

5,092 loaded semis inbound - (5,554 loaded semis outbound - 3,888 empty semis inbound) $=3,426$ semis running empty out of terminal

926 loaded B-Doubles outbound X (1-0\% matched loads) $=926$ B-Doubles running empty into terminal per week

849 loaded B-Doubles inbound X (1-0\% matched loads) $=849$ B-Doubles empty out of terminal per week

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips out + loaded trips in + empty trips in

```
Total B-Double movements = 926 loads out + 849 empty out + 849 loads in +
                    926 empty in
    = 1,774 trips out + 1,774 trips in
    = 3,549 trips
    = 5,554 loads out + 3,426 empty out + 5,092 loads
    in + 3,888 empty in
    = 8,980 trips out + 8,980 trips in
    = 17,960 trips
```

6. It was then assumed that $85 \%$ of container truck movements would occur on weekdays and $15 \%$ would occur on weekends based on current profiles at Port Botany. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday.
> (3,549 B-Double trips per week X 85\%) $\div 5$ = 603 B-Double movements per weekday

(17,960 semi trips per week $X 85 \%) \div 5=3,053$ Semi movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 13 below.

Table 13 : Total combined inbound and outbound moves per week and per weekday (2030)

| Truck Status | Direction on <br> road | Truck Type | Trucks per <br> week <br> (a) | Average trucks <br> per Weekday <br> (b) |
| :---: | :---: | :---: | :---: | :---: |
| Loaded | Outbound | B-Double | 926 | 157 |
|  |  | Semi | 5,554 | 944 |
| Empty | Inbound | B-Double | 926 | 157 |
|  |  | Semi | 3,888 | 661 |
| Loaded | Inbound | B-Double | 849 | 144 |
|  |  | Semi | 5,092 | 866 |
| Empty | Outbound | B-Double | 849 | 144 |
|  | Total Truck <br> movements | Outbound | Semi | 3,426 |
|  |  | Inbound | S-Double | 1,774 |
|  |  | 8,980 | 302 |  |
|  |  | B-Double | 1,774 | 302 |

7. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is based on one $24^{\text {th }}$ of the daily value. This is used because whilst the daily hours of operation may be less than 24 hours, there is an expectation that there would be a desire to avoid peak hour congestion - as a result the peak hour number \% would reduce, however the proportion of interpeak and offpeak volumes could be slightly higher on an hourly basis. This approach was agreed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ in each direction x $4.2 \%=$ trucks on and off site per hour in AM peak

302 B-Double movements per weekday $\div 2 \times 4.2 \%=13$ B-Double truck movements in AM peak hour in each direction

1,527 Semi movements per weekday $\div 2 \times 4.2 \%=64$ Semi truck movements in AM peak hour in each direction

Table 14 : Combined average weekday inbound and outbound Articulated truck movements

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | B-Double | 302 | 13 |
|  | Inbound | Semi | 1,527 | 64 |
|  |  | B-Double | 302 | 13 |

### 4.4.5 Combined IMEX and Interstate movements at 2050

1. As outlined above, the demand analysis has determined likely future demand for both IMEX and interstate markets where Sydney is either an origin or a destination. For the
purposes of simplification all international and interstate cargo destined for the Sydney market is referred to in the following as imports - all international and interstate cargo leaving the Sydney market is referred to as exports.

610,800 TEUs leaving the site by road (imports) $=$ 556,800 full import TEUs + 54,000 empty import TEUs

562,800 TEUs arriving at the site by road (exports) $=257,600$ full export TEUs + 305,200 empty export TEUs
2. It is assumed that the terminal would be operational 52 weeks per year.

610,800 import TEUs $\div 52=11,746$ TEUs leaving the IMT by road per week
562,800 export TEUs $\div 52=10,823$ TEUs arriving at the IMT by road per week
3. It was assumed that trucks moving containers in and out of Moorebank IMT will comprise $80 \%$ semi-trailers and $20 \%$ B-Doubles:

Semi-Trailer TEUs (80\% of TEU's arriving at or leaving the terminal):
11,746 TEUs x $80 \%=9,397$ TEUs out on a Semi

10,823 TEUs $\times 80 \%=8,658$ TEUs in on a Semi

B-Double TEUs (20\% of TEU's arriving at or leaving the terminal):
11,746 TEUs x 20\% = 2,349 TEUs out on a B-Double
10,823 TEUs $\times 20 \%=2,165$ TEUs in on a B-Double
4. Each Semi-Trailer truck is assumed to have the capacity to carry 2 TEUs with an utilisation of $80 \%$ on average resulting in an average 1.6 TEUs per Semi-Trailer truck. B-double trucks will have the capacity to carry 3 TEUs, and with an average utilisation of $80 \%$ the resulting average TEUs per B-Double truck is 2.4. Using these factors, the weekly total loaded truck movements can be derived.

9,397 TEUs out on a Semi $\div 1.6$ TEUs per Semi $=5,873$ Semis out of terminal/per week

8,658 TEUs in on a Semi $\div 1.6$ TEUs per Semi $=5,412$ Semis into terminal per week

2,349 TEUs out on B-Double $\div 2.4$ TEUs per B-Double $=979$ B-Doubles out of terminal per week

2,165 TEUs in on B-Double $\div 2.4$ TEUs per B-Double $=902$ B-Doubles into terminal per week
5. In addition, each outbound movements outlined above will also generate an inbound movement. It is assumed that some load matching would occur, i.e. rather than every truck having to do an empty return journey to its origin, a portion of the journeys could be loaded both ways. For example, some outbound full import movements could be matched with full export or empty containers inbound, the remainder of the trucks would arrive empty. It was assumed that this load matching would be limited to only $30 \%$ of loaded Semi Trailer truck movements (generated off the direction with the more significant volume). All other movements would generate an empty running leg into or out of the terminal.

To generate the empty running trips for each truck type:
Empty running trips in = loaded trips out X (1-\% load matching factor)
Empty running trips out = loaded trips in - (loaded trips out - empty running trips in)

Therefore:

5,873 loaded semis outbound $X$ (1-30\% matched loads) $=4,111$ semis running empty into terminal per week

5,412 loaded semis inbound - (5,873 loaded semis outbound - 4,111 empty semis inbound) $=3,650$ semis running empty out of terminal

979 loaded B-Doubles outbound X (1-0\% matched loads) $=979$ B-Doubles running empty into terminal per week

902 loaded B-Doubles inbound X (1-0\% matched loads) $=902$ B-Doubles empty out of terminal per week

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips out + loaded trips in + empty trips in

$$
\begin{aligned}
\text { Total B-Double movements } & =979 \text { loads out }+902 \text { empty out }+902 \text { loads in }+ \\
& 979 \text { empty in } \\
& =1,881 \text { trips out }+1,881 \text { trips in } \\
& =3,762 \text { trips } \\
& =5,873 \text { loads out }+3,650 \text { empty out }+5,412 \text { loads } \\
\text { Total semi movements } \quad & \\
& =9,523 \text { trips out }+9,523 \text { trips in } \\
& =19,045 \text { trips }
\end{aligned}
$$

6. It was then assumed that $85 \%$ of container truck movements would occur on weekdays and $15 \%$ would occur on weekends based on current profiles at Port Botany. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday.
(3,762 B-Double trips per week $X 85 \%) \div 5=\begin{gathered}639 \text { B-Double movements per } \\ \text { weekday }\end{gathered}$ weekday
(19,045 semi trips per week $X 85 \%) \div 5=3,238$ Semi movements per weekday
Total inbound and outbound moves per week and per weekday can be summarised in
Table 15 below.
Table 15 : Total combined inbound and outbound moves per week and per weekday (2050)

| Truck Status | Direction on <br> road | Truck Type | Trucks per <br> week <br> (a) | Average trucks <br> per Weekday <br> (b) |
| :---: | :---: | :---: | :---: | :---: |
|  | Loaded | Outbound | B-Double | 979 |

7. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is based on one $24^{\text {th }}$ of the daily value. This is used because whilst the daily hours of operation may be less than 24 hours, there is an expectation that there would be a desire to avoid peak hour congestion - as a result the peak hour number \% would reduce, however the proportion of interpeak and offpeak volumes could be slightly higher on an hourly basis. This approach was agreed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ in each direction $\times 4.2 \%=$ trucks on and off site per hour in AM peak

639 B-Double movements per weekday $\div 2 \times 4.2 \%=13$ B-Double truck movements in AM peak hour in each direction

3,238 Semi movements per weekday $\div 2 \times 4.2 \%=68$ Semi truck movements in AM peak hour in each direction

Table 16 : Average combined weekday inbound and outbound Articulated truck movements 2050

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | B-Double | 320 | 13 |
|  | Inbound | Semi | 1,619 | 68 |
|  |  | B-Double | 320 | 13 |

### 4.5 Movements to and from the Warehouses

### 4.5.1 IMEX Market

Warehouse generated truck traffic movements were estimated using a similar methodology to the derivation of container truck movements, with some variation to the underlying assumptions. The most significant changes to the assumptions were:

- the makeup of the fleet;
- the proportion of movements occurring during the week; and
- the level of load matching.

The following steps were taken to derive the daily truck movements in and out of Moorebank IMT for cargo handled through the warehouses:

1. The Moorebank IMT will have enough on-site warehousing capacity to handle approximately $20 \%$ of all full TEUs. It is assumed that half of these will be held in inventory in onsite warehousing for a period of weeks with the rest being general cargo (FAK) which would be deconsolidated and distributed offsite within a few days or arrive onsite for consolidation and export.

## 547,000 full inbound TEUs x 10\% FAK = 54,700 TEU's FAK for distribution from site

547,000 full inbound TEUs x 10\% Inventory = 54,700 TEU's Inventory for distribution from site

173,000 full outbound TEU's $\times 10 \%$ FAK $=17,300$ TEU's FAK arriving at site for consolidation

173,000 full outbound TEU's $\times 10 \%$ Inventory $=17,300$ TEU's Inventory arriving at site for consolidation
2. It is assumed that the terminal would be operational 52 weeks per year.

54,700 FAK + 54,700 Inventory TEUs $\div 52=2,104$ TEUs into warehouse and distributed off site each week

17,300 FAK + 17,300 Inventory TEUs $\div 52$ = 665 TEUs arrive onto site and into warehouse each week
3. It is assumed that each TEU, when deconsolidated will generate approximately 25 pallet loads for domestic distribution:

2,104 TEU's x 25 equivalent pallet loads per TEU = 52,596 equivalent pallet loads into warehouse and distributed off site by road each week
$665 \times 25$ equivalent pallet loads per TEU = 16,635 equivalent pallet loads into warehouse by road and railed offsite each week
4. The truck fleet profile for palletised cargo will be different to that for direct FCL and MT container movements to and from the Moorebank terminal. It is assumed that trucks moving pallets out of Moorebank IMT warehousing will comprise of $34 \%$ semi-trailers and $66 \%$ rigid trucks whilst $100 \%$ of the palletised cargo arriving at the site will be carried by rigid trucks:

Deliveries from Moorebank warehouses:
52,596 pallets per week x $34 \%=17,883$ pallets out on semi-trailer trucks

52,596 pallets per week x 66\% = 34,713 pallets out on rigid trucks

Deliveries to Moorebank warehouses:
16,635 pallets per week x 100\% = 16,635 pallets in on rigid trucks
5. Semi-trailer trucks are likely to carry, on average 20 pallets per truck whilst rigid trucks have been assumed to carry, on average 8 pallets per load. Dividing the number of pallets by each average load determines the average number of loaded truck movements per week into and out of the warehouses.

Deliveries from Moorebank warehouses.
17,883 pallets in semis per week $\div 20$ pallets per truck $=894$ loaded semi-trailer truck movements out per week

34,713 pallets in rigids per week $\div 8$ pallets per truck $=4,339$ loaded rigid truck movements out per week

Deliveries to Moorebank warehouses:
16,625 pallets in rigids per week $\div 8$ pallets per truck $=2,079$ loaded rigid truck movements in per week
6. It is assumed that there will be no truck load matching for palletised cargo movement to and from the Moorebank IMT warehouses. Therefore all movements would generate an empty running leg into or out of the terminal. By adding the total inbound and outbound movements the total truck movements can be estimated.

Empty running trips in = loaded trips out X (1-\% load matching factor)

894 semis empty into terminal per week $=894$ loaded semis outbound X (1-0\% matched loads)

4,339 empty rigids into terminal per week $=4,339$ loaded rigids outbound $X$ (10\% matched loads)

2,079 empty rigids out of terminal per week $=2,079$ loaded rigids inbound X (1 0\% matched loads)

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

```
Total trips per week = loaded trips out + empty trips out + loaded trips in +
empty trips in
Total semi movements \(=894\) loads out +0 empty out +0 loads in +894
    empty in
    \(=894\) trips out +894 trips in
    \(=1,788\) trips per week
Total rigid movements \(=4,339\) loads out \(+2,079\) empty out \(+2,079\) loads in +
    4,339 empty in
    \(=6,419\) trips out \(+6,419\) trips in
    = 12,837 trips per week
```

7. It was then assumed that $95 \%$ of container truck movements would occur on weekdays and $5 \%$ would occur on weekends. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday
(1,788 semi-truck movements per week X 95\%) $\div 5=340$ semi-trailer movements per weekday
(12,837 rigid truck movements per week X 95\%) $\div 5=2,439$ rigid truck movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 17 below.

Table 17 : Average weekly inbound and outbound IMEX warehouse related road movements

| Truck Status | Direction on <br> road | Truck Type | Trucks per <br> week <br> (a) | Average trucks <br> per Weekday <br> (b) |
| :--- | :--- | :--- | :---: | :---: |
| Loaded | Outbound | Semi | 894 | 170 |
|  |  | Rigid | 4,339 | 824 |
| Empty | Inbound | Semi | 894 | 170 |
|  |  | Rigid | 4,339 | 824 |
| Loaded | Inbound | Semi | 0 | - |
|  |  | Rigid | 2,079 | 395 |
| Empty <br> Total Truck <br> movements | Outbound | Semi | 0 | - |
|  | Inbound | Rigid | 2,079 | 395 |
|  |  | Semi | 894 | 170 |

8. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is one 24th of the daily value. This is used because whilst the daily hours of operation may be less than 24 , there is an expectation that there would be a desire to avoid peak hour congestion so the peak hour number \% would reduce. This approach was discussed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ (in each direction) x 4.2\% = trucks on and off site per hour in AM peak in each direction

## 340 semi movements per weekday $\div 2 \times 4.2 \%=7$ semi-truck movements in $A M$ peak hour in each direction

## 2,439 rigid movements per weekday $\div 2 \times 4.2 \%=51$ rigid truck movements in AM peak hour in each direction

Table 18 : Average IMEX warehouse related weekday inbound and outbound truck movements 2030

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | Semi | 170 | 7 |
|  |  | Inbound | Remid | 1,220 |

Note: Some truck numbers have been rounded to the nearest whole number

### 4.5.2 Interstate Containers 2030

The following steps were taken to derive the daily truck movements in and out of Moorebank IMT for interstate cargo handled through the warehouses:

1. As for the IMEX, the Moorebank IMT will have enough on-site warehousing capacity to handle approximately $20 \%$ of all full TEUs. It is assumed that half of these will be held in inventory in onsite warehousing for a period of weeks with the rest being general cargo (FAK) which would be deconsolidated and distributed offsite within a few days or arrive onsite for consolidation and export.

## 120,000 full inbound TEUs x 10\% FAK = 12,000 TEU's FAK for distribution from

 site120,000 full inbound TEUs $\boldsymbol{x} 10 \%$ Inventory $=12,000$ TEU's Inventory for distribution from site

120,000 full outbound TEU's x 10\% FAK = 12,000 TEU's FAK arriving at site for consolidation

120,000 full outbound TEU's x 10\% Inventory = 12,000 TEU's Inventory arriving at site for consolidation
2. It is assumed that the terminal would be operational 52 weeks per year.

$$
\begin{aligned}
& \text { 12,000 FAK }+12,000 \text { Inventory TEUs } \div 52=462 \text { TEUs into warehouse and } \\
& \text { distributed off site each week }
\end{aligned}
$$

12,000 FAK + 12,000 Inventory TEUs $\div 52=462$ TEUs arrive onto site and into warehouse each week
3. It is assumed that each TEU, when deconsolidated will generate approximately 25 pallet loads for domestic distribution:

462 TEU's x 25 equivalent pallet loads per TEU = 11,538 equivalent pallet loads into warehouse and distributed off site by road each week

462 TEU's x 25 equivalent pallet loads per TEU $=11,538$ equivalent pallet loads into warehouse by road and railed offsite each week
4. The truck fleet profile for palletised cargo will be different to that for direct FCL and MT container movements to and from the Moorebank terminal. It is assumed that trucks moving pallets out of Moorebank IMT warehousing will comprise of $34 \%$ semi-trailers and $66 \%$ rigid trucks whilst $100 \%$ of the palletised cargo arriving at the site will be carried by rigid trucks:

Deliveries from Moorebank warehouses:
11,538 pallets per week $x 34 \%=3,923$ pallets out on semi-trailer trucks

# 11,538 pallets per week $x 66=7,615$ pallets out on rigid trucks <br> Deliveries to Moorebank warehouses: <br> 11,538 pallets per week $\times 100 \%=11,538$ pallets in on rigid trucks 

5. Semi-trailer trucks are likely to carry, on average 20 pallets per truck whilst rigid trucks have been assumed to carry, on average 8 pallets per load. Dividing the number of pallets by each average load determines the average number of loaded truck movements per week into and out of the warehouses.

Deliveries from Moorebank warehouses:
3,923 pallets in semis per week $\div 20$ pallets per truck $=196$ loaded semi-trailer truck movements out per week

7,615 pallets in rigids per week $\div 8$ pallets per truck $=952$ loaded rigid truck movements out per week

Deliveries to Moorebank warehouses:
11,538 pallets in rigids per week $\div 8$ pallets per truck = 1,442 loaded rigid truck movements in per week
6. It is assumed that there will be no truck load matching for palletised cargo movement to and from the Moorebank IMT warehouses. Therefore all movements would generate an empty running leg into or out of the terminal. By adding the total inbound and outbound movements the total truck movements can be estimated.

Empty running trips in = loaded trips out X (1-\% load matching factor)
196 semis empty into terminal per week $=196$ loaded semis outbound $X$ (1-0\% matched loads)

952 empty rigids into terminal per week = 952 loaded rigids outbound X (1-0\% matched loads)

1,442 empty rigids out of terminal per week $=1,442$ loaded rigids inbound X (10\% matched loads)

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips out + loaded trips in + empty trips in

Total semi movements = 196 loads out +0 empty out +0 loads in +196 empty in
$=196$ trips out +196 trips in
= 392 trips per week

## Total rigid movements $\quad=952$ loads out $+1,442$ empty out $+1,442$ loads in + 952 empty in <br> $=2,394$ trips out $+2,394$ trips in <br> = 4,788 trips per week

7. It was then assumed that $95 \%$ of container truck movements would occur on weekdays and $5 \%$ would occur on weekends. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday
(392 semi-truck movements per week $X$ 95\%) $\div 5=75$ semi-trailer movements per weekday
(4,788 rigid truck movements per week $X 95 \%) \div 5=910$ rigid truck movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 19 below.

Table 19 : Average weekly interstate inbound and outbound warehouse related road movements 2030

| Truck Status | Direction on <br> road | Truck Type | Trucks per <br> week <br> (a) | Average trucks <br> per Weekday <br> (b) |
| :--- | :--- | :--- | :---: | :---: |
| Loaded | Outbound | Semi | 196 | 37 |
|  |  | Rigid | 952 | 181 |
| Empty | Inbound | Semi | 196 | 37 |
|  | Inbound | Rigid | 952 | 181 |
|  |  | Semi | 0 | - |
| Empty | Outbound | Rigid | 1,442 | 274 |
|  |  | Semi | 0 | - |
| Total Truck <br> movements | Outbound | Rigid | 1,442 | 274 |
|  |  | Semi | Rigid | 2,394 |

8. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is one $24^{\text {th }}$ of the daily value. This is used because whilst the daily hours of operation may be less than 24 , there is an expectation that there would be a desire to avoid peak hour congestion so the peak hour number \% would reduce. This approach was agreed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ (in each direction) $x 4.2 \%=$ trucks on and off site per hour in AM peak in each direction

75 semi movements per weekday $\div 2 \times 4.2 \%=2$ semi-truck movements in AM peak hour in each direction

910 rigid movements per weekday $\div 2 \times 4.2 \%=19$ rigid truck movements in $A M$ peak hour in each direction

Table 20 : Total average weekday interstate related warehouse truck movements

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | Semi | 37 | 2 |
|  |  | Rigid | 455 | 19 |
|  |  | Semi | 37 | 2 |

### 4.5.3 Interstate Containers 2050

The following steps were taken to derive the daily truck movements in and out of Moorebank IMT for interstate cargo handled through the warehouses:

1. As for the IMEX, the Moorebank IMT will have enough on-site warehousing capacity to handle approximately $20 \%$ of all full TEUs. It is assumed that half of these will be held in inventory in onsite warehousing for a period of weeks with the rest being general cargo (FAK) which would be deconsolidated and distributed offsite within a few days or arrive onsite for consolidation and export.

149,000 full inbound TEUs x 10\% FAK = 14,900 TEU's FAK for distribution from site

149,000 full inbound TEUs x 10\% Inventory = 14,900 TEU's Inventory for distribution from site

149,000 full outbound TEU's x 10\% FAK = 14,900 TEU's FAK arriving at site for consolidation

149,000 full outbound TEU's $x$ 10\% Inventory $=14,900$ TEU's Inventory arriving at site for consolidation
2. It is assumed that the terminal would be operational 52 weeks per year.

> 14,900 FAK + 14,900 Inventory TEUs $\div 52=573$ TEUs into warehouse and distributed off site each week

> 14,900 FAK + 14,900 Inventory TEUs $\div 52=573$ TEUs arrive onto site and into warehouse each week
3. It is assumed that each TEU, when deconsolidated will generate approximately 25 pallet loads for domestic distribution:

573 TEU's x 25 equivalent pallet loads per TEU = 14,327 equivalent pallet loads into warehouse and distributed off site by road each week

573 TEU's x 25 equivalent pallet loads per TEU = 14,327 equivalent pallet loads into warehouse by road and railed offsite each week
4. The truck fleet profile for palletised cargo will be different to that for direct FCL and MT container movements to and from the Moorebank terminal. It is assumed that trucks moving pallets out of Moorebank IMT warehousing will comprise of $34 \%$ semi-trailers and $66 \%$ rigid trucks whilst $100 \%$ of the palletised cargo arriving at the site will be carried by rigid trucks:

Deliveries from Moorebank warehouses:
14,327 pallets per week $x 34 \%=4,871$ pallets out on semi-trailer trucks

14,327 pallets per week $\times 66 \%=9,456$ pallets out on rigid trucks

Deliveries to Moorebank warehouses:
14,327 pallets per week $\times 100 \%=14,327$ pallets in on rigid trucks
5. Semi-trailer trucks are likely to carry, on average 20 pallets per truck whilst rigid trucks have been assumed to carry, on average 8 pallets per load. Dividing the number of pallets by each average load determines the average number of loaded truck movements per week into and out of the warehouses.

Deliveries from Moorebank warehouses:
4,871 pallets in semis per week $\div 20$ pallets per truck $=244$ loaded semi-trailer truck movements out per week

9,456 pallets in rigids per week $\div 8$ pallets per truck $=1,182$ loaded rigid truck movements out per week

Deliveries to Moorebank warehouses:
14,327 pallets in rigids per week $\div 8$ pallets per truck $=1,791$ loaded rigid truck movements in per week
6. It is assumed that there will be no truck load matching for palletised cargo movement to and from the Moorebank IMT warehouses. Therefore all movements would generate an empty running leg into or out of the terminal. By adding the total inbound and outbound movements the total truck movements can be estimated.

## Empty running trips in = loaded trips out $\boldsymbol{X}$ ( 1 - \% load matching factor)

244 semis empty into terminal per week $=244$ loaded semis outbound X (1-0\% matched loads)

1,182 empty rigids into terminal per week $=1,182$ loaded rigids outbound $X$ (10\% matched loads)

1,791 empty rigids out of terminal per week $=1,791$ loaded rigids inbound X (10\% matched loads)

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips out + loaded trips in + empty trips in

Total semi movements = 244 loads out $\mathbf{+} 0$ empty out $\mathbf{+} 0$ loads in $\mathbf{+} \mathbf{2 4 4}$ empty in
$=244$ trips out +244 trips in
= 487 trips per week
Total rigid movements $=1,182$ loads out $+1,791$ empty out $+1,791$ loads in + 1,182 empty in
= 2,973 trips out + 2,973 trips in
= 5,946 trips per week
7. It was then assumed that $95 \%$ of container truck movements would occur on weekdays and $5 \%$ would occur on weekends. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday
(487 semi-truck movements per week $X$ 95\%) $\div 5=93$ semi-trailer movements per weekday
(5,946 rigid truck movements per week $X 95 \%$ ) $\div 5=1,130$ rigid truck movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 21 below.

Table 21: Average weekly inbound and outbound warehouse related road movements

| Truck Status | Direction on <br> road | Truck Type | Trucks per <br> week <br> (a) | Average trucks <br> per Weekday <br> (b) |
| :--- | :--- | :--- | :---: | :---: |
| Loaded | Outbound | Semi | 244 | 46 |
|  |  | Rigid | 1,182 | 225 |
| Empty | Inbound | Semi | 244 | 46 |
|  |  | Rigid | 1,182 | 225 |
| Loaded | Inbound | Semi | 0 | - |
|  |  | Rigid | 1,791 | 340 |


| Truck Status | Direction on <br> road | Truck Type | Trucks per <br> week <br> (a) | Average trucks <br> per Weekday <br> (b) |
| :--- | :--- | :---: | :---: | :---: |
| Empty | Outbound | Semi | 0 | - |
|  |  | Rigid | 1,791 | 340 |
|  | Outbound | Semi | 244 | 46 |
|  | Inbound | Rigid | 2,973 | 565 |
|  |  | Semi | 244 | 46 |

8. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is one $24^{\text {th }}$ of the daily value. This is used because whilst the daily hours of operation may be less than 24 , there is an expectation that there would be a desire to avoid peak hour congestion so the peak hour number $\%$ would reduce. This approach was agreed with RMS and FTBS in March 2014.

Average trucks per weekday $\div 2$ (in each direction) x $4.2 \%=$ trucks on and off site per hour in AM peak in each direction

93 semi movements per weekday $\div 2 \times 4.2 \%=2$ semi-truck movements in AM peak hour in each direction

1,130 rigid movements per weekday $\div 2 \times 4.2 \%=24$ rigid truck movements in AM peak hour in each direction

Table 22 : Average total weekday truck movements for interstate related warehouse activity at 2050

| Truck Status | Direction on road | Truck Type | Average trucks per Weekday | Trucks per hour AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck movements | Outbound | Semi | 46 | 2 |
|  |  | Rigid | 565 | 24 |
|  | Inbound | Semi | 46 | 2 |
|  |  | Rigid | 565 | 24 |

### 4.5.4 Combined IMEX and Interstate Containers 2030

Warehouse generated truck traffic movements were estimated using a similar methodology to the derivation of container truck movements, with some variation to the underlying assumptions. The most significant changes to the assumptions were:

- the makeup of the fleet;
- the proportion of movements occurring during the week; and
- the level of load matching.

The following steps were taken to derive the daily truck movements in and out of Moorebank IMT for cargo handled through the warehouses:

1. The Moorebank IMT will have enough on-site warehousing capacity to handle approximately $20 \%$ of all full TEUs. It is assumed that half of these will be held in inventory in onsite warehousing for a period of weeks with the rest being general cargo (FAK) which would be deconsolidated and distributed offsite within a few days or arrive onsite for consolidation and export.

667,000 full inbound TEUs x 10\% FAK = 66,700 TEU's FAK for distribution from site

667,000 full inbound TEUs x 10\% Inventory $=66,700$ TEU's Inventory for distribution from site

293,000 full outbound TEU's x 10\% FAK = 29,300 TEU's FAK arriving at site for consolidation

293,000 full outbound TEU's x 10\% Inventory = 29,300 TEU's Inventory arriving at site for consolidation
2. It is assumed that the terminal would be operational 52 weeks per year.

66,700 FAK + 66,700 Inventory TEUs $\div 52=2,565$ TEUs into warehouse and distributed off site each week

29,300 FAK + 29,300 Inventory TEUs $\div 52$ = 1,127 TEUs arrive onto site and into warehouse each week
3. It is assumed that each TEU, when deconsolidated will generate approximately 25 pallet loads for domestic distribution:

2,565 TEU's x 25 equivalent pallet loads per TEU $=64,135$ equivalent pallet loads into warehouse and distributed off site by road each week
$1,127 \times 25$ equivalent pallet loads per TEU $=28,173$ equivalent pallet loads into warehouse by road and railed offsite each week
4. The truck fleet profile for palletised cargo will be different to that for direct FCL and MT container movements to and from the Moorebank terminal. It is assumed that trucks moving pallets out of Moorebank IMT warehousing will comprise of $34 \%$ semi-trailers and $66 \%$ rigid trucks whilst $100 \%$ of the palletised cargo arriving at the site will be carried by rigid trucks:

Deliveries from Moorebank warehouses:
64,135 pallets per week $x 34 \%=21,806$ pallets out on semi-trailer trucks
64,135 pallets per week $\times 66 \%=42,329$ pallets out on rigid trucks

Deliveries to Moorebank warehouses:
28,173 pallets per week $\times 100 \%=28,173$ pallets in on rigid trucks
5. Semi-trailer trucks are likely to carry, on average 20 pallets per truck whilst rigid trucks have been assumed to carry, on average 8 pallets per load. Dividing the number of pallets by each average load determines the average number of loaded truck movements per week into and out of the warehouses.

Deliveries from Moorebank warehouses:
21,806 pallets in semis per week $\div 20$ pallets per truck $=1,090$ loaded semitrailer truck movements out per week

42,329 pallets in rigids per week $\div 8$ pallets per truck $=5,291$ loaded rigid truck movements out per week

Deliveries to Moorebank warehouses:
28,173 pallets in rigids per week $\div 8$ pallets per truck $=$ 3,522 loaded rigid truck movements in per week
6. It is assumed that there will be no truck load matching for palletised cargo movement to and from the Moorebank IMT warehouses. Therefore all movements would generate an empty running leg into or out of the terminal. By adding the total inbound and outbound movements the total truck movements can be estimated.

Empty running trips in = loaded trips out X (1-\% load matching factor)
1,090 semis empty into terminal per week = 1,090 loaded semis outbound X (10\% matched loads)

5,291 empty rigids into terminal per week = 5,291 loaded rigids outbound X (10\% matched loads)

3,522 empty rigids out of terminal per week $=3,522$ loaded rigids inbound X (1 0\% matched loads)

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips out + loaded trips in + empty trips in

Total semi movements = 1,090 loads out +0 empty out +0 loads in +1,090 empty in
$=1,090$ trips out $+1,090$ trips in
= 2,181 trips per week
Total rigid movements $=5,291$ loads out $+3,522$ empty out $+3,522$ loads in + 5,291 empty in
$=8,813$ trips out $+8,813$ trips in
= 17,625 trips per week
7. It was then assumed that $95 \%$ of container truck movements would occur on weekdays and $5 \%$ would occur on weekends. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday
(2,181 semi-truck movements per week $X$ 95\%) $\div 5=414$ semi-trailer movements per weekday
(17,625 rigid truck movements per week $X$ 95\%) $\div 5=3,349$ rigid truck movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 23 below.

Table 23 : Average weekly inbound and outbound warehouse related road movements 2030 for IMEX and Interstate combined

| Truck Status | Direction on road | Truck Type | Trucks per week <br> (a) | Average trucks per Weekday <br> (b) |
| :---: | :---: | :---: | :---: | :---: |
| Loaded | Outbound | Semi | 1,090 | 207 |
|  |  | Rigid | 5,291 | 1,005 |
| Empty | Inbound | Semi | 1,090 | 207 |
|  |  | Rigid | 5,291 | 1,005 |
| Loaded | Inbound | Semi | 0 | - |
|  |  | Rigid | 3,522 | 669 |
| Empty | Outbound | Semi | 0 | - |
|  |  | Rigid | 3,522 | 669 |
| Total Truck movements | Outbound | Semi | 1,090 | 207 |
|  |  | Rigid | 8,813 | 1,674 |
|  | Inbound | Semi | 1,090 | 207 |
|  |  | Rigid | 8,813 | 1,674 |

8. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is one $24^{\text {th }}$ of the daily value. This is used because whilst the daily hours of operation may be less than 24 , there is an expectation that there would be a desire to avoid peak hour congestion so the peak hour number \% would reduce. This approach was agreed with RMS and FTBS in March 2014.

Average trucks per weekday in each direction x 4.2\% = trucks on and off site per hour in AM peak in each direction

207 semi movements in each direction per weekday x 4.2\% = 9 semi-truck movements in AM peak hour in each direction

## 1,674 rigid movements in each direction per weekday x 4.2\% = 70 rigid truck movements in AM peak hour in each direction

Table 24 : Total combined average weekday truck movements for warehousing activity at 2030

| Truck Status | Direction on road | Truck Type | Average trucks per Weekday | Trucks per hour AM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Total Truck movements | Outbound | Semi | 207 | 9 |
|  |  | Rigid | 1,674 | 70 |
|  | Inbound | Semi | 207 | 9 |
|  |  | Rigid | 1,674 | 70 |

Note: Some truck numbers have been rounded to the nearest whole number
A consolidated flow diagram for movements of full container loads out of the terminal, warehouse generated loads out of the terminal and associated empty running truck trips are illustrated in the following flow diagram.

Figure 7 : Total average weekday truck movements at 2030


Note that there may be some minor differences in truck numbers between the flow diagram and the tables due to consolidation of figures and rounding. A full size diagram is included at Appendix A.

### 4.5.5 Combined IMEX and Interstate Containers 2050

As stated previously, warehouse generated truck traffic movements were estimated using a similar methodology to the derivation of container truck movements, with some variation to the underlying assumptions. The most significant changes to the assumptions were:

- the makeup of the fleet;
- the proportion of movements occurring during the week; and
- the level of load matching.

The following steps were taken to derive the daily truck movements in and out of Moorebank IMT for cargo handled through the warehouses:

1. The Moorebank IMT will have enough on-site warehousing capacity to handle approximately $20 \%$ of all full TEUs. It is assumed that half of these will be held in inventory in onsite warehousing for a period of weeks with the rest being general cargo (FAK) which would be deconsolidated and distributed offsite within a few days or arrive onsite for consolidation and export.

696,000 full inbound TEUs x $10 \%$ FAK $=69,600$ TEU's FAK for distribution from site

696,000 full inbound TEUs x 10\% Inventory = 69,600 TEU's Inventory for distribution from site

## 322,000 full outbound TEU's x 10\% FAK = 32,200 TEU's FAK arriving at site for consolidation

322,000 full outbound TEU's x 10\% Inventory = 32,200 TEU's Inventory arriving at site for consolidation
2. It is assumed that the terminal would be operational 52 weeks per year.

69,600 FAK $+69,600$ Inventory TEUs $\div 52=2,677$ TEUs into warehouse and distributed off site each week

32,200 FAK $+\mathbf{3 2 , 2 0 0}$ Inventory TEUs $\div 52=1,238$ TEUs arrive onto site and into warehouse each week
3. It is assumed that each TEU, when deconsolidated will generate approximately 25 pallet loads for domestic distribution:

2,677 TEU's $\times 25$ equivalent pallet loads per TEU = 66,923 equivalent pallet loads into warehouse and distributed off site by road each week
$1,238 \times 25$ equivalent pallet loads per TEU $=30,962$ equivalent pallet loads into warehouse by road and railed offsite each week
4. The truck fleet profile for palletised cargo will be different to that for direct FCL and MT container movements to and from the Moorebank terminal. It is assumed that
trucks moving pallets out of Moorebank IMT warehousing will comprise of $34 \%$ semi-trailers and $66 \%$ rigid trucks whilst $100 \%$ of the palletised cargo arriving at the site will be carried by rigid trucks:

Deliveries from Moorebank warehouses.
66,923 pallets per week $\times 34 \%=22,754$ pallets out on semi-trailer trucks

66,923 pallets per week $\times 66 \%=44,169$ pallets out on rigid trucks

Deliveries to Moorebank warehouses:
30,950 pallets per week $\times 100 \%=30,962$ pallets in on rigid trucks
5. Semi-trailer trucks are likely to carry, on average 20 pallets per truck whilst rigid trucks have been assumed to carry, on average 8 pallets per load. Dividing the number of pallets by each average load determines the average number of loaded truck movements per week into and out of the warehouses.

Deliveries from Moorebank warehouses:
22,754 pallets in semis per week $\div 20$ pallets per truck $=1,138$ loaded semitrailer truck movements out per week

44,169 pallets in rigids per week $\div 8$ pallets per truck $=5,521$ loaded rigid truck movements out per week

Deliveries to Moorebank warehouses:
30,962 pallets in rigids per week $\div 8$ pallets per truck $=3,870$ loaded rigid truck movements in per week
6. It is assumed that there will be no truck load matching for palletised cargo movement to and from the Moorebank IMT warehouses. Therefore all movements would generate an empty running leg into or out of the terminal. By adding the total inbound and outbound movements the total truck movements can be estimated.

Empty running trips in = loaded trips out X (1 - \% load matching factor)
1,138 semis empty into terminal per week $=1,138$ loaded semis outbound $X$ (10\% matched loads)

5,521 empty rigids into terminal per week = 5,521 loaded rigids outbound X (10\% matched loads)

3,870 empty rigids out of terminal per week $=3,870$ loaded rigids inbound $X$ (10\% matched loads)

By adding the total inbound and outbound movements the total truck movements can be estimated. To generate total number of trips for each truck type:

Total trips per week = loaded trips out + empty trips out + loaded trips in + empty trips in

```
Total semi movements \(\quad=1,138\) loads out +0 empty out +0 loads in \(+1,138\)
    empty in
    = 1,138 trips out \(+1,138\) trips in
    = 2,275 trips per week
Total rigid movements \(=5,521\) loads out \(+3,870\) empty out \(+3,870\) loads in +
    5,521 empty in
    \(=9,391\) trips out \(+9,391\) trips in
    \(=18,783\) trips per week
```

7. It was then assumed that $95 \%$ of container truck movements would occur on weekdays and $5 \%$ would occur on weekends. The proportion on weekdays was then divided by 5 to reach an average number of truck moves per weekday
(2,275 semi-truck movements per week $X$ 95\%) $\div 5=432$ semi-trailer movements per weekday
(18,783 rigid truck movements per week X 95\%) $\div 5=3,569$ rigid truck movements per weekday

Total inbound and outbound moves per week and per weekday can be summarised in Table 25 below.

Table 25 : Average weekly inbound and outbound warehouse related road movements 2050 for IMEX and Interstate combined

| Truck Status | Direction on road | Truck Type | Trucks per week (a) | Average trucks per Weekday <br> (b) |
| :---: | :---: | :---: | :---: | :---: |
| Loaded | Outbound | Semi | 1,138 | 216 |
|  |  | Rigid | 5,521 | 1,049 |
| Empty | Inbound | Semi | 1,138 | 216 |
|  |  | Rigid | 5,521 | 1,049 |
| Loaded | Inbound | Semi | 0 | - |
|  |  | Rigid | 3,870 | 735 |
| Empty | Outbound | Semi | 0 | - |
|  |  | Rigid | 3,870 | 735 |
| Total Truck movements | Outbound | Semi | 1,138 | 216 |
|  |  | Rigid | 9,391 | 1,784 |
|  | Inbound | Semi | 1,138 | 216 |
|  |  | Rigid | 9,391 | 1,784 |

8. Daily truck volumes were multiplied by $4.2 \%$ to generate indicative peak hourly truck volumes for each vehicle class both inbound and outbound. The $4.2 \%$ is one 24th of the daily value. This is used because whilst the daily hours of operation may be less Liability limited by a scheme approved under Professional Standards Legislation.
than 24 , there is an expectation that there would be a desire to avoid peak hour congestion so the peak hour number $\%$ would reduce. This approach was agreed with RMS and FTBS in March 2014.

## Average trucks per weekday $\div 2$ (in each direction) $x 4.2 \%=$ trucks on and off site per hour in AM peak in each direction

432 semi movements $\div 2$ in each direction per weekday $\times 4.2 \%=9$ semi-truck movements in AM peak hour in each direction

3,569 rigid movements $\div 2$ in each direction per weekday $\times 4.2 \%=75$ rigid truck movements in AM peak hour in each direction

Table 26 : Total combined average weekday truck movements for warehousing activity at 2050

| Truck Status | Direction on <br> road | Truck Type | Average trucks <br> per Weekday | Trucks per hour <br> AM Peak |
| :--- | :---: | :---: | :---: | :---: |
| Total Truck <br> movements | Outbound | Semi | 216 | 9 |
|  |  | Inbound | Rigid | 1,784 |

Note: Some truck numbers have been rounded to the nearest whole number
A consolidated flow diagram for movements of full container loads out of the terminal, warehouse generated loads out of the terminal and associated empty running truck trips are illustrated in the following flow diagram.

Figure 8 : Total average weekday truck movements at 2050


Note that there may be some minor differences between the flow diagram and the tables due to consolidation of figures and rounding. A full size diagram is included at Appendix A.

## 5 Additional Sensitivity Analysis

### 5.1 Key Assumptions that impact on Trip Generation

Each of the assumptions set out Section 4.1 can have a significant impact on the number of truck trips generated as a result of both direct movements of containers to and from the terminal and also for cargo movements to and from the warehouses.
We have selected three of these assumptions which are specifically related to the nature of the truck operation and freight distribution to illustrate the relative potential impact that factors beyond the control of the terminal operator could have on possible truck volumes.

### 5.1.1 Pallet Loads

The analysis assumes that 20 per cent of all cargo through the terminal will go via the onsite warehousing. Once the cargo in the import containers is deconsolidated it will either be delivered within a matter of days or stored as inventory and distributed as required.
Furthermore, we have assumed that the majority ( $66 \%$ ) of these movements will be undertaken by rigid vehicles based on the notion that customers who wish to receive larger consignments of cargo on a regular basis may seek to have a full container delivered as a means of avoiding the additional handling costs of unpacking the cargo offsite.

There are a number of truck configurations within what is generally classified as a rigid vehicle. Load capacities range from approximately 6 tonne to as high as 14 tonne with floor space for between 8 and 14 pallets.
Given the light weight of most import containers (the average weight is between 12 and 13 tonne) we have considered the cubic capacity as more relevant and translated cargo volumes to the number of pallets and allocated pallets to truck capacity for the generation of vehicle volumes as set out in the earlier sections.

A conservative approach was taken with regard to the likely volumes carried by each rigid truck arriving or leaving the terminal and an average of 8 pallets per truck was assumed. The impact of achieving a higher pallet load per truck on rigid truck trips generated against the base scenario is illustrated in Table 27 and Table 28 below.

Table 27 : Sensitivity analysis for outbound AM peak hour truck movements for warehousing activity assuming different pallet loads for rigid trucks

| Outbound | 2030 |  |  | 2050 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8 Pallet | 12 Pallet | 14 Pallet | 8 Pallet | 12 Pallet | 14 Pallet |
|  | 0 | 0 | 0 | 0 | 0 | 0 |
| Semi | 9 | 9 | 9 | 9 | 9 | 9 |
| Rigid | 70 | 47 | 40 | 75 | 50 | 43 |
| TOTAL | 79 | 56 | 49 | 84 | 59 | 52 |

Table 28 : Sensitivity analysis for inbound AM peak hour truck movements for warehousing activity assuming different pallet loads for rigid trucks

| Inbound | 2030 |  |  | 2050 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8 Pallet | 12 Pallet | 8 Pallet | 12 Pallet | 8 Pallet | 12 Pallet |
|  | 0 | 0 | 0 | 0 | 0 | 0 |
| Semi | 9 | 9 | 9 | 9 | 9 | 9 |
| Rigid | 70 | 47 | 40 | 75 | 50 | 43 |
| Total | 79 | 56 | 49 | 84 | 59 | 52 |

### 5.1.2 Distribution during AM Peak period

The volume of traffic arriving and leaving the terminal during the AM peak period will be a function of the transport company and their deployment of resources, the proximity, location and operating hours of the cargo owner and the underlying level of congestion on the network during both the peak and inter peak periods.
For the purposes of our analysis we assumed that, over the next 20 years the level of congestion on the road network will rise, particularly at and close to the peak hours in the morning and evening. As a result we believe that cargo owners may wish to minimise the number of movements during the peak hour where possible as the additional costs of standing in traffic will be passed onto them by transport operators - time is as important a factor on transport costs as distance.

The trip generation analysis conducted in earlier sections has been undertaken using a distribution during the AM peak of $4.2 \%$ of total weekday volumes. The following tables illustrate the possible distribution at two other allocations $-6 \%$ and $7 \%$ respectively.

Table 29 : Sensitivity analysis for AM peak hour truck movements for both direct and warehouse related traffic - Peak Hour distribution

|  | 2030 |  |  | 2050 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| In each <br> direction | $4.2 \%$ of <br> daily <br> volume | $6 \%$ of daily <br> volume | $\mathbf{7} \%$ of daily <br> volume | $4.2 \%$ of <br> daily <br> volume | $6 \%$ of daily <br> volume | $7 \%$ of daily <br> volume |
| Bdouble | 13 | 18 | 21 | 13 | 19 | 22 |
| Semi | 73 | 104 | 121 | 77 | 110 | 128 |
| Rigid | 70 | 100 | 117 | 75 | 107 | 125 |
| Total | 156 | 223 | 260 | 165 | 236 | 276 |

### 5.2 Impact of Cumulative Scenarios

As part of the sensitivity analysis we have also assessed the potential impact on both warehousing requirements and truck trip generation should there be both the SIMTA and Moorebank Terminal developments in this location. The two possible scenarios considered were:

1. The IMEX terminal at Moorebank only handles 500,000 TEU at its peak; or
2. The terminal at Moorebank only handles interstate cargoes with the assumption that the SIMTA facility handles all the IMEX volumes.

These scenarios have an impact on both the likely amount of onsite warehousing required to cater to the cargo passing through the intermodal terminal and the likely truck trips generated as a result of the reduced volumes.

It is assumed that any surplus warehousing (i.e. the potential capacity for warehousing on site of $300,000 \mathrm{~m} 2$ less the required warehousing) will be utilised for general distribution activities by the market. Truck trips for the surplus warehousing are not included in the calculations within this technical note.

### 5.2.1 Scenario One - Reduced IMEX volume

A summary of the total volumes for this scenario is set below in Table 30.

Table 30 : Scenario 1 - Reduced IMEX (500k TEU only) plus Interstate

|  | 2030 |  |  |  | 2050 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Terminal <br> Throughput | IMEX | Interstate | Total | IMEX | Interstate | Total |  |
| ('000 TEU) | ('000 TEU) | ('000 TEU) | ('000 TEU) | ('000 TEU) | ('000 TEU) |  |  |
| Total Imports | 261.663 | 164.000 | 425.663 | 261.663 | 203.000 | 464.663 |  |
| Total Exports | 238.337 | 164.000 | 402.337 | 238.337 | 203.000 | 441.337 |  |
| Total Throughput | $\mathbf{5 0 0 . 0 0 0}$ | $\mathbf{3 2 8 . 0 0 0}$ | $\mathbf{8 2 8 . 0 0 0}$ | $\mathbf{5 0 0 . 0 0 0}$ | $\mathbf{4 0 6 . 0 0 0}$ | $\mathbf{9 0 6 . 0 0 0}$ |  |


| Warehousing Requirements m2 | For <br> Freight <br> All Kinds <br> (FAK) | For Inventory (INV) | Total | For <br> Freight <br> All Kinds <br> (FAK) | For Inventory (INV) | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Associated warehousing | 37,948 | 149,420 | 187,368 | 41,718 | 164,264 | 205,982 |
| Surplus warehousing |  |  | 112,632 |  |  | 94,018 |

Note that volumes in the table exclude transhipments

Utilising the same methodology outlined in Section 4 for the generation of truck trips the following estimates for AM Peak period were derived. See Table 31.

Table 31 : Reduced IMEX Scenario - Total combined average weekday truck movements for combined activity at 2030 and 2050

| Truck trips generated at AM Peak Weekdays |  | 2030 |  |  | 2050 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | IMEX | Interstate | Total | IMEX | Interstate | Total |
| Direct <br> Containers | Outbound |  |  |  |  |  |  |
|  | Bdouble | 5 | 3 | 8 | 5 | 4 | 8 |
|  | Semi | 23 | 16 | 39 | 23 | 20 | 43 |
|  | Rigid | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Total | 27 | 20 | 47 | 27 | 24 | 52 |
|  | Inbound |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  | Bdouble | 5 | 3 | 8 | 5 | 4 | 8 |
|  | Semi | 23 | 16 | 39 | 23 | 20 | 43 |
|  | Rigid | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Total | 27 | 20 | 47 | 27 | 24 | 52 |


| Warehousing Related | Outbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Bdouble | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Semi | 3 | 2 | 5 | 3 | 2 | 5 |
|  | Rigid | 24 | 19 | 44 | 24 | 24 | 48 |
|  | Total | 28 | 21 | 49 | 28 | 26 | 54 |
|  | Inbound |  |  |  |  |  |  |
|  | Bdouble | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Semi | 3 | 2 | 5 | 3 | 2 | 5 |
|  | Rigid | 24 | 19 | 44 | 24 | 24 | 48 |
|  | Total | 28 | 21 | 49 | 28 | 26 | 54 |


| Combined total | Outbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Bdouble | 5 | 3 | 8 | 5 | 4 | 8 |
|  | Semi | 26 | 18 | 44 | 26 | 22 | 48 |
|  | Rigid | 24 | 19 | 44 | 24 | 24 | 48 |
|  | Total | 55 | 40 | 95 | 55 | 50 | 105 |
|  | Inbound |  |  |  |  |  |  |
|  | Bdouble | 5 | 3 | 8 | 5 | 4 | 8 |
|  | Semi | 26 | 18 | 44 | 26 | 22 | 48 |
|  | Rigid | 24 | 19 | 44 | 24 | 24 | 48 |
|  | Total | 55 | 40 | 95 | 55 | 50 | 105 |

### 5.2.2 Scenario Two - Interstate terminal only

A summary of the total volumes for this scenario is set below in Table 32.

Table 32 : Scenario 2 - Interstate Terminal cargo only

|  | 2030 |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Terminal |  |  |  |  |  |  |
| Throughput | IMEX | Interstate | Total | IMEX | Interstate | Total |
| Liability limited by a scheme approved under Professional Standards Legislation. | 66 |  |  |  |  |  |
| © 2014 Deloitte Touche Tohmatsu |  |  |  |  |  |  |


|  | ('000 TEU) | ('000 TEU) | ('000 TEU) | ('000 TEU) | ('000 TEU) | ('000 TEU) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Total Imports | 0 | 164.000 | 164.000 | 0 | 203.000 | 203.000 |
| Total Exports | 0 | 164.000 | 164.000 | 0 | 203.000 | 203.000 |
| Total Throughput | $\mathbf{0}$ | $\mathbf{3 2 8 . 0 0 0}$ | $\mathbf{3 2 8 . 0 0 0}$ | $\mathbf{0}$ | $\mathbf{4 0 6 . 0 0 0}$ | $\mathbf{4 0 6 . 0 0 0}$ |


| Warehousing Requirements m2 | For <br> Freight <br> All Kinds <br> (FAK) | For Inventory (INV) | Total | For <br> Freight <br> All Kinds <br> (FAK) | For Inventory (INV) | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Associated warehousing | 15,600 | 61,425 | 77,025 | 19,370 | 76,269 | 95,639 |
| Surplus warehousing |  |  | 222,975 |  |  | 204,361 |

Note that volumes in the table exclude transhipments

Utilising the same methodology outlined in Section 4 for the generation of truck trips the following estimates for AM Peak period were derived. See Table 33.

Table 33 : Interstate Only Scenario - Total combined average weekday truck movements for combined activity at 2030 and 2050


| Combined total | Outbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Bdouble | 3 | 3 | 4 | 4 |
|  | Semi | 18 | 18 | 22 | 22 |
|  | Rigid | 19 | 19 | 24 | 24 |
|  | Total | 40 | 40 | 50 | 50 |
|  | Inbound |  |  |  |  |
|  | Bdouble | 3 | 3 | 4 | 4 |
|  | Semi | 18 | 18 | 22 | 22 |
|  | Rigid | 19 | 19 | 24 | 24 |
|  | Total | 40 | 40 | 50 | 50 |

## 6 Limitation of our work

## General use restriction

This report is prepared solely for the use of Moorebank Intermodal Company. This report is not intended to and should not be used or relied upon by anyone else and we accept no duty of care to any other person or entity. The report has been prepared for the purpose set out in Section 1 of this document. You should not refer to or use our name or the advice for any other purpose.

## Appendix A



Figure 9 : IMEX Flows through the terminal - 2030 to 2050


Figure 10 : Interstate flows through the terminal: 2030


Figure 11 : Interstate flows through the terminal: 2050


Figure 12 : IMEX and Interstate generated truck movements onto and off the terminal: 2030


Empty truck movements
To other clients or delivery to port directly
Internal movements

Liability limited by a scheme approved under Professional Standards Legislation.

Figure 13 : IMEX and Interstate generated truck movements onto and off the terminal: 2050


Empty truck movements
Internal movements
To other clients or delivery to port directly

Liability limited by a scheme approved under Professional Standards Legislation.


[^0]:    +ris
    IMT boundary
    Project site boundary
    $\square$ Northern rail access option
    -Central rail access option
    Southern rail access option

[^1]:    ${ }^{1}$ The figure is calculated as the SMVU total VKT for 'Capital City' multiplied by the SMVU ratio of workrelated VKT to total VKT for NSW (where 'Work-related' is defined as 'All business use' plus 'To and from work', and the 'Personal and other' category is excluded)

[^2]:    ${ }^{1}$ Based on the analysis of data provided by the Australian Customs and Border Protection Service (ACBPS)
    ${ }^{2}$ NSW Container Freight Improvement Strategy
    ${ }^{3}$ http://freight.transport.nsw.gov.au/strategy/task/volume.html
    Liability limited by a scheme approved under Professional Standards Legislation.

